2 (10.04 am) 3 SIR MARTIN MOORE BICK: Good morning, everybody. Welcome to book years printing the property of the control of the property of the control of	1	Tuesday, 20 November 2018	1	overview of conclusions to be drawn about the
sign MARTIN MOORE-BICK: Good morning, everybody. Welcome to doubly shearing with group system thoring from expert trained so with groups of advise us in recommendations arising from the same. Is that corner? Not Grange. Not Grange. Not Grantific Good meeting, Mr Chairman, Yes, we will be bearing today from Professor Jose Turror, who is one of the ecopers who will be going evidence with week. Professor Holly and Defensor Toeco. SIR MARTIN MOORE-BICK: Thank you, yes. PROFESSOR JOSE LUST TORERO (affirmed) Gownam and mela yourself controlable. Not Grange, before you seek, it make you you make a professor. Sit down and make yourself controlable. Not Grange, before you seek. It make we also be no asked to professor, indicate that you would be one at any other possible on the declaration in section 1.5 of your report, you have provided a report to a court; is that right? A. Yes, that's correct. Q. In section 1.4 of your report, you have outlined your background and experience relevant to the matters in this inquiry. We don't need to rehears all of that this		•		
todays hearing. Todays we are going to sust hearing from expert witnesses instructed by the inquiry to advise us in relation to various aspects of the fire. Yes, McGrange. MS GRANGE: Good morning, McChairman, Yes, we will be hearing udof from Professor, Not Torton, who is one of the hearing udof from Professor, Not Torton, who is one of the hearing udof from Professor, Not Torton, who is one of the hearing udof from Professor, Not Torton, who is one of the hearing udof from Professor, Not Torton, who is one of the hearing udof from Professor, Not Torton, who is one of the hearing udof from Professor, Not Torton, who is one of the hearing udof from Professor Torens. Sit MARTIN MORH-BRCK: Thanky you, yes. PROFESSOR JOSH LUIS TORERO (affirmed) Morninge, before you start. In such the professor is well used to delivering lectures and one material to work and make younded the morn and the possible of the months; I think we should have a beak during the middle of the months; I think we should have a new and the fire and smoke spread within Grenfell Tower, the correct? Page 1 stage. If you do, of course let me know. THE WITHNESS: Okay, thank you. Page 1 stage. If you do, of course let me know. Page 1 A Yes. 10 A Yes. 11 A Yes. 12 A Yes. 13 Q. That report addresses your preliminary onclusions on the provide a further report at Plasse 2 which with fire and smoke spread within Grenfell Tower; that's right, yes? 12 A Yes. 13 A Yes, that's correct. Q. In associated, professor that we will be mean any other the professor of civil engineering at the University of Maryland in the USA; is that correct? Page 3 1 A Yes. 2 A Yes, that's correct. Q. Pow have provided to the inquiry a preliminary Plasse 1 report dated 23 May, and you have updated that report in a revised version dated 21 October poils, and also with an accompanying two-page addendum document dated 1 no accompanying two-page addendum document dated 1 no accompanying tw				·
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8 Yes, McGrange: 9 MS GRANGE: Good morning, Mr.Chairman. Yes, we will be leaving foday from Protessor foze Tozco, who is one of the leaving foday from Protessor foze Tozco, who is one of three experts who will be giving evidence this week. 11 Protessor Bialty and De Lanc will be flow tomorrow and 13 Thurnday. 13 Thurnday. 14 So if I can now call Professor Tozeo. 15 SIR MARTIN MOORE-BICK: Tankyou, yes. 16 PROFESSOR JOSE LUIS TORERO (affirmed) 17 Questions by MS GRANGE 18 SIR MARTIN MOORE-BICK: Thankyou vey much, professor. Sit down and make yeo foreign of the service of				
9 MS GRANGE: Good morning, Mr Chairman. Yes, we will be 10 hearing today from Professor fore Toreno. Who is one of 11 three experts who will be giving evidence this week. 12 Professor Bisby and Dr Lanc will follow tomorrow and 13 Thunday. 14 So if I can now call Professor Toreno. 15 SIR MARTIN MOORE BICK: Thank you, yes. 16 PROFESSOR (DISELLIST TORERO (affirmed) Questions by MS GRANGE: 17 Questions by MS GRANGE: 18 SIR MARTIN MOORE BICK: Thank you very much, professor. Sit down and make younged conformable. 19 down and make younged conformable. 19 for quite extended periods. but I think we should have 21 a break during the middle of the morning. I think 22 prosessor, indicate that you would like one at any other 25 professor, indicate that you would like one at any other 26 A. Jose Luis Torero Cullen. 27 Q. You specialise in the University of Maryland in the USA; is that correct? 28 A. Yes. 18 SIR MARTIN MOORE-BICK: Is that all right? 19 professor indicate that you would like one at any other 29 professor indicate that you would like one at any other 29 professor indicate that you would like one at any other 29 professor indicate that you and put the inquiry your name? 29 A. Yes. 20 Corober; is that right? 20 Q. You specialise in fire safety angineering and the University of Queensland in Australia between 2012 and 20 October; is that right? 20 Q. That report addresses your preliminary conclusions on the ignition of the Grenfell Tower; that fright, yes? 21 Q. Its important to note that you have also been 20 instructed to provide a further report at Plase 2 which will be a fire and smoke spread within Grenfell Tower; that's right, yes? 21 Q. Its important to note that you have also been 20 instructed to provide a further report at Plase 2 which will address fornesis fire and smoke spread within Grenfell Tower; that's correct. 20 Q. Its important to note that you have also been 20 instructed to provide a further report at Plase 2 which will address fornesis fire and smoke spread throughout 22 Grenfell Tower; the		-		
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thee experts who will be giving evidence this week. Professor lisby and Dr Lane will follow tomorrow and So if Lean now call Podessor Toerco. SIR MARTIX MOORE-BICK: Thank you, yes. FOFESSOR JOSE LIUS TORERO (affirmsd) Own and make youned confortable. MS GRANGE yous start. In sure the professor. Sit down and make youned confortable. MS Grange, before you start. In sure the professor. Sit a above during the middle of the morning. I think 24 possibly one break will be sufficient, unless you. Page 1 stage. If you do, of course let me know. THE WITNESS. Okay, thank you. SIR MARTIN MOORE-BICK: Is that all right? MS GRANGE: Yes, absolutely. Thank you. SIR MARTIN MOORE-BICK: Is that all right? MS GRANGE: Yes, absolutely. Thank you. SIR MARTIN MOORE-BICK: Is that all right? MS GRANGE: Yes, absolutely. Thank you. The work of the Grenfell Tower, and a revised version dated 21 October 2018, and also with an are companying two-page addendum document dated an accompanying two-page addendum document dated and fire and smoke spread within Grenfell Tower; the and fire and smoke spread within Grenfell Tower; the right, yes? A. Yes, that's correct. Q. I's important to note that you have also been instructed to provide a further report at Phase 2 which in fire safety or Fire Engineering and science over fire safety; is that are correct? A. Yes, that's correct. Q. I's important to note that you have also been instructed to provide a further report at Phase 2 which in fire safety or fire affects of the Centrell Tower; that's right, yes? The provided of the inquiry provided to the inquiry our mane? A. Yes, that's correct. Q. I's important to note that you have also been instructed to provide a further report at Phase 2 which instructed to provide a further report at Phase 2 which instructed to provide a further report at Phase 2 which instructed to provide a further report at Phase 2 which instructed to provide a further report at Phase 2 which instructed to provide a further report at Phase 2 which instructed to prov				
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13 Thursday. 14 So if I can now call Professor Toren. 15 SIR MARTIN MOORE-BICK: Thank you, yes. 16 PROFESSOR LOSE LUIS TORERO (affirmed) 17 Questions by MS GRANGE 18 SIR MARTIN MOORE-BICK: Thank you very much, professor. Sit 19 down and make youncelf comfortable. 20 Ms Grange, before you start. In sure the professor 21 is well used to delivering lectures and other material 22 for quite extended periods, but I think we should have 23 a break during the middle of the morning. I think 24 possibly one break will be sufficient, unless you, 25 professor, indicate that you would like one at any other 26 Page 1 1 stage. If you do, of course let me know. 27 THE WITNESS: Okay, thank you. 28 SIR MARTIN MOORE-BICK: Is that all right? 29 A Yes, 20 Page 1 20 A Yes, 21 A Yes, 22 That report addresses your preliminary Phase 1 report dated 23 May, and you have updated that treport in a arevised version dated 21 October 2018, and also with 9 a revised version dated 21 October 2018, and also with 9 an accompanying two-page addendum document dated 10 October; is that right? 21 A Yes, 22 A Yes, 23 A Yes, that's correct. 24 A Yes, 25 Posser and on the exterior of Grenfell Tower; that's right, yes? 26 A Jose Luis Torero Gullen. 27 Q. That report addresses your preliminary conclusions on the liquition of the Grenfell Tower; that's right, yes? 28 A Yes, that's correct. 29 Lis will address forensic fire and smoke spread throughout Grenfell Tower; that's right, yes? 30 A Yes, that's correct. 31 Q. In 2008, you were awarded the Arhur B Guise Medal by the Society of Fire Protection Engineering at the University of Queensland in Australia between 2012 and 2017; is that correct? 31 Q. And you also held the BRE Trust/Royal Academy of Engineering at the University of Edinburgh between 2004 and 2011. 32 A. Yes. 33 Legisland of the School of Civil Engineering at the University of Queensland in Australia between 2012 and 2017; is that correct? 4 Q. Before moving to Australia, you held the Landolt & Cochair for innovation for a sustainable futur				
14 So If Lea more call Professor Foren. 15 SIR MARTIN MOORE-BICK: Thank you, yes. 16 PROFESSOR JOSE LIUS TORERO (affirmed) 17 Questions by MS GRANGE 18 SIR MARTIN MOORE-BICK: Thank you very much, professor. Sit 19 down and make yourself confortable. 20 Ms Grange, before you start, I'm sure the professor 21 is well used to delivering lectures and other material 22 for quite extended periods, but I think we should have 23 a break during the middle of the morning. I think 24 possibly one break will be sufficient, unless you. 25 professor, indicate that you would like one at any other 26 A. Jose Luis Torero Cullen. 27 THE WITNESS: Okay, thank you. 28 Please would you give the inquiry your name? 29 A. Yes. 20 A. Yes, that's correct. 20 Page 3 1 stage. If you do, of course let me know, 21 THE WITNESS: Okay, thank you. 22 The WITNESS: Okay, thank you used the professor of civil engineering at the University of Maryland in the USA; is that correct? 29 Page 3 20 A. Yes, 21 Page 3 22 Possibly one beask will be sufficient, unless you. 23 Page 1 24 Stage. If you do, of course let me know, 25 THE WITNESS: Okay, thank you. 26 Please would you give the inquiry your name? 27 A. Jose Luis Torero Cullen. 28 Please would you give the inquiry a preliminary Phase 1 report dated 23 May, and you have updated that report in a revised version dated 21 October; 918, and 180 with an a revised version dated 21 October; 918, and 180 with an a revised version dated 21 October; 918, and 180 with an a revised version dated 21 October 2018, and also with an a revised version dated 21 October 2018, and also with an a revised version dated 21 October 2018, and also with an a revised version dated 21 October 2018, and also with an a revised version dated 21 October 2018, and also with an accompanying two-page addendum document dated 20 October; is that right? 21 A. Yes. 22 A. Yes. 23 Q. That report addresses your preliminary conclusions on the ignition of the Grenfell Tower facade materials; fire spread to and on the exterior of Grenfell Tow		•		
15 SIR MARTIN MOORE-BICK: Thank you, yes, 16 PROFESSOR JOSE LUIS TORERO (affirmed) 17 Questions by MS GRANGE 18 SIR MARTIN MOORE-BICK: Thank you very much, professor. Sit 19 down and make yourself confortable. 19 Ms Grangs, before you start, I'm sure the professor 20 Ms Grangs, before you start, I'm sure the professor 21 is well used to delivering lectures and other material 22 for quite extended periods, but I think we should have 23 a break during the middle of the morning. I think 23 a break during the middle of the morning. I think 24 possibly one break will be sufficient, unless you. 25 professor, indicate that you would like one at any other 25 morning and the director of the Center for Disaster Resilience at the Department of Grid Engineering, and the director of the Center for Disaster Resilience at the Department of Grid Engineering, and the director of the Center for Disaster Resilience at the Department of Grid Engineering at the University of Maryland in the USA; is that correct? 1 stage. If you do, of course let me know. 2 THE WITNESS: Okay, thank you. 3 SIR MARTIN MOORE-BICK: Is that all right? 4 MS GRANGE: Yes, absolutely. Thank you. 4 Please would you give the inquiry your name? 5 A. Jose Luis Torero Cullen. 6 A. Jose Luis Torero Cullen. 7 Q. You have provided to the inquiry a preliminary Phase 1 report dated 23 May, and you have updated that report in a revised version dated 21 October 2018, and also with an accompanying two-page addendum document dated 12 October; is that right? 4 A. Yes. 12 Q. A. Yes. 13 Q. That report addresses your preliminary conclusions on the ignition of the Grenfell Tower facade materials; fire spread to and on the exterior of Grenfell Tower; and fire and smoke spread within Grenfell Tower; that's correct. 19 Q. It's important to note that you have also been instructed to provide a further report at Phase 2 which will address forensic fire and smoke spread throughout Grenfell Tower; the correlation between the fire safety strategy for 24 Grenfell Tower, and various asp		-		
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1	Q. You have been involved in numerous fire investigations,	1	Q. At page 17 of your report, you've explained that the
2	many of which have been landmark studies.	2	main characteristic that defines a high-rise building is
3	A. Yes.	3	what you call a convergence of timescales.
4	Q. Between 2001 and 2010, you were involved in	4	A. Yes.
5	an independent investigation of the World Trade Center	5	Q. Can you just explain for us what you mean by that?
6	buildings 1 and 2 collapses.	6	A. Yes. There are several factors that happen when you
7	A. Yes.	7	have a fire. Fire is unusual in the sense that it's one
8	Q. You have conducted a cause and origin investigation into	8	of the few hazards that actually evolves in space and
9	the Texas City explosion at subsequent fires, as well as	9	time. So it is going to grow as a function of time and
10	a damage correlation exercise.	10	it can grow slower or faster.
11	A. Yes.	11	Normally, for example, if you were to have
12	Q. You conducted dispersion fire modelling supporting the	12	a low-rise building, egress time, so the time that it
13	litigation relevant to the Buncefield explosion and the	13	takes for people to get out, is extremely fast. So,
14	Sego mine explosion in the USA.	14	effectively, that is an independent timescale. In
15	A. Yes, that's correct.	15	a few minutes, you will get everybody out, while the
16	Q. You conducted a post-fire structural assessment of the	16	fire can take half an hour or an hour to grow. In
17	Abu Dhabi Plaza fire in Kazakhstan, probably the biggest	17	a similar manner, the structure is going to take
18	ever fire of a building under construction; is that	18	a significant time to heat up.
19	correct?	19	So you can separate the timescales and basically get
20	A. Yes, that's correct.	20	the life safety aspects of the building taken care of in
21	Q. You've been awarded a number of prizes in this field for	21	a few minutes, while everything else has a different
22	your writing. I just want to pick out one.	22	timescale.
23	You have, together with your co-authors, been	23	Now, in the case of a tall building, that is not
24	awarded the FM Global Best Paper Award for a paper on	24	possible because you have multiple levels, so it will
25	the precision of fire models and the required skills for	25	normally take a very significant period of time for
	1		
	Page 5		Page 7
		1	
1	fire modelling; is that correct?	1	neonle to be able to descend through those levels
1	fire modelling; is that correct?	1 2	people to be able to descend through those levels.
2	A. Yes, that's correct.	2	Therefore, the number of minutes that it will take to
2	A. Yes, that's correct. Q. Thank you.	3	Therefore, the number of minutes that it will take to address the life safety issues of people can be well
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1 a structure to fail, a door to fail, a window to crack; 2 you would expect people to be out of those spaces before 3 that.

In a similar manner, we have pre-specified required times for the fire service to arrive on site. Depending on which country and which jurisdiction you have, that will be a few minutes, 5 minutes, 6 minutes. Therefore, all life safety aspects of the building in principle would have been taken care of before the firefighters arrive or before anything has failed. So people will be out of the building and they will be safe before any of these things happen.

In a tall building, because it takes much longer for people to arrive[sic], you would expect that the firefighters would have arrived on scene before everybody is out of the building, and you would have expected that before everybody is out of the building, some components of the building will already be experiencing some element of distress or failure.

- Q. Can you explain the significance of that convergence of timescales for a high-rise strategy? Does it mean, for example, that you need safe areas to exist in the building?
- A. Yes. Because you cannot take everybody out in such a short period of time that they are not being affected

for a very long period of time. There's very
significant uncertainty on human behaviour. So the
timescales are very difficult to predict, so it's very
difficult to calculate how long a person would be within
building.
There have been cases, for example, like the first

There have been cases, for example, like the first bombing of the World Trade Center, where effectively people were inside the stairs for many hours, and so we have to make provisions to protect those areas in such a way that they remain viable for as long as it is necessary. And because "as long as it's necessary" is not very well defined, you know, we have to make that almost a permanent feature of the building.

Q. You talk about redundancies being necessary for all safety systems, and you explain also that lobbies are typical of redundancies built into a fire safety strategy.

Can you explain why those redundancies are so important? You probably just explained that, but with reference to lobbies as well as stairs.

A. Yes. Every time you design a safety system, safety systems are not perfect, and there will always be a probability of failure. So you cannot rely on a single safety system to protect the lives of people. So what you do is you always introduce multiple levels

Page 9

by the fire itself. People are going to be in the building while certain areas of the building are already going to be fully compromised.

So you can have a fire that starts, like in the case of Grenfell, in the kitchen, and that fire has already fully compromised the kitchen before people have had enough time to be able to get out of the building.

So a way in which we address the problem is we sectorise the building and we create safe areas. So what we are considering as our time to egress is the time that it takes not to get out of the building, but the time that it takes to enter a place that is considered to be a safe place.

So by creating the sectors and separating the building in different components, we are allowing certain parts of the building to be fully compromised, while other parts of the building remain perfectly safe, so people can actually be in those parts while the building is being affected by the fire.

- Q. You say in your report that the most common safe areas are the stairwells. You also say that there's no limit to the time that stairwells need to remain safe. Can you just expand on that?
- A. Yes, because in a high-rise you're going to have a situation in which people are going to be evacuating

Page 11

of redundancy until you're satisfied that the overall probability of the entire chain is so low that you can almost guarantee the safety of people.

So depending on the complexity of the system, you will introduce more levels of redundancy. If a system is very simple, you might need just two levels of redundancies, but if a system is very complex, for example if you're dealing with a nuclear power plant, you will have multiple levels of redundancy to make sure that the system doesn't fail.

So as a common practice in any matter of safety, we will always introduce to all safety systems levels of redundancy to make sure that in case something doesn't work, there is something else to cover for us.

Q. In your report in general, what you've done is you've broken down the substance of that report into four seminal stages in the progress of the fire at Grenfell Tower. You say that these four stages are where distinctive interactions between the fire, the building, its occupants and the Fire Brigade were observed.

I'm just going to establish what these four stages are at this stage.

So stage 1 is initiation of the fire event through to breach of the compartment of origin, which is

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1 redundancies that we have in the building have provided 1 approximately 00.54 am to 1.05 am. 2 2 Stage 2 is from the breaching of that compartment of of enabling people to actually migrate out of the 3 3 origin to the point where the fire reaches the top of building. 4 the building on the east face, approximately 1.05 am to 4 By the time you get to the third stage of the 5 5 1.30 am. building, the process becomes a very dynamic process, in 6 Stage 3 you characterise as lateral fire spread and 6 which effectively we have sufficient evidence that the 7 7 internal migration of the fire and smoke, until the full means of egress have been compromised. 8 compromise of the interior of the building, including 8 Now, the fact that they are compromised doesn't 9 the stairs. Again, that's approximately 1.30 am to necessarily mean that people cannot get into those means 10 10 of egress and successfully get out; all that it means is 2.30 am. 11 Stage 4 is what you describe as the untenable stage, 11 that there is significant evidence that there is 12 12 where significant parts of the building are untenable. a deterrent for people to do so, in the sense that there 13 We'll come back to this. Approximately 2.30 am until 13 will be smoke in many ways, people will be identifying 14 14 extinction is the untenable stage. smoke. 15 As I say, we're going to come back to each of those 15 So, effectively, the means of egress are not acting the way they should be acting, so we have fundamentally 16 stages in detail during your evidence, but at this 16 breached all levels of redundancy and we have reached to 17 stage, can you just explain why you have chosen to 17 18 divide the fire into those four stages in your report? 18 the core of the safe area of the building. 19 A. Yes. I mean, beyond just trying to keep a little bit of 19 Now, the final stage of the fire is when there is 20 order to all this information, I think the different 20 a generalised perception that that core safety area of 21 stages have very distinct characteristics that are quite 21 the building has been lost and, therefore, there is very 22 fundamental to the behaviour of a building. Therefore, 22 little evidence that people can actually use the means 23 23 I believed it was very important to separate those. of egress to exit the building. 24 The first stage is, to me, fundamental, because as 24 Q. Let's start, then, and look in detail at stage 1, which 25 25 I explained in my report, at the backbone of the fire is the breach of that first compartment. We've got this Page 13 Page 15 safety strategy is the concept of no spread, external 1 time frame of 00.54 through to roughly 1.05 am. 1 2 2 At section 3.1 of your report, you've explained that spread, of the fire, 3 3 you have conducted a simple modelling analysis, what you So we make this assumption that the fire will be 4 4 describe as a "simple first principles elimination boxed in within one floor, and on the basis of boxing in 5 the fire within one floor -- even beyond that, within 5 analysis" of the fire scenario in the compartment of 6 one unit -- we make this assumption that the fire is 6 origin; is that correct? 7 7 boxed in, and on the basis of that, we construct the 8 8 Q. You say that you've done this to "bound the actual fire whole fire safety strategy. g 9 So the primary assumption behind every component of scenario within the kitchen more precisely". Can you 10 the fire safety strategy remains this concept of having 10 explain what you mean by "bound the actual fire 11 the fire boxed in within one unit. 11 scenario"? 12 12 So that initial stage represents the period where A. Yes. I think one of the things that is always very 13 the building is actually behaving as designed, where 13 important to try to establish is if this event was 14 14 effectively the fire is boxed in within the unit and it outside the expected conditions that the building was 15 has not managed to come out and penetrate other units 15 designed for. So if you are in a housing complex, there 16 within the building. 16 are certain fire events that we accept as being events 17 17 So that particular stage effectively represents the that are a regular occurrence, what I call in my report 18 18 building operating as designed. an event of probability of 1. 19 The second stage, again, it is fundamental in the 19 Now, people sometimes believe that fire is a rare 20 sense that the building is now not operating as 20 event, and actually fires are not rare events; fires 21 designed. Nevertheless, within that process of vertical 21 occur very regularly. What happens is generally we have 22 flame spread, which is quite rapid, there is no 22 put so many provisions to try to protect us from fire 23 23 significant evidence that the means of egress in the that what becomes a rare event is an event of a 24 building have been severely compromised. 24 magnitude that is sufficient to actually affect people 25 25 So, effectively, there is still the ability that the or affect the building in a significant way. Page 14 Page 16

1 So we have all these provisions and we design these basically meant that there was no attainment of 2 2 provisions to be able to cope with certain scenarios, flashover. 3 3 and those scenarios are considered to be the common So given that we have that evidence, that is our key 4 4 piece of evidence and we can go back and try to then put 5 5 So the first thing that I was trying to establish is as much fuel as we can and as small fuel as we can given 6 given the evidence that we have, and the actual nature 6 the typical fuels that you have in there, and see when 7 7 of the evidence that we have that is quite coarse -- and it stops having enough oxygen. Effectively, the smoke 8 this is quite common to a reconstruction of a fire, that 8 has descended to the floor and the oxygen is prevented 9 9 you are working from debris, so it's very difficult to from reaching the fire and, therefore, the fire cannot 10 get detailed information of everything that was 10 continue to increase, not because the fuel is not there 11 happening in the space. So what we're aiming at is to 11 but because the oxygen is not getting there. 12 12 try to look and see if the fires that created the By doing that, we can ascertain that the fire that 13 situation were of a nature that was extraordinary. 13 actually was occurring in that space was somewhere 14 Now, by doing this very small bounding analysis, 14 between 60 and 300 kilowatts. 15 which is we took the worse possible fire growth, the 15 Q. I am going to come to that. 16 16 slowest possible fire growth and we applied it into the So in your simple modelling that you've done in the 17 17 kitchen. The kitchen has a very small floor plan, so main body of your report, just to be clear what the 18 effectively it is very rapidly filled up with smoke. 18 parameters are for that simple model, you've assumed 19 For a fire to burn, you need fuel and you need oxygen. 19 that all windows and doors to the kitchen were closed, 20 20 So lack of either of the two of them will actually stop and you've plotted different fire scenarios, the size of 21 the fire. 21 the fire and its heat release rate. We see that 22 22 Now, if the fire gets strong enough, then what reference, HRR, heat release rate. 23 23 Can you explain what a heat release rate is? happens is that the temperature of the smoke gets so hot 24 that the fire follows this process that is called 24 A. Yes. So the heat release rate is the actual energy that 25 25 flashover. So, effectively, everything within the is being released by the fire. Page 17 Page 19 1 compartment ignites and effectively the fire flashes 1 Q. As you said, you've looked at fire growth and you've 2 2 classified the fire as either slow, medium, fast or 3 3 ultrafast. So what we had observed was that in the particular 4 4 kitchen of Grenfell Tower, the fire had never reached Are those general classifications that are routinely 5 flashover. So, effectively, what happened was that at 5 used in fire modelling? 6 some point during the growth of the fire, the fire 6 A. Yes. Those are classifications used mostly for design, 7 7 and, therefore, they are the classic classifications we either was lacking fuel or it was lacking oxygen in such 8 a way that it could not get to temperatures that were 8 will use to test our design. q 9 high enough to bring the room to flashover. So it's what we normally will use as a reference to 10 Q. Pausing there, what would you have expected to see in 10 try to bound the fire. So a slow fire will be as slow 11 a flashover event that we didn't see in the kitchen of 11 as possible and an ultrafast as fast as possible. 12 12 Q. They're your two extremes? 13 A. So in a flashover event, every combustible material 13 A. Extremes. 14 14 would have ignited, because there is enough heat coming Q. Is it right your simple model also assumes that the fire 15 from the smoke to bring them to ignition. So what you 15 is in the middle of the room? 16 would get is effectively the full destruction of all the 16 A. Well, the kind of model that we're doing, it doesn't 17 17 components. make any difference where the fire is. It basically 18 18 Now, you can see, for example, in Grenfell, there treats the problem in a way such that it doesn't really 19 are appliances, for example, on which the paint remains 19 matter where you put the fire. The reason for that is 20 undamaged. So the fact that the paint remains 20 that in a small compartment of that nature, the impact 21 21 of the fire will effectively affect the entire undamaged, that means the fire did not reach flashover 22 because the paint would have blistered and ignited. 22 compartment almost simultaneously, so it really doesn't 23 So, effectively, there's sufficient evidence within 23 matter where you put the fire. 24 the space of elements that were in sufficient proximity 24 Q. Let's go to one of your figures which help illustrate 25 25 that actually were not ignited by the fire, which this. Can we go to your figure 6. We have a new

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1	reference for this document because it didn't appear as	1	corresponds to a hot layer of approximately 220 degrees;
2	clearly as we'd like in your report.	2	is that right?
3	Can we go to JTOS0000003, please, on the screen.	3	A. Yes.
4	Can we zoom in on the top diagram, please.	4	Q. In contrast with the slow fire growth, that results in
5	Just to be clear, unfortunately in the PDF of your	5	a peak heat release rate of approximately 60 kilowatts
6	report that we released, the grey smoke layer wasn't	6	and a hot layer temperature of approximately 110 degrees
7	very clear.	7	centigrade; is that correct?
8	Can you just explain what this basic model is	8	A. Yes.
9	showing?	9	Q. So you've put your fire in the size range 60 to
10	A. Yes. So basically that shows a little bit of	10	300 kilowatts in terms of heat release rate on your
11	a schematic of the model that we presented. Basically	11	simple modelling?
12	what it shows is an upper smoke layer in grey, which	12	A. Yes.
13	will be basically a homogeneous layer that represents	13	Q. Is that a small or a large fire?
14	the smoke, then in the bottom you have the air.	14	A. So a 60-kilowatt fire will be no bigger than
15	So the fire acts as a pump; it basically takes fresh	15	a waste-paper basket. A 300-kilowatt fire will be about
16	air and sends smoke to the top. That is called	16	half a chair. So in both cases, those will be fires
17	-	17	· · · · · · · · · · · · · · · · · · ·
	a two-zone model and it's the most simple representation		that we will expect to be below our typical design
18 19	that we have as a tool, as a regularly used tool, of	18	values. So these are the kinds of fires you will expect
	a fire.	19	we will regularly have in a house and building and,
20	Q. If we now go to figure 7, which if we can pull up	20	therefore, the building has to respond appropriately to
21	JT0S0000001 at page 39.	21	these fires.
22	If we can zoom in on the graph at the top, please,	22	Q. You say on page 39 of your report that you've used
23	figure 7.	23	a computation zone modelling tool which enables you to
24	This explains the results of your simple	24	look at different fire scenarios in your analysis; is
25	modelling	25	that right?
	Page 21		Page 23
1	A. Yes.	1	A. Yes.
1 2	Q in basic terms; is that correct?	1 2	A. Yes. Q. That's a computer modelling tool developed in the USA;
2	Q in basic terms; is that correct?	2	Q. That's a computer modelling tool developed in the USA;
2 3	Q in basic terms; is that correct?A. Yes.	2 3	Q. That's a computer modelling tool developed in the USA; is that correct?
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2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	 Q. — in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example — I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	 Q in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will touch the floor and the fire will stop growing at that 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts. Q. What you've said about that very basic modelling is it
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	 Q. — in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example — I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will touch the floor and the fire will stop growing at that point when the temperatures reach slightly above 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts. Q. What you've said about that very basic modelling is it confirms that the kitchen door was probably closed
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	 Q. — in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example — I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will touch the floor and the fire will stop growing at that point when the temperatures reach slightly above 100 degrees. 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts. Q. What you've said about that very basic modelling is it confirms that the kitchen door was probably closed during the early stages of the fire; is that correct?
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	 Q. — in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example — I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will touch the floor and the fire will stop growing at that point when the temperatures reach slightly above 100 degrees. Q. So in this very simple model, we have a peak heat	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts. Q. What you've said about that very basic modelling is it confirms that the kitchen door was probably closed during the early stages of the fire; is that correct? A. Yes.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	 Q. — in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example — I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will touch the floor and the fire will stop growing at that point when the temperatures reach slightly above 100 degrees. Q. So in this very simple model, we have a peak heat release rate before smoke filled the kitchen during the	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts. Q. What you've said about that very basic modelling is it confirms that the kitchen door was probably closed during the early stages of the fire; is that correct? A. Yes. Q. Just turning then to appendix B of your revised report,
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	 Q. — in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example — I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will touch the floor and the fire will stop growing at that point when the temperatures reach slightly above 100 degrees. Q. So in this very simple model, we have a peak heat	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts. Q. What you've said about that very basic modelling is it confirms that the kitchen door was probably closed during the early stages of the fire; is that correct? A. Yes.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	 Q. — in basic terms; is that correct? A. Yes. Q. Can you talk us through what we see here? A. Yes. Basically what you get is the temperature of the smoke on the vertical axis and you get the time on the horizontal axis. The red curve shows the evolution of the temperature of the smoke as a function of time. So as you see, because that is the ultrafast fire, the temperature will grow faster. By the time it reaches, in this particular example — I need to clarify that we ran this model multiple times under different conditions. So in this particular example, the smoke will reach the floor and the fire will stop growing at a temperature of about 230 degrees. In the other extreme will be the case of the slow growth fire. What you can see is the temperatures are growing much, much slower, and the smoke layer will touch the floor and the fire will stop growing at that point when the temperatures reach slightly above 100 degrees. Q. So in this very simple model, we have a peak heat release rate before smoke filled the kitchen during the	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	 Q. That's a computer modelling tool developed in the USA; is that correct? A. Yes, it's a computer model developed by the National Institute of Standards and Technology and CFAST. Q. CFAST. A. Yes. Q. You say this enabled you, for example, to model the fire including with an open kitchen door. A. Yes. Q. You say that the results of that show that if the door was open, the smoke layer will exit the kitchen, allowing the fire to grow because of the oxygen, resulting in higher temperatures and a flashover; is that correct? A. Yes. Q. Is it right that the heat release rate necessary to deliver that flashover was around 1,000 kilowatts? A. Yes, it would be approximately 1,000 kilowatts. Q. What you've said about that very basic modelling is it confirms that the kitchen door was probably closed during the early stages of the fire; is that correct? A. Yes. Q. Just turning then to appendix B of your revised report,

1	provided some more detail of the additional modelling	1	The computational fluid dynamics model, it was
2	work that you have done?	2	developed by the same organisation, the National
3	A. Yes.	3	Institute of Standards and Technology, and it's called
4	Q. Is it right that you've expanded appendix B in your most	4	the Fire Dynamics Simulator. Effectively what it does
5	recent report served in October compared with what we	5	is breaks the room into slightly little cubes. So
6	saw in May?	6	instead of having two big layers, what you have is
7	A. Yes.	7	thousands of little cubes, and you're basically
8	Q. In general, can you just explain in very general terms	8	modelling every little cube. So you can resolve in
9	what you've sought to do in appendix B?	9	every position of the room what the temperature is going
10	A. Yes. I think one of the very important aspects of	10	to be, and basically the heat release rate and the flows
11	an analysis of this nature is to be able to use the tool	11	and all the details.
12	that is appropriate for the precision of the input	12	So it's just simply a higher spatial resolution so
13	elements that we have.	13	you can see what is happening in every point.
14	So we have some information from the scene, we have	14	Q. Is what we see in appendix B the same as a sensitivity
15	some information from videos, and on the basis of that,	15	analysis?
16	we have to use a model that has a consistent level of	16	A. It's beyond a sensitivity analysis, because
17	precision.	17	a sensitivity analysis, normally what it is, is you take
18	If we use a model that is more precise, effectively	18	the input parameters that you put in and you vary them
19	what we're doing is giving a false sense of precision.	19	through a certain percentage, just to make sure your
20	So we have to stick to a model that is of adequate or	20	inputs are correct.
21	comparable level of precision to the information that we	21	Here we're trying to test also the physics. By
22	have. So the simple model is that.	22	using a much more sophisticated physics with the same
23	Now, what I do is to gain confidence on my simple	23	inputs, we're trying to make sure that, actually, the
24	model, I use more sophisticated tools to inform me and	24	simple model is delivering the right answers to the
25	run a whole bunch of other different scenarios, all	25	questions that we want to answer.
	D 05		D 07
	Page 25		Page 27
1	different characteristics, try to play with different	1	
1 2	different characteristics, try to play with different variables that are enabled by a more sophisticated	1 2	Q. So let's just start with the computation zone modelling that you've carried out.
	· · · · · · · · · · · · · · · · · · ·		Q. So let's just start with the computation zone modelling
2	variables that are enabled by a more sophisticated	2	Q. So let's just start with the computation zone modelling that you've carried out.
2 3	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided	2 3	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model
2 3 4	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct.	2 3 4	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific
2 3 4 5	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B	2 3 4 5	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation
2 3 4 5 6	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the	2 3 4 5 6	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example
2 3 4 5 6 7	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model.	2 3 4 5 6 7	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and
2 3 4 5 6 7 8	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model. Q. You've explained that you've done two different forms of	2 3 4 5 6 7 8	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and then, secondly, exploring other scenarios, for example
2 3 4 5 6 7 8	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model. Q. You've explained that you've done two different forms of modelling: you've done the computation zone modelling,	2 3 4 5 6 7 8 9	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and then, secondly, exploring other scenarios, for example kitchen door open or closed or other windows open.
2 3 4 5 6 7 8 9	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model. Q. You've explained that you've done two different forms of modelling: you've done the computation zone modelling, the CFAST modelling you just talked about	2 3 4 5 6 7 8 9 10 11 12	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and then, secondly, exploring other scenarios, for example kitchen door open or closed or other windows open. Before we discuss the results of those models,
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2 3 4 5 6 7 8 9 10 11	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model. Q. You've explained that you've done two different forms of modelling: you've done the computation zone modelling, the CFAST modelling you just talked about A. Yes. Q and you've also done something called computational	2 3 4 5 6 7 8 9 10 11 12 13 14	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and then, secondly, exploring other scenarios, for example kitchen door open or closed or other windows open. Before we discuss the results of those models, I just want to remind ourselves what the kitchen window looked like in flat 16 because I think that's helpful to remind ourselves of that. Can we go to one of the figures in Dr Lane's report.
2 3 4 5 6 7 8 9 10 11 12 13 14 15	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model. Q. You've explained that you've done two different forms of modelling: you've done the computation zone modelling, the CFAST modelling you just talked about A. Yes. Q and you've also done something called computational fluid dynamics, or CFD, modelling using a simulator.	2 3 4 5 6 7 8 9 10 11 12 13 14 15	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and then, secondly, exploring other scenarios, for example kitchen door open or closed or other windows open. Before we discuss the results of those models, I just want to remind ourselves what the kitchen window looked like in flat 16 because I think that's helpful to remind ourselves of that. Can we go to one of the figures in Dr Lane's report. That's BLAS0000008 at page 23.
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2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model. Q. You've explained that you've done two different forms of modelling: you've done the computation zone modelling, the CFAST modelling you just talked about A. Yes. Q and you've also done something called computational fluid dynamics, or CFD, modelling using a simulator. Can you just explain the difference between the two and what that is?	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and then, secondly, exploring other scenarios, for example kitchen door open or closed or other windows open. Before we discuss the results of those models, I just want to remind ourselves what the kitchen window looked like in flat 16 because I think that's helpful to remind ourselves of that. Can we go to one of the figures in Dr Lane's report. That's BLAS0000008 at page 23. Thank you. I think this is the kitchen window. I believe it's
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	variables that are enabled by a more sophisticated model, just to make sure that the answers I provided with my simple model are correct. So, effectively, this whole exercise of appendix B is a mechanism to gain confidence on the validity of the simple model. Q. You've explained that you've done two different forms of modelling: you've done the computation zone modelling, the CFAST modelling you just talked about A. Yes. Q and you've also done something called computational fluid dynamics, or CFD, modelling using a simulator. Can you just explain the difference between the two and what that is? A. Yes. So the simple model that I use effectively uses two layers, so it has a hot layer and a cold layer and it has no opening, so effectively you're just filling	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Q. So let's just start with the computation zone modelling that you've carried out. You've explained in appendix B that two zone model variations have been used for this more specific analysis: first, trying to model the assumed ventilation conditions based on the available evidence, for example kitchen door closed, main window partially open; and then, secondly, exploring other scenarios, for example kitchen door open or closed or other windows open. Before we discuss the results of those models, I just want to remind ourselves what the kitchen window looked like in flat 16 because I think that's helpful to remind ourselves of that. Can we go to one of the figures in Dr Lane's report. That's BLAS0000008 at page 23. Thank you. I think this is the kitchen window. I believe it's in flat 13 on the opposite side, but can you confirm
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1	A. So that window could open tilted inwards or open	1	A. Yes.
2	completely, so	2	Q. Can you explain why you've done that?
3	Q. Swinging in or tilting in?	3	A. The dynamics of the fire are very different if you have
4	A. Yes.	4	a fire that is on the floor then if you have one that is
5	Q. How about the little window underneath the kitchen	5	progressing behind an obstacle. When you have a fire
6	extractor fan?	6	that is progressing behind an obstacle, you will
7	A. I believe it can only swing open.	7	restrain the amount of air that can get into the fire,
8	Q. So when you talk about looking at different modelling,	8	so the flames will be longer, because the fuel requires
9	different scenarios of different windows open, we're	9	to get air from higher points to be able to be fully
10	talking about these windows here?	10	consumed, while if you put it in the middle, the flames
11	A. Exactly.	11	will be shorter because you have air coming from all
12	Q. Thank you.	12	directions. So you have to model both extremes.
13	In terms of your modelling, for scenario 1, which is	13	In the simple model, we only model the one in the
14	the assumed ventilation conditions based on the existing	14	middle because we were looking for the smaller possible
15	evidence, which is kitchen door closed, large window	15	fire because we were bounding the conditions. But in
16	partially open, what you've said is that your more	16	here we tried both, just to make sure that we covered
17	sophisticated modelling shows that the heat release rate	17	both potential scenarios.
18	is in the range 110 to 360 kilowatts; is that right?	18	Q. You say that you've modelled several ventilation
19	A. Yes.	19	conditions in terms of the windows being open or shut.
20	Q. You say that compares well with the your simple model of	20	In terms of the fire size for the fridge, is it
21	60 to 300 kilowatts?	21	right that you've used results from some of the
22	A. Yes.	22	stand-alone tests carried out by the BRE for the
23	Q. In scenario 2, you say that the extra ventilation from	23	Metropolitan Police to estimate the potential heat
24	the open door means a flashover scenario with a peak	24	release rate for the fridge?
25	heat release rate of 1.5 megawatts; is that correct?	25	A. Yes.
	Page 29		Page 31
1	A Voc	1 1	O So what happened as Lunderstand it is that the
1	A. Yes. O. Turning then to the computational fluid dynamics. You	1 2	Q. So what happened, as I understand it, is that the
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1 range you've used for your simple model. Can you just	1 A. Yes. So this type of model, because it's modelling
2 explain that?	2 things in a lot more detail, it allows you to see really
3 A. Yes. So the tests conducted by BRE were conducted under	3 how much energy is being released. So it's taking into
4 a hood, so you're basically allowing for all the oxygen	4 account how much air is meeting with the fuel and how
5 that is necessary to reach the fire. So this will be	5 much energy really is releasing.
6 the maximum burning capacity of the refrigerator,	6 So I can input energy, but I can measure also the
7 without considering the fact that oxygen might not get	7 output. So effectively what this model does is whatever
8 there, like will happen in a compartment.	8 cannot burn, then it's left as unburned smoke that just
9 So if you look at the timeline of about 7 minutes	9 goes away and I can actually account for that.
10 until reaching 400, that is fairly consistent with	10 So effectively with the model, I can tell that no
11 somewhere in between a slow and an ultrafast. So it	11 matter how much energy I put in, only 400 burns. I can
12 falls more or less in between the range of values that	12 put 1,000, I can put 500, and it will immediately go
13 we worked with.	back down and only 400 will burn.
14 We observed also that the smoke layer descended in	14 So effectively it verifies that you are oxygen
15 less than 5 minutes. So, effectively, you will not	15 starved, so you cannot burn more because you don't have
16 reach to 400 kilowatts; you will probably stop a little	16 enough air getting into the fire.
17 bit earlier because the smoke would've gone down.	17 Q. You've also said in your appendix B that your 60 to
18 That's more or less what the results show, that	18 300-kilowatt simple model gave a good estimate of
19 effectively the fire stops growing because there is not	19 average compartment temperatures, but that only the CFD
20 enough air being able to feed the fire.	20 model can establish something called the spatial
So, in many ways, using this as an input is quite	21 distribution.
22 effective in trying to compare it with the simple model	22 Can you explain what spatial distribution is?
23 to show that, effectively, all the numbers are within	23 A. Yes. Because in the CFD we are modelling the small
24 the same ranges that we were operating.	24 little cubes that fill up the entire compartment, each
25 Q. So that explains why you haven't gone back in your main	25 cube will have a temperature. So I can know exactly
Page 33	Page 35
1 report and adjusted your range of 60 to 300 to make it	1 what the temperature is in that point. So spatially, in
2 60 to 400.	2 all the directions, I can know exactly what the
3 A. Absolutely. Again, I go back to the fact that we need	3 temperature is.
4 to use the right tool for the right problem. So I do	4 In the other models, I'm assuming that the hot
5 not want to, with my report, make anybody think that we	5 layer, the smoke, is only one temperature and the cold
6 have more precision than the precision that the simple	6 layer is only one temperature. So I only have two
7 model has.	7 numbers and I don't have the spatial distribution in the
8 Q. So turning, then, to the results of your CFD model, you	8 compartment.
9 say that the results from that model for a fire located	9 O. You've also said that your CFD model delivers more
in the back of the fridge, and with the large window	10 accentuated temperatures. Can you explain what you mean
tilted open, the small window open but the door closed,	by accentuated temperatures?
show that temperature magnitudes both by the window and	12 A. I think the easiest way to describe it is to look at
by the door are within the bounds of the predictions in	13 Q. Figure 91, I think.
the simple model; is that correct?	14 A figure 91, yes.
15 A. That's correct.	15 Q. If we go JTOS0000001, at page 149.
Q. You've also run the same analysis, but with a higher	16 Can you just explain it by reference to this figure?
heat release rate, just to check the figures	17 A. Yes. So as you can see, the dotted line represents the
18 A. Yes.	simple model, and effectively gives you the same
19 Q at 400 to 500 kilowatts; is that right?	19 temperature all along the height, because the whole
20 A. Yes.	20 smoke layer has the same temperature.
21 Q. You say again that for a fire located in the back of the	21 The CFD will show that the temperatures are slightly
fridge, and with the large window open, small window	22 lower at the bottom and slightly hotter at the top, and
23 open but the door closed, the model managed to maintain	23 therefore gives you the distribution with height of the
24 the 400-kilowatt level, but it didn't maintain the	24 temperature.
25 500-kilowatt level. Can you just explain that?	Now, one of the things that I need to clarify in
D. O.	D 24
Page 34	Page 36

there is that while it shows this accentuated 1 1 Because remember, we're bounding. All we're doing is 2 2 temperatures and it shows that it's obviously going to trying to find what are the fires that effectively could 3 3 be hotter at the top and colder at the bottom, we cannot do what they did. 4 rely on those numbers. 4 Q. In your simple analysis that you did in your main 5 report, it was based on a calculation from Dougal 5 So those numbers are beyond the precision of the Drysdale, which was based on a fire in an open space; is 6 information that we have. 6 7 7 that correct? So, effectively, the fact that the red curve shows 8 that you are at 300 degrees might not necessarily be 8 A. Yes. 9 Q. Do you agree that other aspects of that Drysdale paper 9 correct. At the top, you probably don't have 10 300 degrees, you might have a little bit lower, and 10 deal with fires closer to a wall or in a corner? 11 those things we will never be able to ascertain because 11 A. Yes. So, basically, if you look at Dougal Drysdale's 12 12 book, you will find he will produce different equations the precision of the information that we're inputting 13 into the model is not good enough. 13 for fires in a wall, fires around a corner, but in all 14 14 those cases, the flame will be taller. So, effectively, So being able to say that is 260, 250, is about as 15 precise as we can be. And, yes, we can see it's 15 it will be already included in my bounding analysis, I'm 16 16 plus/minus 50 degrees and that will be perfectly fine, just setting the boundary. So if I did all those 17 17 but we cannot claim that the precision of the field refinements, I will find points that are already 18 curve is actually correct. 18 included in my two limits. 19 Q. Within the CFD modelling that you've carried out, you've 19 Q. That was my next question: does your modelling take 20 20 also looked at variability by fire location, as we account of that? 21 discussed before, both at floor level and at the back of 21 A. Yes. Because, effectively, you are looking at the 22 22 the fridge freezer; is that correct? smallest possible and the biggest possible, so 23 23 everything is already -- all the in-betweens that are A. Yes. 24 Q. You've said -- I think you've mentioned this before --24 more precise are already included. 25 2.5 that a floor fire produces what you called more scatter Q. So you don't accept your simple models should've Page 37 Page 39 1 of the data. Again, can you just explain what that 1 referred to those other Drysdale calculations? 2 2 A. No, no, I mean, you know, you could do it just as 3 3 A. Yes. What happens when you put a fire in the floor is a further validation to show that they fall in between, 4 4 that the way in which the hot gases go up and they bring but the CFD model already does all that. So, 5 the cold gases in creates a situation by which the 5 effectively, if I'm already running the CFD model, there 6 flames fluctuate. You're going to have the hot gases 6 is really no point in using again simple calculations 7 7 going up, then they bring cold air, and then the flame for a situation that I have already calculated. 8 shrinks, because everything burns, then the hot gases so 8 O. You've also looked at variability in ventilation in the 9 9 up again. So you have flames that go like this, kitchen, with different windows open and closed. That 10 pulsating. 10 includes the large window in the open tilt position and 11 That creates data points that are going to change. 11 the small window open; is that correct? 12 When the flames are up, the temperature goes up; when 12 A. Yes. 13 the flames go down, the temperature goes down. 13 Q. You've said that this produces a peak heat release rate 14 14 of about 400 kilowatts, which can be sustained. But when you have a vertical fire and it's burning 15 as a wall, everything is pushing up. So effectively 15 A. Yes. 16 it's much more stable. Then what you get is fairly 16 Q. Can we just look at what you say in your report about 17 consistent temperatures at all the different heights. 17 this. It's on page 152, JT0S0000001. Can we zoom in on 18 18 Q. Does it follow from that that you accept that a fire lines 3431, to 3438. 19 located in a corner or against a wall will behave 19 So there you say: 20 differently from a fire in the middle of the room? 20 "Results presented in Figure 88 indicate that for 21 A. Oh, yes. They will behave differently. Nevertheless, 21 the large window in the tilted position and small window 22 the more you confine the fire -- so if you're behind 22 fully open ... a peak HRR of approximately 400kW can be 23 something or you're in a corner -- effectively what you 23 sustained. This means that a larger fire will result in 24 get is a taller flame. So it's the scenario that is 24 higher overall compartment temperatures as shown in

already considered when you consider the smallest fire.

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25

25

Figure 89 as there is more air available to support

combustion." 1 of a significant difference other than a slight trend 1 2 2 Again, does that mean that there's any difficulty upwards. 3 3 with your simple model of 60 to 300 kilowatts? But, effectively, given the inputs that we're 4 A. No, all that it means is that the model says that if 4 putting, I could not ascertain that even that difference 5 I put 400 -- if I open the window, the heat release rate 5 is actually that real. So normally what I will do in a plot of that nature 6 will increase a little bit. Now, the model says that is 6 7 7 is average everything, give a single plot and put 400 kilowatts, but that level of precision is not 8 granted. So all we can say is that the temperatures 8 an error bar of plus/minus 10 degrees. 9 that I gave are approximately right, but they could be Q. Just testing that, then, what about potential gaps 10 potentially slightly bigger if the window was open. 10 around the doors? So there's the sliding door to the 11 Q. Do you think it makes much difference whether it's 11 kitchen and then there's also the kitchen door itself. 12 300 kilowatts or 400 kilowatts? 12 Is it possible that the doors would not have provided 13 A. Well, it does make a difference, but when you say it 13 a complete seal, and could that have made a difference? 14 makes "much difference", I think you have to ask that 14 A. It would've been a very, very minor difference. I mean, 15 question in the context. It makes much difference for 15 generally leaks will be considered as being a much, much 16 16 what? And I think that's the important question. smaller flow rate than an open window. 17 17 So in some cases it will make a difference, and then I mean, clearly the one thing that does make a big difference is an open door, and that has to be taken 18 at that point I will have to say this model is not 18 19 sufficient to do that. But for other things, it doesn't 19 into account. But leakages are lower in the pecking 20 20 make any difference because we are way outside the order than an open window. An open window will be 21 21 a much, much more -- so if an open window can change ranges, for example. 22 22 Q. As you go on to say on the same page in the next things by 10 or 15 degrees, I would imagine that 23 23 paragraph, we have it here on the screen: leakages will not change it by 1 or 2 degrees. 24 "Models were run to analyse the difference in 24 Q. What about evidence from witnesses of draughts around 25 25 thermal profiles created by the opening of the small the windows and from under the doors post-refurbishment? Page 41 Page 43 1 Again, would you think that that could change the 1 kitchen window in addition to the tilted kitchen window 2 ... The results, shown in Figure 95, indicate that there 2 results in your modelling? 3 3 A. No. Again, it will fall way within the category of is little difference between the two, with the lower 4 ventilation resulting an only slightly higher 4 5 5 temperatures, attributable [to] the lower heat losses Q. What if the doors were not fully shut, could that affect 6 from the compartment." 6 your modelling? 7 So that's what you were just explaining. 7 A. When you say not fully shut, I mean, if you're talking 8 8 about 5 per cent, it's going to be a very, very small g 9 Q. Can we just look at that in figure 95. I think it will gap and, therefore, again, it will make no difference, 10 help to look at that. That's JTOS0000001 at page 153. 10 but if you're talking about 20/30 per cent, then of 11 Here, basically this is showing, between the 11 course, as you start opening the door, you're making 12 continuous lines and the dotted lines, the difference 12 a very significant area --13 between whether the small window is open or closed; is 13 Q. That's where you got to flashover scenarios? 14 that correct? 14 A. That's when you get to flashover. 15 A. Yes. 15 Q. What about if the extractor fan was in the "on" mode and 16 Q. So in case 1, the small window was closed, but in case 2 16 sucking air out of the kitchen? Again, could that make 17 the small window is open. 17 a difference? 18 Can you just explain why you're saying this shows 18 A. Again, it would make a slight difference. If you look 19 that there's little difference between those two 19 at the typical flow rates of an extractor fan, in 20 scenarios? 20 general they're very small compared to the types of flow 21 A. Basically, given the coarseness of the inputs that go 21 rates that you will get by smoke production or by egress 22 into this model, you will consider all those lines to be 22 of smoke out of a door. 23 the same. The way you will normally represent that is 23 So imagine what you see when you have a fire and you 24 that will be an average plus an error of about 10 to 24 open a window. You see an enormous amount of smoke 25 15 degrees on both sides. So there is really not much 25 coming out. So that is clearly much, much more than Page 42 Page 44

1	what a fan can extract.	1	A. Yes.
2	So of course all these things will make a slight	2	Q. Why have you done that?
3	difference, but it will not be a significant difference.	3	A. Because what we were testing with the CFD was
4	Q. Would you agree that if you did allow for some	4	effectively if there was enough oxygen to burn. So
5	additional ventilation, such as around the doors, and	5	there was no point in increasing the fire; you just put
6	for the possibility that the fire was not positioned in	6	it at the maximum value and see if you have enough
7	the centre of the room but was against a wall or in	7	oxygen to burn.
8	a corner, there might be local areas within the smoke	8	So many times you use different modelling strategies
9	layer, for example at ceiling level, where the fire	9	depending on what you're testing, and because in this
10	could have reached approximately 550 degrees C? Would	10	case what we were testing is do we have enough oxygen,
11	you accept that?	11	then I want to fix the fire at the maximum and see if
12	A. Yes.	12	I actually have enough oxygen, or the fire starts going
13	Q. Can you explain why you've not taken that account in	13	down on its own because it doesn't have enough oxygen to
14	your modelling, or have you taken that into account?	14	burn.
15	A. No, we have taken it into account. So, basically, we	15	Q. We're nearly finished with the modelling. Let's turn to
16	made a clear distinction between heating by means of the	16	the external spill plume temperatures.
17	smoke and heating by means of flame impingement. So	17	A. Yes.
18		18	Q. So you've done some modelling which assists in terms of
19	what you're talking about of hot-spots, localised	19	
20	heating areas, is effectively the flame in itself reaching that location and creating a hotter area within	20	what you refer to as these external spill plume
21		20	temperatures. Those are temperatures if the fire had
	the smoke layer.	21 22	vented out of the kitchen window; is that correct?
22	So the conclusion that we came up with is that the	23	A. Yes, but that's different to what I was talking about,
23	temperatures that the smoke layer can reach cannot reach	23	which is the flame impingement.
24 25	the typical ignition temperatures of most of these	25	Q. Yes. Can you explain the difference?
23	materials. But the flames, if they actually touch any	23	A. No, no, there's three things. So when you have the
	Page 45		Page 47
1	of these components, will actually reach those	1	compartment akay you're going to produce a smoke
1 2	of these components, will actually reach those	1 2	compartment, okay, you're going to produce a smoke
2	temperatures.	2	layer, so the smoke has a certain temperature.
2 3	temperatures. We did a detailed analysis of that.	2 3	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the
2 3 4	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume	2 3 4	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in
2 3 4 5	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures	2 3 4 5	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my
2 3 4 5 6	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures A. The spill	2 3 4 5 6	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my report when I discuss what I call the ceiling jet
2 3 4 5 6 7	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures A. The spill Q. I'm coming to that next, yes.	2 3 4 5 6 7	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my report when I discuss what I call the ceiling jet temperatures. So it's effectively how far the flames
2 3 4 5 6 7 8	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures A. The spill Q. I'm coming to that next, yes. Before we get to that, can you just explain why you	2 3 4 5 6 7 8	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my report when I discuss what I call the ceiling jet temperatures. So it's effectively how far the flames can reach. It's not the hot smoke temperature, it is
2 3 4 5 6 7 8	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures A. The spill Q. I'm coming to that next, yes. Before we get to that, can you just explain why you used an average smoke layer temperature in your	2 3 4 5 6 7 8 9	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my report when I discuss what I call the ceiling jet temperatures. So it's effectively how far the flames can reach. It's not the hot smoke temperature, it is the flame itself touching.
2 3 4 5 6 7 8 9	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures A. The spill Q. I'm coming to that next, yes. Before we get to that, can you just explain why you used an average smoke layer temperature in your modelling?	2 3 4 5 6 7 8 9	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my report when I discuss what I call the ceiling jet temperatures. So it's effectively how far the flames can reach. It's not the hot smoke temperature, it is the flame itself touching. Then the third one is what is happening to the
2 3 4 5 6 7 8 9 10	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures A. The spill Q. I'm coming to that next, yes. Before we get to that, can you just explain why you used an average smoke layer temperature in your modelling? A. Yes, because you have to differentiate two things: one	2 3 4 5 6 7 8 9 10	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my report when I discuss what I call the ceiling jet temperatures. So it's effectively how far the flames can reach. It's not the hot smoke temperature, it is the flame itself touching. Then the third one is what is happening to the outside, and that's the spill plume. So you have
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2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	temperatures. We did a detailed analysis of that. Q. I am coming to that. Is that about spill plume temperatures A. The spill Q. I'm coming to that next, yes. Before we get to that, can you just explain why you used an average smoke layer temperature in your modelling? A. Yes, because you have to differentiate two things: one is the smoke and one is the flame impingement. So I wanted to separate both. So if the smoke gets hot enough that it can ignite the components, that basically means any component within the room could have ignited when it enters the smoke layer. If the smoke layer cannot reach those temperatures, that basically means that only the components that were in reach of the flames could have ignited. So that allows me to establish how far the fire can be before it cannot touch any combustible material. So I'm separating the two things to make sure that I establish what is igniting what. Q. Is it also right that you've used a steady state fire in	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	layer, so the smoke has a certain temperature. Within the smoke, there will be the fire, and the fire can penetrate the smoke sometimes and get hotter in a certain region. So there's a whole section in my report when I discuss what I call the ceiling jet temperatures. So it's effectively how far the flames can reach. It's not the hot smoke temperature, it is the flame itself touching. Then the third one is what is happening to the outside, and that's the spill plume. So you have a compartment that has hot smoke and the hot smoke will come out of the compartment, mix with cold air and that will create a spill plume. Q. On the external spill plume temperatures analysis, you say that this shows that smoke temperature would only reach temperatures capable of igniting the ACP cladding if there was a large fire size with ventilation able to support it and thus under post-flashover conditions; is that correct? A. Yes. Q. In general, you've said that this more sophisticated modelling confirms your confidence in the simple model; is that correct?
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1	Q. Do you think it's likely that you would like to do more	1	Q. So let's turn, now, to the section of your report where
2	modelling at Phase 2?	2	you looked at the role of the uPVC window surrounds.
3	A. I do think that the modelling will only become necessary	3	When looking at the breaching of the compartment,
4	as a function of more detailed testing. So if there is	4	you focus quite heavily on the role of the uPVC around
5	a need to refine what are the exact conditions that led	5	the windows. In general, can you just explain why
6	to ignition of the external system, you know, then tests	6	you've done that?
7	will have to be done before modelling because you have	7	A. Yes, because the uPVC serves as a cover for a whole
8	to produce the right input data so that you actually	8	array of other materials that potentially could burn.
9	get it is justifiable to do a more precise model.	9	Now, uPVC is a material that, from a flammability
10	Q. I'm coming on to look at the role of the uPVC window	10	perspective, is a very robust material, it's a material
11	surrounds, and that section of your report I think you	11	that is very difficult to burn. So, in principle, it
12	were just talking about.	12	could potentially be an adequate protection layer for
13	A. Yes.	13	those materials.
14	Q. But before we leave this modelling topic, I just have	14	Nevertheless, the uPVC has a particularity, which is
15	a question about table 7 of your report. Can we go to	15	that it loses its mechanical strength at very low
16	that: JT0S0000001 at page 140.	16	temperatures, so effectively can actually fall off.
17	In that table, you've summarised some of the results	17	So this is the reason why I thought it was important
18	from your zone modelling. In the fourth substantive	18	to focus on the uPVC.
19	line, you have a smoke-filling time of 50 seconds for an	19	Q. You've explained in your report that is has a melting
20	ultrafast fire with a corresponding peak heat release	20	range of between 75 and 105 degrees C
21	rate of 360 kilowatts; is that right?	21	A. Yes.
22	A. Yes.	22	Q is that correct?
23	Q. If you look in the fourth line down, the last of the 1s	23	And it rapidly loses stiffness at 60 degrees
24	under scenario 1.	24	Celsius; is that right?
25	Is it right that this does not use the standard heat	25	A. Yes.
	Page 49		Page 51
		1	
1	malacca mata calculation from an ultrafact fine which	1	O. It loses 90 per cent by 90 degrees and 100 per cent by
1	release rate calculation from an ultrafast fire which	1	Q. It loses 80 per cent by 80 degrees and 100 per cent by
2	would result in figure of 470 kilowatts?	2	90 degrees.
3	would result in figure of 470 kilowatts? A. There's a confusion on what that 475 is. So when we use	2 3	90 degrees. A. Yes.
2 3 4	would result in figure of 470 kilowatts? A. There's a confusion on what that 475 is. So when we use an input, we utilise as standard what is called an alpha	2 3 4	90 degrees. A. Yes. Q. Can we just look at table 1 of your report. That's
2 3 4 5	would result in figure of 470 kilowatts? A. There's a confusion on what that 475 is. So when we use an input, we utilise as standard what is called an alpha t-squared fire. So effectively we plug in a time and we	2 3 4 5	90 degrees. A. Yes. Q. Can we just look at table 1 of your report. That's JT0S000001, at page 37.
2 3 4 5 6	would result in figure of 470 kilowatts? A. There's a confusion on what that 475 is. So when we use an input, we utilise as standard what is called an alpha t-squared fire. So effectively we plug in a time and we get a heat release rate, but that is the input, that is	2 3 4 5 6	90 degrees.A. Yes.Q. Can we just look at table 1 of your report. That's JT0S000001, at page 37.SIR MARTIN MOORE-BICK: Can I just ask you, when it gets to
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1	that has an ignition temperature of 377 degrees C; is	1 2	strength to having no strength.
2	that right?		Q. You said in your report that most fires originating from
3	A. Yes.	3	fuels typical of a domestic kitchen will have the
4	Q. That's just the polyethylene; is that right?	4	capacity to significantly damage the uPVC; is that
5	A. Yes.	5	right?
6	Q. It's not related to the aluminium. We'll come later to	6	A. Absolutely, because if we go back to the original
7	the panels.	7	discussion that we were having, we established that we
8	A. Yes.	8	needed a fire the size of a frying pan to be able to
9	Q. Then we have PIR, which is effectively insulation	9	bring the smoke layer to the floor, and that was the
10	A. Yes.	10	limits in which we were operating. So this particular
11	Q in the second column, and you have that with an	11	fire could not be bigger than a frying pan.
12	ignition temperature of 306 to 377 degrees C; is that	12	Then if you look at the smoke layer temperature, the
13	correct?	13	smoke layer temperature is around at the most
14	A. Yes.	14	200 degrees, so it cannot ignite anything. But
15	Q. In terms of the uPVC, you've talked about the fact that	15	nevertheless, it's 100 degrees above the temperature
16	it has this elastic modulus, which is of importance,	16	that you need to basically take the PVC down. In other
17	which I think is what you were just describing.	17	words, it loses all its mechanical properties.
18	Can we just look at that. Let's look at figure 9 of	18	We did a detailed heat transfer calculation,
19	your report. That's JTOS0000001 at page 41.	19	actually a very conservative one, and we showed we had
20	Can you just describe for us what we see here and	20	plenty of time to heat the uPVC to the point it would
21	what the red and the blue lines are? We have blue as	21	have lost all its mechanical integrity.
22	the modulus, I think.	22	This is very important because, again, it
23	A. Yes.	23	separates and this is a reason behind the strategy we
24	Q. Can you just explain what that is, and also what the red	24	follow for modelling the smoke temperature from the
25	line is showing?	25	flame temperatures. So the smoke cannot ignite
	Page 53		Page 55
	0		0
1	<u> </u>	1	<u> </u>
1 2	A. Yes. So this is a test conducted by Professor Bisby and	1 2	anything, but it can actually mechanically fail the
2	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC	2	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame.
2	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can	2 3	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've
2 3 4	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature	2 3 4	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical
2 3 4 5	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2,	2 3 4 5	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that
2 3 4 5 6	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the	2 3 4 5 6	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right?
2 3 4 5 6 7	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts	2 3 4 5 6 7	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes.
2 3 4 5 6 7 8	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get	2 3 4 5 6 7 8	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that
2 3 4 5 6 7 8	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperaturesorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other	2 3 4 5 6 7 8 9	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause
2 3 4 5 6 7 8 9	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about	2 3 4 5 6 7 8 9	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right?
2 3 4 5 6 7 8 9 10	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So	2 3 4 5 6 7 8 9 10	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations
2 3 4 5 6 7 8 9 10 11	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line.	2 3 4 5 6 7 8 9 10 11 12	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple
2 3 4 5 6 7 8 9 10 11 12 13	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at	2 3 4 5 6 7 8 9 10 11 12 13	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial
2 3 4 5 6 7 8 9 10 11 12 13 14	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the	2 3 4 5 6 7 8 9 10 11 12 13 14	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere
2 3 4 5 6 7 8 9 10 11 12 13 14 15	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature — sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's	2 3 4 5 6 7 8 9 10 11 12 13 14 15	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees. So what you're looking for on the red line is when	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say is vulnerable to heating. You say the ability to secure
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature — sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees. So what you're looking for on the red line is when it starts going up, because that's telling you when it	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say is vulnerable to heating. You say the ability to secure the uPVC at elevated temperatures is considered
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature — sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees. So what you're looking for on the red line is when it starts going up, because that's telling you when it starts to change.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say is vulnerable to heating. You say the ability to secure the uPVC at elevated temperatures is considered negligible.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees. So what you're looking for on the red line is when it starts going up, because that's telling you when it starts to change. What you're looking from the blue line is when it	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say is vulnerable to heating. You say the ability to secure the uPVC at elevated temperatures is considered negligible. Can we look at that. If we go to figure 55 of your
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees. So what you're looking for on the red line is when it starts going up, because that's telling you when it starts to change. What you're looking from the blue line is when it ends, because that tells you when it doesn't have any	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say is vulnerable to heating. You say the ability to secure the uPVC at elevated temperatures is considered negligible. Can we look at that. If we go to figure 55 of your report. That's JTOS0000001_0042.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees. So what you're looking for on the red line is when it starts going up, because that's telling you when it starts to change. What you're looking from the blue line is when it ends, because that tells you when it doesn't have any more strength. So between 60 and 100 degrees, you	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say is vulnerable to heating. You say the ability to secure the uPVC at elevated temperatures is considered negligible. Can we look at that. If we go to figure 55 of your report. That's JTOS0000001_0042. So what we're seeing here is underneath the uPVC
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	A. Yes. So this is a test conducted by Professor Bisby and basically shows you what is the elastic modulus for uPVC at ambient, which is 2.5 times 10 to the 9 and you can see that as you start increasing the temperature sorry, ambient temperature it's a little bit above 2, times 10 to the 9. So as you start increasing the temperature, what happens is that the value starts dropping, so that's the blue line. So you get a decaying value that eventually hits 0, so in other words it has no strength by the time it gets to about 80/90 degrees, and by 100 clearly has nothing left. So that will be the blue line. What the red line is, it just shows you the rate at which that happens. So what you can see is that at the beginning, there's very little change, you can see it's flat, very little change, and then eventually it starts changing drastically, and that happens at about 60 degrees. So what you're looking for on the red line is when it starts going up, because that's telling you when it starts to change. What you're looking from the blue line is when it ends, because that tells you when it doesn't have any	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	anything, but it can actually mechanically fail the uPVC. To ignite things, we need a flame. Q. You've said in your report that the uPVC would've reached temperatures with a total loss of mechanical strength in approximately 5 to 11 minutes; is that right? A. Yes. Q. You also say that the kitchen is sufficiently small that it doesn't matter where in the room the fire is to cause that total loss of mechanical strength; is that right? A. Exactly. So with the CFD and all the other validations we did, we showed that, effectively, the very simple model that doesn't take into account spatial resolution in other words, you can place it anywhere you want will effectively be sufficient to be able to establish that. Q. You've noted in your report that the uPVC is held in place by an adhesive, a kind of glue, which you also say is vulnerable to heating. You say the ability to secure the uPVC at elevated temperatures is considered negligible. Can we look at that. If we go to figure 55 of your report. That's JTOS0000001_0042.
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1	A. Yes.	1	Q. I believe there's actually one on the next page as well,
2	Q. Can you just draw your attention to the adhesive, is it	2	if we can go to that.
3	the bottom label there?	3	A. Yes, you can see it on the side, and in this case also
4	A. Yes, it's the bottom label and you can see the mark of	4	on the top.
5	the adhesive. So adhesive is a polymer and it will	5	MS GRANGE: Yes, thank you. Sorry.
6	actually behave in a very similar way as a uPVC. It	6	So I think that's a convenient moment for a break.
7	will lose all its mechanical integrity by the time it	7	SIR MARTIN MOORE-BICK: Would it be a good idea?
8	gets to about 60/70 degrees. So effectively both the	8	MS GRANGE: Yes, I think it would.
9	adhesive and the PVC will have no mechanical strength.	9	SIR MARTIN MOORE-BICK: I think we'll all have a break now,
10	So the adhesive has no capacity to keep the uPVC in	10	professor.
11	place, and the weight of the uPVC is much more than what	11	I'm going to ask you not to talk to anyone about
12	the uPVC can hold itself.	12	your evidence while you're out of the room. If you go
13	Q. What we can see the reference of under there are the PIR	13	with the usher, she'll look after you. We'll come back
14	foam insulation which was all the way around the	14	at 11.30. All right?
15	windows; is that's correct?	15	Thank you very much, you go with the usher now.
16	A. Yes.	16	All right, 11.30, please.
17	Q. Top, bottom, left, right yes.	17	(11.20 am)
18	What is your view about this arrangement in terms of	18	(A short break)
19	any potential path of fire spread out of the window?	19	(11.30 am)
20	A. Well, effectively, the smoke, even though its	20	SIR MARTIN MOORE-BICK: All right, professor? Ready to
21	temperature is very low, is capable, with a big margin	21	carry on?
22	of safety, to mechanically fail the uPVC. So it opens	22	THE WITNESS: Yes, thank you.
23	a direct path for any flame to actually impinge on any	23	SIR MARTIN MOORE-BICK: Thank you.
24	of the combustible materials on the inside.	24	Yes, Ms Grange.
25	Q. Just on this topic, can we look at some of the photos	25	MS GRANGE: Thank you.
			No ora i (oz.) Tilana you
	Page 57		Page 59
1	that you've used in your report to illustrate the	1	I now want to turn to the topic of the break-out of
2	failure of the uPVC we saw at Grenfell Tower. Can we go	2	the fire from flat 16 and the method of ignition of the
3	to JTOS0000001 at page 43 to start with.	3	facade materials.
4	Can we zoom in on the top one for the moment.	4	I'm going to give a trigger warning at this point
5	You said in your report that the failures are	5	because in about 5 to 10 minutes I'm going to be showing
6	usually around the head and the jamb. Can you explain	6	a video of the early stages of the fire at
7	what you mean by the head and the jamb by reference to	7	Grenfell Tower, going up the east face from flat 16.
8	these photographs?	8	This contains images and audio that some may find
9	A. So you can see the piece of uPVC hanging in there, and	9	distressing.
10	you see where it came from. So effectively this will	10	SIR MARTIN MOORE-BICK: Yes.
11	rip off downwards, falling all the way to the bottom.	11	MS GRANGE: I will also be taking Professor Torero to
12	That's kind of what I meant.	12	a number of stills and photographs of the fire in this
13	Q. You've also used the word "fall-off" in this context.	13	section of my questioning.
14	Is that just it falls off? A. Folls off. It begins by first starts forming and	14	SIR MARTIN MOORE-BICK: Right. MS GRANGE: I will give enother warning when I get to that
15	A. Falls off. It basically first starts forming and		MS GRANGE: I will give another warning when I get to that
16 17	eventually falls off. You see it more clearly in the	16	video, but I wanted to give it now in case anyone wants
	next photograph.	17	to be prepared for that. SIR MARTIN MOORE-BICK: Thank you, that's very helpful.
	MS CDANICE: Mr Chairman Ura navy sains to turn to	10	
18	MS GRANGE: Mr Chairman, I'm now going to turn to	18	•
18 19	a different topic.	19	MS GRANGE: In section 3.5 of your report first of all,
18 19 20	a different topic. SIR MARTIN MOORE-BICK: Did you want to show us the next	19 20	MS GRANGE: In section 3.5 of your report first of all, just to be clear, you have not addressed cause and
18 19 20 21	a different topic. SIR MARTIN MOORE-BICK: Did you want to show us the next photograph?	19 20 21	MS GRANGE: In section 3.5 of your report first of all, just to be clear, you have not addressed cause and origin of the fire in your report, which is dealt with
18 19 20 21 22	a different topic. SIR MARTIN MOORE-BICK: Did you want to show us the next photograph? THE WITNESS: Yes, if you can look.	19 20 21 22	MS GRANGE: In section 3.5 of your report first of all, just to be clear, you have not addressed cause and origin of the fire in your report, which is dealt with by other inquiry experts; is that correct?
18 19 20 21 22 23	a different topic. SIR MARTIN MOORE-BICK: Did you want to show us the next photograph? THE WITNESS: Yes, if you can look. MS GRANGE: Oh, sorry. Let's finish these photographs.	19 20 21 22 23	MS GRANGE: In section 3.5 of your report first of all, just to be clear, you have not addressed cause and origin of the fire in your report, which is dealt with by other inquiry experts; is that correct? A. Yes, I've taken the information from Professor Nic Daeid
18 19 20 21 22 23 24	a different topic. SIR MARTIN MOORE-BICK: Did you want to show us the next photograph? THE WITNESS: Yes, if you can look. MS GRANGE: Oh, sorry. Let's finish these photographs. Let's go to the one at the bottom of the page.	19 20 21 22 23 24	MS GRANGE: In section 3.5 of your report first of all, just to be clear, you have not addressed cause and origin of the fire in your report, which is dealt with by other inquiry experts; is that correct? A. Yes, I've taken the information from Professor Nic Daeid and Professor Bisby on that matter.
18 19 20 21 22 23	a different topic. SIR MARTIN MOORE-BICK: Did you want to show us the next photograph? THE WITNESS: Yes, if you can look. MS GRANGE: Oh, sorry. Let's finish these photographs.	19 20 21 22 23	MS GRANGE: In section 3.5 of your report first of all, just to be clear, you have not addressed cause and origin of the fire in your report, which is dealt with by other inquiry experts; is that correct? A. Yes, I've taken the information from Professor Nic Daeid
18 19 20 21 22 23 24	a different topic. SIR MARTIN MOORE-BICK: Did you want to show us the next photograph? THE WITNESS: Yes, if you can look. MS GRANGE: Oh, sorry. Let's finish these photographs. Let's go to the one at the bottom of the page.	19 20 21 22 23 24	MS GRANGE: In section 3.5 of your report first of all, just to be clear, you have not addressed cause and origin of the fire in your report, which is dealt with by other inquiry experts; is that correct? A. Yes, I've taken the information from Professor Nic Daeid and Professor Bisby on that matter.

1 calculated that? 1 Have you considered the different hypotheses posited 2 2 by Professor Bisby in terms of the method of ignition of A. Yes. So, basically, if we provide enough ventilation to 3 3 the cladding materials on the facade? allow the temperature of the flames to reach those 4 4 temperatures, you can establish what is the heat release 5 Q. In his latest report, Professor Bisby discusses two 5 rate that will deliver the necessary temperature so that 6 particular hypotheses. 6 you can ignite the cladding from the outside. 7 7 First, what is now called hypothesis B1, which is The one thing that is very different about both 8 essentially the impingement of flaming and hot gases 8 hypotheses -- and maybe this is the time to clarify through an open window, whether that be through the 9 that -- is that when we have a compartment fire, the 10 extract panel or via the extract fan itself, and then 10 compartment is always going to be hotter than the plume 11 subsequent ignition of the external ACM panels 11 outside. So from a physical perspective, a path that 12 immediately above the kitchen window. 12 ignites from the inside is a more probable cause of 13 Is that correct? 13 ignition because the temperatures are always going to be 14 14 higher in the inside than in the outside. A. Yes. 15 Q. He's also discussed what's now called hypothesis B2, 15 Now, Professor Bisby comes from a different angle, 16 which is the ignition by flame of exposed flammable 16 which is also perfectly possible, which is once 17 17 materials in the window surround and the external something ignites, that something can create a flame, 18 cladding system being penetrated by fire, allowing flame 18 and that flame can be the one that results in the 19 spread back into the back of the cladding cavity. 19 ignition of the subsequent materials. 20 20 Is that correct? Now, he's coming from the observation, so he's 21 21 looking at different images and he's basically looking 22 Q. Do you agree that these are the two possible routes of 22 at the different flames that are moving in different 23 ignition out and into the cladding? 23 directions. He is observing that there is a high 24 24 probability that a flame could have impinged on the 25 25 Q. Do you think there are any other plausible candidates external cladding. Page 61 Page 63 1 for that? 1 So the two options and the weighing that we are 2 A. They are clearly the two most probable causes. 2 giving to the two options, and the reason why I didn't 3 3 Q. I just want to start by discussing hypothesis B1, the feel there was any need for me to clarify any further in 4 venting through the window opening and up into the 4 my report, is because we are coming from different 5 5 angles, and I believe that the chairman needs to panels above the window. 6 As we discussed just before the break, does it 6 consider both, in the sense that one comes from a purely 7 7 remain your view that the smoke itself is not going to physical analysis of the problem, that shows that the 8 be hot enough for the smoke that's venting through the 8 hotter part and the closest to a flame will be from the 9 9 window opening to ignite the cladding? inside, but the other one is more a probabilistic one, 10 A. Yes. 10 it is: what ignited first? And if there is a sequence 11 Q. You say that the maximum temperature of the smoke layer 11 of ignitions that resulted in a flame, that could 12 is around 220 degrees Celsius, even with an ultrafast 12 perfectly be the case of igniting on the outside. But 13 fire; is that correct? 13 that comes more from observations of images and 14 14 A. Yes. evidence. 15 Q. So ignition of the materials even surrounding the 15 Q. It might be helpful at this point to look at your 16 window, specifically the PIR insulation which is behind table 3, JTOS0000001 at page 50. 16 17 the uPVC, that requires 306 degrees Celsius; is; that 17 If we can zoom in on the table at the top of the 18 right? 18 19 A. Yes. 19 Can you just talk us through in basic terms what 20 Q. You've calculated that direct ignition via direct flame 20 this table is showing us in terms of fire size and 21 or plume impingement through the window would require 21 distance and these three materials? 22 a fire of around 830 kilowatts to ignite the ACP through 22 A. Yes. So, basically, what you see in the table is, 23 23 the window; is that correct? depending on the location of the material and its 24 24 ignition characteristics, we looked into having 25 25 Q. Can you just explain for the chairman how you've a flame -- maybe we should look at the diagram first.

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1	Q. Is that figure 14?	1	why we're giving the two ranges.
2	A. That would be	2	SIR MARTIN MOORE-BICK: Yes.
3	Q. Or is it figure 13? Which one?	3	MS GRANGE: So this helps explain what we see in your
4	A. That would be figure 13.	4	table 3
5	Q. So if we go to JTOS0000001_0047.	5	A. Exactly.
6	If we can zoom in on figure 13 at the bottom.	6	Q is that correct? Do you want to just go back to that
7	A. Okay.	7	now?
8	Q. Is that what you're referring to?	8	A. Yes.
9	A. Yes. So, basically, those are the two potential	9	Q. So if we just go back to table to 3, which is on
10	options. So you can have a fire that is unobstructed	10	page 50.
11	that directly impinges on a target, and that target	11	If you can now just talk us through for each of the
12	could be the PIR or the uPVC or the cladding.	12	elements what we're seeing.
13	So we know what the position of these components is,	13	A. Yes. So we know how big a fire can be now because we've
14	so we can establish what the distance is between the	14	done the analysis. So if we take that size of a fire,
15	fire and the target. On the basis of that, I can	15	then the distance you see there is: how far do I need to
16	establish how big of a fire do I need so that the flame	16	move the fire away from the target before it cannot
17	at the position of the target has sufficient temperature	17	
18	to ignite. Okay?	18	reach the ignition temperature? On The tight where we see the figure of \$20 kilowette.
19	If there's an obstacle, the flames will have to go	19	Q. That's where we see the figure of 830 kilowatts.
20	to the ceiling, then progress along the ceiling, and	20	A. That's where you see the maximum distance.
21	effectively hit the target.		Q. Yes.
22	·	21	A. The final column.
23	So given that the smoke cannot ignite, it has to be	22	Q. Yes. But I put to you the smallest fire, 830 kilowatts
24	direct impingement from the flame.	23	would be needed to ignite the polyethylene
25	So what we looked into was, given the position of	24	A. Yes.
23	the fire, how big of a fire we had to have to be able to	25	Q at the top of the window.
	Page 65		Page 67
1	ignite the targets, and that's what you have on the	1	A. Yes, exactly.
2	table.	2	Q. You say that's a flashover fire, so you think that's
3	Q. You just talked about the phenomenon of a ceiling jet	3	unlikely.
4	that might occur behind an object.	4	A. Yes.
5	A. Yes.	5	Q. In terms of direct flame impingement through an open
6	Q. So the fire goes up behind the object and then across	6	window, is it therefore relevant that the flames
7	the ceiling and out	7	would've fed out into the open atmosphere outside the
8	A. Yes.	8	flat?
9	Q towards the window.	9	A. Yes, it would've had to ignite something in between
10	How likely do you think that might have been here?	10	because the flame would've had to be placed closer to
11	A. Well, if the fire was established behind any obstacle,	11	the opening to be able to be smaller and still reach the
12	that would've had to be the case because effectively it	12	ignition temperatures of the cladding.
13	had to go through the obstacle before it reaches	13	Q. Does the flame get cooled in the process of coming out
14	a target. So the only way that could've happened is it	14	of an open window, and is that relevant to the analysis
15	going up, hitting the ceiling and then propagating	15	of whether or not that's a likely method of impingement?
16	across the ceiling towards the target. So it would be	16	A. Yes. So the moment the flame exits the compartment,
17	highly probable.	17	there is going to be fresh air and that's going to cool
18	SIR MARTIN MOORE-BICK: Can I ask you to consider a slightly	18	the temperatures of the flame. It is always going to be
19	different hypothesis, which is that the fire breaks out	19	the case that the spill flame is going to be colder than
20	behind an obstacle but to the side of the target. In	20	the interior compartment. It cannot be the opposite.
21	other words, it doesn't have to go over the obstacle to	21	So, yes, that will definitely influence the analysis.
22	get to the target, it might go at a different angle.	22	But I want to make this point again, that in this
23	A. It would be bounded by the two of them. So this is the	23	particular type of scenarios, because we're talking
24	worst-case scenario and the other one is the best case	24	about flames that can impinge on numerous things, there
25	scenario. So it would be somewhere in between. That's	25	can be a sequence of ignitions. So one thing can ignite
	2	23	can be a sequence of ignitions. So one thing can ignite
	Page 66		Page 68

1	another one and ignite another one, and those things you	1	ignite those panels.
2	can only ascertain by looking into the visual evidence	2	The mechanism would've been that eventually, either
3	that you have.	3	through melting or through splitting, you would've had
4	So I think when comparing my conclusions with	4	a surface of the polyethylene that is exposed, a flame
5	Professor Bisby's conclusions, we have to make sure that	5	will have crept in there and that's what would have
6	we understand that I did not do the detailed analysis of	6	ignited the material.
7	the images, that's what he did, and he didn't do the	7	Q. Are there any exposed edges of polyethylene above the
8	detailed analysis of the fire dynamics, which is what	8	window?
9	I did, and the two things complement each other.	9	A. I would imagine that there would be.
10	Q. Can we just look for a moment about what the method of	10	Q. Dr Lane had some I think marked here on the
11	impingement might have been for the ACP panels above the	11	A. Yes.
12	window.	12	Q right-hand side.
13	Can we look at a picture of what we see above the	13	Does that affect the analysis in terms of whether or
14	window. Can we go to figure 40 of Professor Bisby's	14	not there are those
15	report. That's LBYS0000001 at page 68.	15	A. Well, if there were no exposed edges, it would be even
16	This is a good photograph which shows you what you	16	more difficult to ignite because you would have to
17	see. Just to make clear, the ACM material on the column	17	breach the encapsulation of the material. So all those
18	has been removed here to the left of the picture, but to	18	details will have some impact on the way it ignites, but
19	the right, we're looking directly up from the window to	19	one that it would be very, very difficult to predict.
20	the ACM cassettes that were immediately above; is that	20	Q. If this had been the mechanism of fire spread, would you
21	correct?	21	have expected a time delay, given the factors you were
22	A. Yes.	22	just talking about, when compared with other possible
23	Q. We see there the way the cassettes were fabricated was	23	routes?
24	there was a 90-degree return and then a kind of level	24	A. Not necessarily.
25	A. Yes.	25	Q. Can we just look at the thermal imaging from flat 16,
	Page 69		Page 71
1	Q underneath the window, immediately above the	1	which indicates that the fire may have vented from the
1 2	Q underneath the window, immediately above the extractor fan; is that correct?		which indicates that the fire may have vented from the window in the corner of the room.
	•	2	window in the corner of the room.
2	extractor fan; is that correct?		•
2	extractor fan; is that correct? A. Yes.	2 3 4	window in the corner of the room. If we go again within Dr Lane's report to BLAS0000009 at page 43. Can we go to figure 9.37.
2 3 4	extractor fan; is that correct? A. Yes. Q. Can we also look at another picture, a picture from	2 3	window in the corner of the room. If we go again within Dr Lane's report to BLAS0000009 at page 43. Can we go to figure 9.37. So in the image at the top we have a still from the
2 3 4 5	extractor fan; is that correct? A. Yes. Q. Can we also look at another picture, a picture from Dr Lane's report. That is BLAS0000010 at page 26,	2 3 4 5	window in the corner of the room. If we go again within Dr Lane's report to BLAS0000009 at page 43. Can we go to figure 9.37.
2 3 4 5 6	extractor fan; is that correct? A. Yes. Q. Can we also look at another picture, a picture from Dr Lane's report. That is BLAS0000010 at page 26, figure 10.26.	2 3 4 5 6	window in the corner of the room. If we go again within Dr Lane's report to BLAS0000009 at page 43. Can we go to figure 9.37. So in the image at the top we have a still from the thermal imaging that was taken; is that correct? A. Yes.
2 3 4 5 6 7	extractor fan; is that correct? A. Yes. Q. Can we also look at another picture, a picture from Dr Lane's report. That is BLAS0000010 at page 26, figure 10.26. This is another photograph of the window, this is to	2 3 4 5 6 7	window in the corner of the room. If we go again within Dr Lane's report to BLAS0000009 at page 43. Can we go to figure 9.37. So in the image at the top we have a still from the thermal imaging that was taken; is that correct?
2 3 4 5 6 7 8 9	extractor fan; is that correct? A. Yes. Q. Can we also look at another picture, a picture from Dr Lane's report. That is BLAS0000010 at page 26, figure 10.26. This is another photograph of the window, this is to the right-hand side of the window, and we can see those	2 3 4 5 6 7 8 9	window in the corner of the room. If we go again within Dr Lane's report to BLAS0000009 at page 43. Can we go to figure 9.37. So in the image at the top we have a still from the thermal imaging that was taken; is that correct? A. Yes. Q. Does this image help at all in your view about what the
2 3 4 5 6 7 8	extractor fan; is that correct? A. Yes. Q. Can we also look at another picture, a picture from Dr Lane's report. That is BLAS0000010 at page 26, figure 10.26. This is another photograph of the window, this is to the right-hand side of the window, and we can see those cassettes above. She's put a ring in there which we'll	2 3 4 5 6 7 8	window in the corner of the room. If we go again within Dr Lane's report to BLAS0000009 at page 43. Can we go to figure 9.37. So in the image at the top we have a still from the thermal imaging that was taken; is that correct? A. Yes. Q. Does this image help at all in your view about what the route of escape may have been through the window?
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those are the areas that seem to be the hottest. 1 1 than the temperatures that the flame could provide. 2 2 Q. Just to be clear, which areas do you think? Effectively, as soon as the flame reaches a certain 3 3 A. The areas are in yellow. size, you will create a condition by which any of these 4 4 materials could ignite. 5 5 A. But as you can see, still the temperatures are Q. What materials are we talking about here? Let's be clear what the candidates are. We talked before by 6 150 degrees. So clearly there is a concentration of 6 7 7 reference to the photograph of immediately behind the heat in there, but it is more the smoke layer type of 8 heat. 8 uPVC we have the insulation. 9 9 One of the things that many times our thermal images 10 cameras mislead us is the different materials have 10 Q. The small layer of insulation that we have top, bottom, 11 different emissivities. So while the camera might think 11 left and right; is that correct? That's PIR 12 it is reading more heat, it might actually reading less 12 insulation --13 heat it's the material that is emitting more energy. 13 A. Yes. 14 So I wouldn't make too much out of that image other 14 O. -- around the window. 15 than the fact there seems to be a slight concentration 15 Then we also have an EDPM membrane on the column 16 of heat in that area. 16 side. 17 Q. You have concluded in your report that you think the 17 A. Yes. 18 most likely route of ignition of the facade is by flame 18 Q. Do you think those two are both candidates for --19 of exposed flammable materials in the window surrounds; 19 A. So is the uPVC. 20 is that correct? 20 Q. Itself? 21 A. Yes. 21 A. Of course. 22 22 Q. Does that remain your view, despite reading Q. From there, if those materials had ignited around the 23 Professor Bisby's report? 23 window sides -- let's take the column sides, so we have 24 A. That remains my view from a physical perspective, 24 the insulation, the EPDM membrane -- what happens then 25 25 in terms of the column? What's next? I think that that is the case, but I do not discount by Page 73 Page 75 1 A. Then you will get flames into a cavity, and effectively 1 any means, you know, what the visual evidence might 2 show, because clearly, as I say, you can have a random 2 you are affecting the ACM panel, you are affecting 3 3 everything. So what follows after will be just the sequence of ignitions that can actually lead to an 4 external ignition. So I cannot discard that as 4 progression of the fire through the space, and it could 5 a possibility. 5 come out as easy as it went in. 6 6 Q. Can you summarise for us why you think that's the most So, in principle, the sequence that follows after 7 7 is, again, almost impossible to detail step by step. likely route? 8 8 A. Fundamentally because the fire dynamics will tell you But all the different components as you could see in the 9 previous photograph that you showed, they're all so much 9 that the highest temperatures and the closest proximity 10 10 to the flames is going to be in the compartment. in proximity that there is no question that there will 11 Anything outside the compartment is going to be colder 11 be a sequence of ignitions of all of them. 12 12 Q. So you think all of those would have ignited as part of and further unless you find the path of ignition after 13 ignition that brings you there, and that you can only 13 the path out? 14 14 A. Yes. tell by a detailed analysis of images. 15 Q. Can we be clear on what you think the most likely path 15 Q. It's right, isn't it, there were no cavity barriers around the windows? 16 is. So we've talking about the melting and deforming of 16 the uPVC --17 A. I don't believe so. 17 18 18 Q. You've calculated that a fire with characteristics A. Yes. 19 19 Q. -- possibly via the smoke layer itself -similar to that of a kitchen fire, if placed within 20 20 3 metres of the window, is capable of igniting those 21 21 combustible materials adjacent to the window; is that Q. -- without any direct flame impingement. 22 What's the next thing you think is most likely to 22 correct? 23 23 have ignited? 24 A. That's impossible to say because all the materials in 24 Q. For example, you've said in your report that a fire at 25 25 floor level of just 20 kilowatts is capable of igniting there will have ignition temperatures that are lower Page 74 Page 76

1 1 materials at windowsill level, ie at the lower parts of much faster. 2 2 Q. Is it right that the PIR insulation would've had the the level. 3 lowest thermal inertia of any of those materials we were 3 A. Yes. 4 Q. Again, what materials are we talking about there? 4 just discussing? 5 5 A. Basically we took as a reference the ignition A. Yes. Q. Is it right that the polyethylene would've had the 6 temperatures of all of them, so it could've ignited any 6 7 7 of them. highest thermal inertia? 8 Q. As you say, you've also looked at fires behind 8 A. Yes. 9 9 Q. Do those thermal inertia values assist in working out an obstacle because of the fact that it may have been 10 behind the fridge; is that correct? 10 which is likely to have been the route of ignition? 11 A. Yes, where the two bounding -- so the fire that is 11 A. Not clearly, they just give you an estimate of what 12 unobstructed is the smallest possible fire and the other 12 could've gone first. But these numbers are only valid 13 extreme will be the one that is fully confined behind 13 in the sense that they had to be under exactly the same 14 an obstacle. 14 conditions. So if you have a flame impinging on the 15 Q. In terms of that fire we were just discussing behind 15 polyethylene but 10 centimetres away from the PIR, the 16 16 an obstacle and then a ceiling jet across the ceiling, polyethylene will ignite faster than the PIR. 17 17 you've noted in your report that there was a strip of So the way in which the fire evolves and how it 18 18 purlboard -interacts with those materials is really the dominant 19 A. Yes. 19 function. I mean, what we're talking about here is 20 20 Q. -- a kind of legacy strip of purlboard above the window a very small fire being capable of igniting any of these 21 on the flat side of the window before you got to the 21 things. That's the ultimate question. 22 22 uPVC surround. What the sequence is and all the details is 23 23 A. Yes. extremely difficult, because while they are related to 24 Q. Is that something that you remain interested in? 24 all these material properties, they're much more related A. Yes, because obviously that will be the one that will be 25 2.5 to where the flame was in relationship to the material. Page 77 Page 79 1 Q. Again, just to test this a little bit more, what about 1 in closest proximity to a flame, so it would be the 2 first one to be affected. 2 the aluminium skins that we have on different materials? 3 3 Q. So you think it's possible that the ceiling jet may have You've talked previously when we looked at the ACM 4 impinged on that first and then onto the uPVC or the 4 cassettes that they had an aluminium skin that may well 5 have been relevant in terms of whether it was first to insulation? 5 6 6 A. Yes. 7 Q. Do you think that's something that should be the subject 7 What about the PIR and the foil that is on the PIR? 8 of further consideration and testing at Phase 2? 8 A. The foil on the PIR and in as much as the aluminium skin 9 9 A. I mean, I think that clearly it is important to try to are going to have an impact in trying to slow down 10 have as many pieces of the puzzle as possible. 10 ignition, that's clear. 11 Nevertheless, the importance to the overall outcome of 11 The aluminium skin of the ACM being thicker 12 what was the first thing to catch on fire is probably 12 obviously has a bigger impact, so it is actually quite 13 not that significant. 13 difficult to ignite an ACM panel. But all these things, 14 O. It's right, isn't it, that the different materials 14 again, you know, they do have an impact. So obviously around the window would've had different thermal 15 15 exposed PIR will be more susceptible to ignition than 16 inertias; is that correct? 16 PIR covered by an aluminium film. 17 A. Yes. 17 SIR MARTIN MOORE-BICK: Just help me with this: is the 18 Q. That's the speed at which they flame, at which they 18 purpose of the -- because it's a very thin skin of 19 pyrolyse and release combustible gases. 19 aluminium, isn't it, on the PIR? Is its function to 20 A. Yes. It's the speed at which they can absorb energy 20 dissipate the heat or exclude the oxygen or what? 21 towards ignition. 21 A. Its function is to actually -- it's not to dissipate the 22 Q. If something has a low thermal inertia, does that mean 22 heat in this case, although it does have a reflective --23 it's first to ignite compared to something with a 23 so part of the heat gets reflected out. Its function is 24 material of a high thermal inertia? 24 mostly to separate the fuel from the oxidiser. So that 25 A. Yes, a material with low thermal inertia will ignite 25 delays the whole process of ignition. Because once the Page 78 Page 80

1	material reaches the point where it starts evaporating,	1	exposed PE cores where it's been cut in relation to
2	it still has to reach the oxygen before it ignites, and	2	those columns.
3	the barrier serves to block that transfer.	3	Again, do you think that that could've been
4	SIR MARTIN MOORE-BICK: Thank you.	4	significant in terms of the route of fire spread out of
5	MS GRANGE: Do you think that the exposed sides of the	5	flat 16?
6	insulation in the columns so they had a foil face but	6	A. Again, you know, all those elements are potentially
7	they had exposed sides might be significant in this	7	significant, they could potentially have an influence.
8	context?	8	But once again, I mean, look at the complexity of the
9	A. Well, they are going to change the outcome, in the sense	9	system. Being able to predict to what extent it
10	that the exposed sides will ignite faster than the areas	10	mattered to me is completely overwhelmed by the fact
11	that are not exposed. But in this context, I think,	11	that you have a very small fire in the interior that can
12	given, as I say, the proximity of all these materials,	12	actually have the capacity to ignite any of those
13	the complexity of the cavity, and the nature of the fire	13	components. That at the end remains to me the bottom
14	event, it's extremely difficult to figure out to what	14	line. The details are very, very difficult to
15	extent that would've mattered or not.	15	articulate in a separate way.
16	Q. Can we look at a picture of that just to orientate	16	MS GRANGE: I now want to turn to the visual evidence which,
17	ourselves on that.	17	as you say, Professor Bisby has considered in a lot of
18	If we go to figure 8.37 in Dr Lane's report, that's	18	detail.
19	BLAS0000008 at page 35.	19	I'm about to play Professor Bisby's video, so I want
20	So this is a picture where we can see the column	20	to repeat the trigger warning at this point. We're now
21	insulation, which was 100 millimetres, with the foil	21	going to be showing a video of the early stages of the
22	skin. The ACM column panels have been taken off, so we	22	fire at Grenfell Tower at the east face. This contains
23	see it inside, and we can see the exposed edge there.	23	images and audio that some may find distressing.
24	Is that what you were just talking about?	24	I'm then going to be asking you about a number of
25	A. Yes.	25	stills that we see in relation to that visual evidence.
	Page 81		Page 83
1	O. V	,	The coincide installanths first port of the video
1	Q. You are saying, therefore, that may have played a	1 2	I'm going to just play the first part of the video,
2	slightly different in terms of if it's got into the	3	approximately 8 minutes, and we're going to look at the
3	column, you've got potentially an exposed edge there.	4	time period between 01.05 and 01.17 in this video. We're going to stop it there.
4 5	A. Yes. But, again, going back to the point I was making, you will see also other materials involved a very	5	So if I can now
6	intricate geometry.	6	SIR MARTIN MOORE-BICK: Shall we just pause for a minute
7	· ·	7	because well, I can't see anyone making to leave this
8	From an idealised perspective, a designer would like to be able to model performance. So I would like to be	8	room, but there might be people in the overflow room who
9	able to create some calculations that allow me to tell	9	might want to get out.
10	you what the performance is of the system.	10	(Pause)
11	Here we have designed and built a system, and we've	11	All right, shall we go on then?
12	made it so intricate and complex that we have no	12	MS GRANGE: Yes. So if I can now play that video.
13	capacity to be able to predict performance.	13	(Video Played)
14	So when we are discussing these little details, we	14	Can you stop that there.
15	have to put that into context, that effectively this is	15	I've shown that now because that passage is going to
16	such a complex system that being able to say, "This is	16	be relevant to a number of topics that we're going to
17	how it went and this is the direction and it jumped from	17	come to in a moment.
18	here to here", is a complete impossibility because the	18	That visual evidence has been addressed, as you say,
19	system is way too complex.	19	in Professor Bisby's report. Can we just turn up what
20	Q. Can we also look at figure 10.10 of Dr Lane's report.	20	Professor Bisby has said about it in particular. If we
20	That's BLAS0000010.	20 21	look at his report, LBYS0000001, at page 145,
22		22	paragraph 692 to start with.
	So here what we're seeing is we're looking at the	23	If we can just zoom in on that that's great, yes.
	column let's focus on the right wo're looking at	1 43	if we can just zoom in on that that's great, yes.
23	column let's focus on the right we're looking at		So there he cave:
23 24	some on the column panels, the ACM panels covering those	24	So there he says: "Since Leubmitted my initial Phase 1. Expert
23			So there he says: "Since I submitted my initial Phase 1 — Expert
23 24	some on the column panels, the ACM panels covering those	24	•

1	Report, additional video evidence of the early fire	1	growth started. In that case, then that conclusion will
2	spread to the cladding — taken from outside the tower —	2	be probably most appropriate.
3	has become available This shows that, beginning at	3	But if the incubation period would've been very
4	approximately 01:11:45 molten material is burning on	4	short, then all the major events would've happened in
5	the upper surface (i.e. sill) of the spandrel rainscreen	5	the first 10 minutes. So effectively that would've been
6	cassettes immediately below the kitchen window of	6	too late and most likely would've ignited from the
7	Flat 16. This is coincident with external flaming	7	inside before.
8	venting through the hole created by the failure and	8	So there's a lot of uncertainty on the way in which
9	movement of the extract fan and infill panel. It is	9	the fire actually evolves at the beginning, and the fact
10	considered likely that this burning material is melted	10	that we have an alarm doesn't necessarily tell us what
11	PE filler from the ACM cassettes located directly above	11	was the stage of the fire and how long it will take it
12	the window. It should be noted that this material could	12	before it starts affecting things.
13	also be XPS core material from the window infill panel	13	In a similar manner, the image is what we're seeing
14	housing the extract fan; however, I consider this less	14	from the outside, so we have no capacity to see what is
15	likely."	15	happening behind.
16	Just pausing there, can we look, before I ask you	16	So I think this is a very important piece of
17	some questions about this, at figure 65 of	17	evidence that shows you that there is significant
18	Professor Bisby's report, which is a still which he's	18	involvement of the external cladding in the fire at this
19	referring to there.	19	point, but it is not necessarily conclusive that that is
20	That is at LBYS0000001 at page 122, figure 65.	20	the only way in which the fire could have ignited,
21	If we can zoom in on 65 at the bottom.	21	because it really depends on the way the fire evolved
22	Professor Bisby appears to be highlighting in	22	and that's something we will probably never know.
23	particular at this point that we have molten material	23	Q. When you talked a moment ago about "we know we had the
24	burning immediately below the kitchen window. Is that	24	alarm", are you talking about the smoke alarm going off
25	what we can see there in this photograph, burning on the	25	in flat 16?
	Page 85		Page 87
1	edge of the kitchen window?	1	A. Yes.
2	A. Yes, I would agree with that.	2	SIR MARTIN MOORE-BICK: If we look at that picture on the
3	Q. What conclusions would you draw from the presence of	3	screen at the moment, would it be right to understand
4	that burning material in that bottom left-hand corner of	4	that the whole of the area surrounding the window is now
5	the window?	5	involved in the fire?
6	A. That clearly the ACM is already involved at that point	6	A. Potentially, although not necessarily. Cameras saturate
7	in the fire.	7	very rapidly, and then the smoke reflection and numerous
8	Q. Do you think it likely that that burning material is	8	different things. So at that distance, it will be quite
9	melted PE filler from the ACM cassettes located directly	9	hard to pinpoint exactly what sectors are actually
10	above the window?	10	burning. But because of the demarcation lines, it is
11	A. Most likely.	11	quite clear that there is a significant event going on
12	Q. Does that affect your view that the most likely route of	12	in there.
13	ignition is by flame of exposed flammable materials in	13	SIR MARTIN MOORE-BICK: All right, thank you.
14	the window surrounds?	14	MS GRANGE: If we can just finish off what Professor Bisby
15	A. Not necessarily. I think you have to keep in mind that	15	says, then. If we can go back to LBYS000001 at
16	we're talking about 01.12. So if we take the moment in	16	page 145, and look at paragraph 693.
17	which the fire was noticed by the detector, we're	17	There he says:
18	already about 17 minutes into the fire.	18	"If the external cladding was first ignited (and
19	Now, fires, before they start the period of growth,	19	sustained burning) due to heat from flames venting from
20	they sometimes have a very long incubation period where	20	the kitchen window of Flat 16 (i.e. by an external fire
21	they might be just simply simmering in there, but they	21	plume (see Drysdale [1]), one would expect to observe
22	have the capacity, depending on their location, to	22	the earliest evidence of dripping burning ACM PE filler
23	activate the detector. So the detector could have	23	originating from the location directly above the fan
24	detected the fire at that very early stage and could've	24	mounting and inward swinging kitchen window that was
		1	
25	given us maybe 5, 6. 10 minutes of incubation before the	25	located directly beneath the extract fan panel. The
25	given us maybe 5, 6, 10 minutes of incubation before the	25	located directly beneath the extract fan panel. The

dripping PE would most likely originate from directly 1 1 compartment, but there is no great motion going on. In 2 2 above the extract fan panel. However, as already noted those cases, the smoke would just simply spill and it 3 3 will be adhered to the wall. So effectively you will the available visual evidence presented in this section 4 suggests that dripping, burning PE spears to have first 4 have smoke just literally touching the walls and moving 5 been observed falling from the base of the window at its 5 6 southernmost edge." 6 Now, many times, for example, when you have a door 7 7 So would you agree with Professor Bisby in what he's open and you have some ventilation, what you get is 8 saying in that paragraph, that you would've expected the 8 a flow. So the fire acts like a pump and it pushes the 9 dripping and melting ACM, had it been as a result of the 9 smoke out, in which case you get a disattached smoke 10 flaming through the extract panel, to have been dripping 10 plume, because the smoke is pushed away by the flow that 11 and melting at the top of the window, not at the bottom 11 gets created in the compartment. 12 left-hand corner of it? 12 So in this particular case, given the fact that the 13 A. Yes, I couldn't disagree with that, which doesn't mean 13 door was closed, and given the fact that most of the 14 14 openings were closed, it is very unlikely that you had that dripping could not have been happening inside that 15 we couldn't see. So in many ways, this is the 15 high velocities inside the compartment. So it will be 16 difference between putting some physical arguments and 16 most likely that you have an adhered fire plume, in 17 other words you will have the smoke touching the --17 putting evidence from images that we need to contrast, 18 because that's really what we have. 18 Q. Sticking to the surfaces. 19 But I think the points being made are fundamentally 19 A. Sticking to the surfaces and moving out. 20 correct and they stem from visual imaging. It's 20 Q. Yes 21 information that is extremely valuable that should 21 A. So, effectively, at this point you do have ignition that 22 complement the analysis from the inside. But it's very 22 has happened of a component that is partially in, 23 23 partially out, and how that happened is very difficult difficult to put a sequence of events and say which one 24 comes first. 24 to define. 25 25 Q. Because what you're saying is you wouldn't see it if Again, the interesting thing is that this is Page 89 Page 91 1 it's come round the inside because it may have gone 1 10 minutes from the moment of the smoke alarm. So we 2 inside the column and been burning there before we 2 already have 10 minutes of gap happening in there. 3 actually see it visually on the outside. 3 So as a symptom, that the fire is emerging out of 4 4 A. Exactly. the compartment is a very clear symptom, but it's hard 5 Q. Can I take you back to another image. This is 5 to relate to anything else beyond that. 6 an earlier image at 01.05 from Mr Kebede's mobile phone. 6 Q. Do you think this sheds any light on whether there might If you go in your report to JTOS0000001 at page 56, 7 7 have been direct flame impingement from an adhered fire line 1582. If we can focus in on that image there. 8 8 plume on the external wall materials at the head of the So this is a screenshot taken from the video 9 window? 10 recovered from Mr Kebede's mobile phone at time stamp 10 I think what is being suggested is it comes out of 11 01.05.57. 11 the window where the extract fan has gone and sticks to 12 Do you agree that this image appears to show flames 12 the surface of the ACM cassette that we looked at before 13 around the extractor fan in the window of the kitchen of 13 that's immediately above the window and ignites it that 14 flat 16 and a visible fire plume behind the window? 14 way. Do you think that visual evidence helps on that? 15 A. Yes. 15 A. Well, basically what you have is a flame. Now, that 16 Q. Is it possible that a fire located by the wall or in the 16 particular flame will result in a heat flux that is 17 corner of flat 16 would've produced an adhered fire 17 applied to all that section, and effectively it is true plume? 18 18 that the flame will impinge. 19 A. Well, firstly, I guess, we need to define the concept of 19 This in size is a fairly small flame and it is 20 what an adhered fire plume is. 20 entraining a lot of air. So the question here will 21 Q. What is an adhered fire plume? 21 be: does that flame have enough heat to be able to 22 A. So when you have a fire, there is two types of 22 ignite the cassette? That question is one that we have 23 compartment fires. There are types of fires where you 23 not resolved, and I do think that probably, if that path 24 have the smoke layer that dominates the problem, in 24 is going to be followed, then that needs to be tested, 25 other words what you get is gases that fill the 25 because effectively it is not about having a flame, it's Page 90 Page 92

1	shout having a flame that is sufficiently strong to	1	norticular nacitian Effectively what you have is
1	about having a flame that is sufficiently strong to	1	particular position. Effectively what you have is
2	provide sufficient heat flux to be able to ignite the	2	a flame, and if the flame for whatever reason is tilted
3	cassette.	3	in a certain direction, it might be impinging on many of
4	Q. Just to be clear, I think both you and Professor Bisby	4	the objects that are there, and could potentially heat
5	have excluded the idea that the flame could've started	5	them up quite significantly.
6	in the extract fan and produced sufficient heat to then	6	Q. So you're talking about direct flame impingement
7	ignite the panels above; is that correct?	7	potentially could've melted the window frame and its
8	A. Yes, basically, if you do a simple analysis of the size	8	fixings. What about weakening the plastic thermal
9	of the flame, by the time you get to the cassette, even	9	disrupter that held the two-part window together?
10	if it's adhered, the heat flux will have already decayed	10	A. Everything is possible.
11	enough. That is quite unlikely that that is the only	11	Q. And the XPS core of the window infill panels, which are
12	source of ignition.	12	to the left of the kitchen window?
13	Now, if other things are burning around, then it's	13	A. Same. I mean, I think
14	a slightly different story, because you're supporting	14	Q. It's possible?
15	with an extra flame an already existing amount of heat.	15	A. Yes.
16	But just the fan by itself doesn't have the capacity to	16	Q. Melting of the components between the ends of the window
17	produce enough heat to be able to do that.	17	assemblies and the original structure.
18	Q. Just a few more questions on this topic.	18	A. These are made of aluminium, I presume.
19	I've been asked to put to you that there was	19	Q. Yes.
20	firefighter evidence from Firefighter Brown that when he	20	A. So the melting temperatures are about 600, and so you
21	was leaning out of the kitchen window and trying to	21	will have to have you know, for melting of aluminium
22	squirt the hose back at the fire, he could see flames	22	you will have to be able to demonstrate what kind of
23	travelling within the cavity.	23	size of a fire you will be able to need to get to those
24	Now, that's certainly after 01.20. Is that of any	24	temperatures. But, effectively, if you put it close
25	assistance at all in terms of this question of breakout	25	enough, you will be able to get to those temperatures.
23	assistance at an in terms of any question of freatout	20	enough, you will be able to get to those temperatures.
	Page 93		Page 95
1	from the compartment?	1	Q. I am now going to turn to some connected but different
2	A. Well, the only information that that provides is the	2	topics.
3	fact that the uPVC was gone, because he could actually	3	Compartmentation.
4	see through, and the fact that there were flames in the	4	Do you agree that a high degree of compartmentation
5	cavity, that tells you that the fire had already	5	around each flat, enclosing every surface riser, the
6	progressed into the cavity.	6	stairs, the lobbies, is the first layer in the layer of
7	So, if anything, the conclusion that you can make is	7	safety forming the basis of fire safety guidance in
8	at that point the fire service knew that the fire was in	8	high-rise buildings?
9	the cavity.	9	A. Compartmentation is the one layer that not only gives
10	Q. But does it help us at all, his evidence, about	10	you protection, but gives robustness to the strategy.
11	break-out from the compartment?	11	It's very difficult to break the compartmentation.
12	A. It's too late.	12	So it's not the first layer of protection; it is
13	Q. It's too late in time?	13	a very important layer of protection because it's the
14	A. Yes.	14	only one that really brings robustness into the system.
15	Q. Finally on this topic, I've asked you before about the	15	The other ones can all fail, and there's no recovery
16	possibility that with additional ventilation in that	16	from them. So if the smoke detector doesn't work, the
17	room, in that kitchen, for example around the doors, and	17	smoke detector does not work, while if the
18	if the fire was not in the centre of the room but in	18	compartmentation gets a crack, you might get a little
19	a corner or against a wall, whether there could've been	19	bit of a leak, but you still get a significant amount of
20		20	
	local areas within the smoke layer where temperatures	20 21	protection. So the comportmentation in itself provides that
21	could've been higher and might have melted, for example,	1	So the compartmentation in itself provides that
22	the following elements: the window frame and its	22	component of robustness that no other layer of
23	fixings is that possible?	23	protection provides.
24 25	A. Of course. I mean, it doesn't need the extra	24 25	Q. So you agree that's the critical feature in the design
23	ventilation, it doesn't need the flames to be in any	23	of high-rise buildings?
	Page 94		Page 96

1	A. For this type of high-rise building, yes, it is	1	unexpected, because it is not a flame being projected
2	a critical feature.	2	outside and not igniting anything or propagating into
3	Q. Is it your evidence that in the event of any fire	3	other spaces; it is a flame that has barely come
4	starting near a window at Grenfell Tower, there was	4	outside, but it is already creeping into the external
5	a disproportionately high probability of fire spread	5	components of the building.
6	into the cladding system?	6	Q. So that is your evidence about the time when
7	A. Absolutely.	7	compartmentation has failed.
8	Q. You've said in your report that, based on your analyses,	8	A. That's an estimate of time that I put as the end of my
9	the size of the fire that could breach the uPVC and	9	stage 1.
10	ignite the combustible materials around the window are	10	Q. Which is 01.05 to 01.08, or 01.05?
11	within a range that can be considered a feasible event	11	A. Well, 01.05 to 01.08.
12	within a residential kitchen; is that correct?	12	Q. A slightly different question: at what time do you think
13	A. Beyond that; I think it will be an event that will	13	compartmentation had visibly failed, or is it the same
14	happen inevitably in a kitchen in a residential house.	14	answer?
15	So it has what I call a probability of 1.	15	A. Well, it has clearly failed by 01.08/01.09, and there's
16	Q. Yes, I've been asked to ask you about that.	16	evidence of failure by 01.05. So between those two
17	When you say it's got a probability of 1, precisely	17	times, you have an evolution of the images, as you saw
18	what do you mean by that? You mean it's inevitable?	18	from the video, that by the time you end the minute
19	A. A fire of a frying pan is going to happen in a kitchen	19	01.08, it is very clear that you have external
20	within the life of the building, and when we design, for	20	components burning. By the time you are in 01.05, you
21	example, for compartmentation, we design for	21	have the first evidence. So you have that range of time
22	a post-flashover fire. So we accept everything smaller	22	where it becomes absolutely clear that there is external
23	than that is very highly probable, so we have to design	23	burning.
24	our compartmentation to withstand a post-flashover fire.	24	Q. Do you think that that is the point that firefighters
25	So, yes, I mean, this is an inevitable, perfectly	25	ought to have realised that compartmentation had been
	D 0-		P
	Page 97		Page 99
1	foresceable event	1	<u> </u>
1 2	foreseeable event. O You also say that because a fire of this nature can be	1 2	breached?
2	Q. You also say that because a fire of this nature can be	2	breached? A. I mean, that's a very difficult question to answer
2 3	Q. You also say that because a fire of this nature can be expected, the building is required to respond	2 3	breached? A. I mean, that's a very difficult question to answer because it is: how do you interpret the images?
2 3 4	Q. You also say that because a fire of this nature can be expected, the building is required to respond appropriately. Precisely what do you mean by that?	2 3 4	breached? A. I mean, that's a very difficult question to answer because it is: how do you interpret the images? Now, clearly firefighters are used to seeing flame
2 3 4 5	Q. You also say that because a fire of this nature can be expected, the building is required to respond appropriately. Precisely what do you mean by that?A. What I said at the beginning was that fires are very	2 3 4 5	breached? A. I mean, that's a very difficult question to answer because it is: how do you interpret the images? Now, clearly firefighters are used to seeing flame projections, because a post-flashover fire will normally
2 3 4 5 6	 Q. You also say that because a fire of this nature can be expected, the building is required to respond appropriately. Precisely what do you mean by that? A. What I said at the beginning was that fires are very common events, but fires that create significant damage 	2 3 4 5 6	breached? A. I mean, that's a very difficult question to answer because it is: how do you interpret the images? Now, clearly firefighters are used to seeing flame projections, because a post-flashover fire will normally break the window and you will have a flame projecting to
2 3 4 5 6 7	 Q. You also say that because a fire of this nature can be expected, the building is required to respond appropriately. Precisely what do you mean by that? A. What I said at the beginning was that fires are very common events, but fires that create significant damage are rare events and we design buildings to make that 	2 3 4 5 6 7	breached? A. I mean, that's a very difficult question to answer because it is: how do you interpret the images? Now, clearly firefighters are used to seeing flame projections, because a post-flashover fire will normally break the window and you will have a flame projecting to the outside.
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1	A. Yes.	1	the energy that I'm producing is being delivered to the
2	Q. Is it right that once the compartment has been breached	2	material step by step.
3	and you have ignition of the facade, it is going to be	3	So, effectively, I'm not losing energy; all the
4	undermining and invalidating of the stay-put policy?	4	energy is going to where it's supposed to go. So it is
5	A. It invalidates by definition the stay-put policy,	5	heating up the material very rapidly and allowing it to
6	because it's based on a required boxing of the fire into	6	ignite and allowing the flame to spread.
7	one compartment.	7	Now, if I'm trying to spread down, which is what we
8	Q. Is it your view at that point that once compartmentation	8	call opposed spread, then I'm producing the energy here,
9	is breached, egress or rescue rather than stay put is	9	the energy's mostly going up, and only a minute fraction
10	a preferred option?	10	is going down because all the gases are going up, no?
11	A. It is my opinion that that will be the case.	11	So effectively what you're getting is very weak spread
12	Q. I now want to turn to stage 2 of your analysis.	12	because you have very little energy heating up the
13	You have stage 2 as covering the fire ascending to	13	material and bringing it to ignition.
14	the top of the east elevation and the associated	14	If you spread laterally, in that case what you have
15	vertical fire spread, and that's between approximately	15	is the heat is going up and you're trying to heat on the
16	1.05 am and 1.30 am; is that correct?	16	side. Obviously the flames are sometimes going to tilt,
17	A. Yes.	17	so you're going to get a slightly better condition, but
18	Q. I want to consider first the importance of this vertical	18	still, you are going against the flow because the flow
19	fire spread.	19	is coming here and bringing the heat up.
20	You say in your report that the flame spreads	20	So because all the heat is going in the direction of
21	rapidly from level 4 to the architectural roof detail in	21	spread, vertical spread is going to be significantly
22	approximately 12 to 15 minutes from the establishment of	22	faster than downward spread or lateral spread. Both
23	flames on the facade; is that correct?	23	cases are what we call opposed flame spread, where this
24	A. Yes.	24	is what we call forward spread.
25	Q. You also say that, in general, vertical flame spread is	25	The final nuance to this is that if I don't have
	Page 101		Page 103
1	much faster than horizontal flame spread, and this was	1	enough energy, it will not spread, while with vertical.
1 2	much faster than horizontal flame spread, and this was the case at Grenfell Tower; is that right?	1 2	enough energy, it will not spread, while with vertical, I will always have enough energy because all the
1 2 3	the case at Grenfell Tower; is that right?	2	I will always have enough energy because all the
2	the case at Grenfell Tower; is that right? A. Yes.		I will always have enough energy because all the energy's going there, it just takes longer. So if this
2	the case at Grenfell Tower; is that right?	2 3	I will always have enough energy because all the energy's going there, it just takes longer. So if this was a weaker fire, it will take slightly longer, but
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2 3 4 5 6	the case at Grenfell Tower; is that right? A. Yes. Q. We heard something about this when Professor Bisby gave his presentation back in June, but can you explain again in simple terms why vertical fire spread is expected to be so much faster?	2 3 4 5 6	I will always have enough energy because all the energy's going there, it just takes longer. So if this was a weaker fire, it will take slightly longer, but eventually it will get there. But here, because I'm fighting against cold air, I might not have enough energy, so it actually will not spread.
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1	Control of the contro	١,	
1	fast enough laterally by the time you've burned out all	1	Can you just explain to us here we seem to have
2	the material, then you stop having the energy supply and	3	lots of different fires at the bottom, and then what do we see in the graph?
4	then it stops burning. So depending on what is the amount of fuel that you have, you will have a longer	4	A. Yes, so what you see in the horizontal axis is the
5	time to assist the spread. So if you don't have very	5	different events from the Andraus building in 1972 all
6	much fuel, which is normally the case in this particular	6	the way to the Grenfell Tower, and then you get
7	type of installations, then you will not be able to	7	an average vertical external flame spread.
8	spread horizontally or downwards.	8	Given that the quality of the images is not always
9	Q. You've given some examples of what you were just talking	9	consistent, what we opted to do here was just take a few
10	about. Can we go to those at figure 21. That's	10	data points that we could actually see and then just
11	JTOS0000001, at page 59.	11	take an average, knowing that normally the flame spread
12	So you've given us three examples here: The Torch	12	starts slower and then it starts speeding up, so it
13	building in Dubai, the Lacrosse building fire in	13	accelerates at the end, but we didn't include that.
14	Melbourne and The Address building in Dubai.	14	That's why we have the error bars in there to show that,
15	Can you briefly talk us through each of those by	15	for example, the case of the Water Club, the maximum
16	reference to this concept of vertical flame spread, much	16	value was 25, the minimum value was 5. So it gives you
17	more rapid, and less horizontal flame spread.	17	a sense of the range. But the average value is the one
18	A. Yes. The most clear ones are the top two, so it would	18	that is important.
19	be The Torch and the Lacrosse building.	19	So as you can see, Grenfell falls in the category of
20	So as you can see, in The Torch building you have	20	the fires that actually spread slower.
21	a very large fire that propagates upwards, and on the	21	Q. So we have Grenfell on the bottom right hand here, and
22	right-hand figure you will see in the left corner	22	it's placed amongst some of the slowest vertical fire
23	it's unfortunately a different angle the damaged area	23	spread rates.
24	of the building, and you can see the very narrow strip	24	A. Yes, with an average speed of about 4 metres per minute,
25	that has propagated all the way from the bottom to the	25	as opposed to the extreme case of The Address, for
			D 40-
	Page 105		Page 107
1	top.	1	example, where you have about 22 metres per minute.
2	In the case of the Lacrosse building, you have	2	Q. You've said in your report that the expected heat fluxes
3	a fire that starts in a balcony, in an air conditioning	3	on an external wall can be of a magnitude of
4	unit, and it spreads over the cladding all the way to	4	120 kilowatts per metre squared; is that correct?
5	the top. But as you can see from the right picture,	5	A. Yes.
6	there's only one row of apartments that gets affected	6	Q. Can you explain very briefly how you've calculated that?
7	and it never spreads laterally.	7	You've referred to the Agarwal global research technical
8	In the case of The Address, it's slightly more	8	report. Is it right that you've taken that as
9	complicated because there is a bit of lateral flame	9	an extrapolation from that report?
10	spread in the case of The Address because, as you can	10	A. Yes. So, effectively, if you look at the data that you
11	see, it was a windy day, so the wind is carrying the	11	have on internal compartment fires, you will find that
12	flames to the one side. But the rate at which it	12	internally you can get above 200 kilowatts per metre
13	propagated vertically was easily much more than ten	13	squared. So inside the compartment, you're going to
14	times greater than the lateral spread, and eventually	14	have about 200. Once that heat starts coming out, it
15	this fire dies on its own before it actually manages to	15	starts decaying, and it drops.
16	go more than two and a half apartments.	16	So this report by Agarwal effectively tries to use
17	Q. You said the available footage from these incidents	17	that information to create a test, and in their test,
18	indicates that once flames spread to the top, they	18	they try to create a profile of how this heat flux is
19	proceed to decay and eventually extinguish; is that	19	going to decay. So it's going to go from this
20	right?	20	originally more than 200 inside and start dropping until
21	A. Yes.	21	it goes to about 5 or something lower than that.
22	Q. You've actually quantified the flame spread rates in	22	So they produce a curve that stops at about
23	those other international fires compared with Grenfell.	23	15 centimetres from the edge, or from the bottom, and
24 25	Can we just look at that. That's figure 23, at page 61 of your report.	24	that 15 centimetres is at about 112 kilowatts. So
23	or your report.	25	basically I just filled it up and put above 120, because
	Page 106		Page 108

1	I know it has to go from about 200, you know, to 110 in	1	Q. Please do.
2	that corner or that little part.	2	A. So, to me, this is where the great complexity of the
3	Q. I now want to discuss some of the architectural elements	3	system stands, in the sense that you have multiple
4	that might impact on the rate of vertical flame spread.	4	layers, so you have the concrete structure in here, you
5	You've explained in your report that there's	5	have a material that is a charring material that
6	a complex interrelationship between a number of	6	eventually is going to consume itself, you have a gap
7	different elements of these kind of systems in terms of	7	between the two of them and then you have a composite
8	the impact on vertical flame spread; is that correct?	8	system that has two layers of aluminium plus the
9	A. Yes.	9	polyethylene in the middle.
10	Q. And that you've got effectively multiple processes	10	This polyethylene is going to melt as it heats up.
11	interacting with one another.	11	The rate at which it heats up in the aluminium is going
12	A. Yes.	12	to result in altering the rate at which it's going to
13	Q. Can we focus for a moment on the ACM panels themselves.	13	melt. So how this material is going to start falling
14	Can we go to the text of your report, that's	14	off is going to depend on how fast the heat goes through
15	JTOS0000001, page 60, lines 1649 and 1651.	15	the aluminium.
16	If we can just read that. You say there:	16	Now, how fast the heat goes through the aluminium
17	"The polyethylene infill was placed between two	17	depends on if you have a fire inside or you have a fire
18	aluminium plates that will melt in the range 580 -	18	outside. It depends on the wind that you have, it
19	650°C. Thus, in the presence of a significant flame the	19	depends on the width of the cavity, and it depends on
20	aluminium would have represented no protection to the	20	how the insulation is burning.
21	polyethylene. Flames are typically between 600°C-800°C,	21	So, effectively, you have all these systems of
22	thus are hotter than the melting temperature of	22	incredible complexity all interacting with each other to
23	aluminium."	23	try to give you the final outcome, and eventually the
24	Is that correct?	24	system is so complex in nature that it's almost
25	A. Yes.	25	impossible to predict what is its true behaviour.
	Page 109		Page 111
	1.100		150 111
1	Q. So you've explained in your report that the high thermal	1	Q. So when we were talking a moment ago about these complex
2	conductivity of the aluminium is resulting in a heat	2	systems with multiple processes interacting, that's what
3	transfer to the polyethylene infill; is that correct?	3	you're trying to show in this diagram; is that right?
4	A. And also away.	4	A. Absolutely. So this diagram basically gives you
5	Q. Away from it as well?	5	a schematic that is actually quite simplified of all the
6	A. Yes.	6	different processes that you can actually have all
7	Q. And the significance of the away from it?	7	interacting with each other in one of these particular
8	A. That it can potentially melt it and produce a gap that	8	systems.
9	splits the two panel faces.	9	Q. One of the things you say in your report is that the
10	Q. Exactly. We're just going to come to the splitting in	10	aluminium provides no protection to the polyethylene
11	a moment.	11	inside. Can you explain precisely why that is?
12	In fact, let's go to that. Let's took at your	12	A. Yes. So if you have a flame here, and that is a very
13	figure 26. Again, there's a new reference to that	13	significant flame that has already been established,
14	because the version in your report is not very clear.	14	that flame is going to have heat fluxes that are quite
15	That's JTOS0000003, the bottom diagram.	15	significant and can bring the aluminium far above its
16	So here, as I understand it, you've attempted to	16	melting temperature. So you might have dripping of the
17	explain what processes are occurring when we get	17	aluminium.
18	vertical flame spread with an ACM panel where you have	18	Not only that, you're going to have melting of the
19	aluminium on the outside and then the polyethylene on	19	polyethylene, which results in splitting. So you will
20	the inside; is that correct?	20	have the two of them separating, so the flames are going
21	A. Yes.	21	to creep inside. So the aluminium cannot be seen once
22	Q. You talked a moment ago about the splitting you've	22	the flame is established as a protection to the
23	got a little diagram there can you just explain that	23	polyethylene, it is just simply a barrier that is going
24	and the significance of it?	24	to disappear very rapidly once you have a flame that is
25	A. Yes. Would you mind if I actually stand up and point?	25	established.
	D 440		D 112
	Page 110	1	Page 112

1 1 Q. You've also highlighted in your report the important the flame spread, but I'm not 100 per cent sure if it's 2 role of these open vertical cavities, these open 2 going to be detrimental or positive. But the cavity 3 vertical columns. 3 clearly has an effect. 4 You've said that the acceleration of vertical fire 4 Q. Does it have an effect -- we're going to talk about this 5 5 spread can be explained in part by these channels in a moment -- combined with the PIR insulation? If you 6 producing chimney effects. 6 have a cavity where the insulation is on fire or 7 7 flaming, does the fact that you have a cavity there 8 Q. Is that because flames elongate possibly up to five to 8 potentially grow in importance? 9 9 ten times in a concealed space; is that right? A. Well, absolutely. Well, I think that if you have 10 A. Well, what happens is that, depending on the size of 10 a cavity in here, and you have a material here, you're 11 this gap, if this gap is too narrow, it's going to block 11 going to hit an exchange of heat between these two. So 12 12 the oxygen and the flame is going to try to creep not only the PIR is going to support burning within the 13 outside. In that case, it will not spread. 13 cavity, but actually the cavity and the burning in the 14 14 Now, as I start increasing this, what you create is cavity is going to support the burning of the PIR. 15 a chimney effect, and this flow becomes very dominant. 15 PIR requires a fairly significant heat flux to 16 So you get a flow that is going in that direction and is 16 continue to burn. So if I was to remove everything and 17 carrying the fuel away, so it's elongating the flame and 17 eliminate the cavity, it is very likely that the PIR 18 allowing it to spread much faster. 18 will extinguish. But if I put all this ensemble, and 19 Q. You say that the width of the cavity is playing 19 I have this exchange of heat between all the surfaces 20 a fundamental role in terms of determining the flame 20 and the flow and the burning in between the cavity, 21 21 I can sustain the burning of the PIR. spread? 22 A. Absolutely. So if you make the width of the cavity 22 So all these things are playing with each other in 23 23 very, very small, you might end up choking the fire this system at a level of complexity that is incredibly 24 because the air cannot get in, but as you start opening 24 difficult to come up with a prediction of what leads to 25 2.5 it up, you might accelerate it. But as everybody knows, what. Page 113 Page 115 1 Q. We will come on in a moment -- and we may have to do it 1 if you make a chimney too big, it doesn't draw the air, 2 so in that case you will start decaying again. 2 after the break -- to look at the PIR in a bit more 3 detail. 3 So it's a very sensitive parameter that can have 4 4 You've referred in your report to other complex a huge impact on the outcome. But it's difficult to 5 know if it's going to be beneficial or detrimental, 5 geometries of the system that might affect the rate of 6 because it also depends on all the other interplay. 6 fire spread. 7 7 Would you agree that angular geometry, including, For example, if this material burns very vigorously, 8 it's going to have a huge impact on the temperature in 8 for example, wing walls or re-entrant corners, might g here and the nature of the chimney. q have played a role? 10 10 Q. We're going to come to that material in a moment. So take, for example, column corners, where we have 11 When you say "this material", you were pointing 11 an angle of 135 degrees as between the column and then 12 there, I think, to the PIR insulation; is that right? 12 the face of the spandrels. 13 A. Yes. 13 A. It would have most definitely played a role. I think 14 Q. We'll come to that just in a moment. 14 the most difficult question to answer is: would it 15 Have you specifically considered the width of the 15 actually help the spread or deter the spread? That's 16 cavities created by both the columns and the spandrels 16 a question I have no capability to answer. 17 at Grenfell Tower in terms of its impact on vertical 17 Q. How could it have deterred the spread? 18 flame spread? 18 A. Because if you look at the geometry, it is all about how 19 A. No, I don't think I have the capacity to be able to 19 the heat is being exchanged. So if I have something, 20 consider that in a quantitative way and establish how 20 for example, that has an angle like this (Indicates), 21 that width is going to determine a flame spread. 21 then the way in which the heat is being transferred from 22 Q. Do you think that, in general terms, the presence of 22 one surface to the other one is actually far. So if 23 that cavity would've promoted vertical flame spread? 23 it's sufficiently far, this might not have ignited, in 24 A. Not necessarily. I do not have a clear opinion of it. 24 which case it represents a barrier. 25 I think clearly it would have influenced the nature of 25 But if I slightly move it, and I put it close enough

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1	and then it ignites then the two of them are evaluating	1	with most other intermetional events, and you see that
1 2	and then it ignites, then the two of them are exchanging	2	with most other international events, and you see that
	heat with each other, in which case it will become much	3	actually the spread rate is not among the fastest, it's
3	faster.	4	actually on the lower end, you can tell that all these
4 5	So it really depends on the detailed	5	things more or less worked okay to try to slow the
	characteristics. And many times, unfortunately, it will	6	spread. But effectively they didn't solve the main
6	be even coupled to the conditions of the day. If it was		problem, which is the fact that we had a combination of
7	a windy day, maybe 130 degrees would not be enough, you	7 8	materials that could sustain the problem.
8	would need 140 to stop the spread.	9	So I could've put many other of these little
9	So all these things we can really not ignore the		corrections and probably would've not made even any
10	level of complexity of what we're talking about. This	10	improvement, and some of the faults that you might find
11	really is not a very simple system, it's an incredibly	11	in some of the components might have not been
12	complex system.	12	responsible for any worse behaviour. What we can see is
13	Q. As we discussed before, the presence of films or skins	13	that given the type of materials that we have, we are
14	or coatings on material, they have the potential to	14	more or less at the baseline of the type of spread that
15	affect the vertical flame spread?	15	we're going to have.
16	A. Absolutely. Films that are combustible are what we call	16	Q. So you're saying that the important thing is the
17	thermally thin. Materials like paper. So, for example,	17	material composition of those materials
18	a log of wood is thermally tick, and a log of wood will	18	A. Yes.
19	have a very, very hard time burning on its own because	19	MS GRANGE: here, yes.
20	it's a big bulk of material. So if I take the log of	20	Sir, I think that is an appropriate moment.
21	wood out of the chimney, it will extinguish, while	21	SIR MARTIN MOORE-BICK: Is that a good point?
22	a piece of paper, which has the same composition as	22	MS GRANGE: Yes.
23	a log of wood, because it's very thin, it will burn very	23	SIR MARTIN MOORE-BICK: Well, time we had a break for some
24	easily.	24	lunch, professor. So we'll stop now and we'll come back
25	So thin films, when they're combustible, will have	25	and resume at 2 o'clock.
	Page 117		Page 119
1	a cignificant impact on appending flames	1	Again. I'm gaing to ask you not to talk to anyone
1	a significant impact on spreading flames.	1	Again, I'm going to ask you not to talk to anyone
2	Q. Just to round this off, then, can we just go to what you	2	about your evidence while you're out of the room.
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1	Q. You agreed with me that once compartmentation is	1	big residue of carbon, and that big residue of carbon is
2	breached, evacuation becomes the preferred option; yes?	2	going to eventually lead to extinguishment of the
3	A. When vertical compartmentation yes, when the fire	3	material itself. It's going to stop burning on its own.
4	starts spreading beyond the floor of origin.	4	Q. You've explained in your report that the features of the
5	Q. Would you agree that once compartmentation is breached,	5	PIR give rise to the potential to burn for a much longer
6	evacuation is necessary to secure the fire safety of	6	time period.
7	those in the building?	7	Again, first of all, what data or other information
8	A. Yes.	8	have you relied upon when you say that the PIR has the
9	Q. Is it the only viable option at that point?	9	potential to burn for longer periods?
10	A. Yes.	10	A. Well, this is relative, and the reason why it's relative
11	Q. I just want to return to the importance of the PIR	11	is because the duration of burning is a function of the
12	insulation. We were just talking about it before the	12	total mass that burns. So if you have a certain
13	break.	13	thickness of PIR, that will give you a certain amount of
14	Just to be clear, just to kind of remind ourselves,	14	mass, and that certain amount of mass will determine how
15	there was PIR insulation behind the spandrel panels, the	15	long it's going to burn.
16	ACM panels, in two layers of 80 millimetres, and also	16	Now, obviously, the mass that you're considering is
17	a single layer of 100 millimetres on the columns. That	17	the fraction that burns, not the fraction that remains
18	was Celotex RS5000 PIR insulation.	18	as char. So when you compare the amount of mass that
19	There was some Kingspan K15 phenolic foam boards	19	you have of PIR, compared to other combustible materials
20	also used on some of the spandrels, also that's possibly	20	like polyethylene or the EDPM, the mass of PIR is more
21	only about 7 per cent of the total insulation. Just to	21	significant and, therefore, it has a propensity to
22	be clear what we're talking about here.	22	remain burning for a fairly long period of time relative
23	A. Yes.	23	to the other materials.
24	Q. As we've discussed, PIR has a low thermal inertia, and	24	Q. Can you just explain your view about the interaction
25	you've agreed that that means a low time to ignition.	25	that we may have got on the building between the ACP
	Page 121		Page 123
	W. I. J. Harris M. D. Harris H.	١.	1 14 PM : 14 a
1	You've also said that the PIR is liable to char.	1	panels and the PIR insulation?
2	A. Yes.	2	You talk, for example, about radiative feedback.
3	Q. Can you explain what impact those features of the PIR	3	Can you just explain what radiative feedback is as between those two?
4	ie low thermal inertia and propensity to char have on	4	
5	flame spread?	5	A. Yes. As I mentioned, the PIR by itself, it will
6	A. Yes. The low thermal inertia results in very little	6 7	self-extinguish. So effectively the char layer forms and, unless you put an external heat to try to keep the
7	energy required to ignite the material. All the energy	8	
8	gets stuck very close to the surface. So with very	9	burning going, it will just fade out and die. So when
10	little energy, you can bring the surface to	10	you have the polyethylene burning in front, that
	a temperature of ignition and it starts burning.	11	polyethylene provides that extra source of heat. That's
11 12	When a charring material starts degrading and burning, it produces a layer of carbon that effectively	12	what we call radiative feedback. So between the two of them, they are supporting each other.
13	starts protecting the material behind.	13	So what we see in the images of the burning of the
14	So as opposed to a non-charring material that will	14	tower, it's quite complex in the sense that there is
15	burn completely, this material will burn only a fraction	15	different forms of behaviour. There's certain areas
16	and the layer that is produced prevents the heat from	16	where you have fairly intense burning, where that
17	burning any further.	17	radiative feedback is having both materials burning
18	So you need to have some heat from the outside to	18	quite significantly. But then, later on, when you see
19	help it burn. The moment you remove the heat from the	19	the PE has disappeared, then you will have
20	outside, it tends to extinguish on its own because,	20	self-extinction of the PIR and you get residue of
21	effectively, no heat can get from the flame to the fuel	21	unburnt PIR left behind.
22	to keep evaporating the fuel.	22	So eventually you will get multiple forms of
23	So the charring has one fundamental outcome, which	23	interaction, and the question if it's going to continue
24	is that it will reduce the fraction of the mass of the	24	burning or not continue burning is a question of how the
25	material that is actually going to burn and leave this	25	two of them are interacting in any particular location.
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	Daga 122	1	Daga 124

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1	Q. How does the PIR affect the rate at which the aluminium	1	right now, the particular tests that are being
2	composite panels burn?	2	conducted, and that's BS 8414, is a test that in many
3	A. That is a very difficult question to answer, but	3	ways doesn't give enough detail to be able to come up to
4	I believe that it is likely that the PIR will have	4	any real conclusions. It doesn't have adequate
5	a minor effect on the rate of burning, because the	5	instrumentation and the scenario is a scenario that
6	polyethylene, being thermally thin, once it ignites and	6	doesn't really honour the complexity of the system.
7	starts spreading, it will spread at a much faster rate	7	Q. So in terms of those DCLG tests after Grenfell using the
8	than the PIR.	8	mineral wool insulation, what significance do you place
9	So the support that the PIR can provide to the rate	9	on the results of those tests?
10	of spread is probably of secondary importance.	10	A. I would say very little.
11	Q. Why does the fact that they're going to burn out at	11	Q. You've said it's very difficult to quantify the impact
12	different stages matter in terms of the development of	12	that the PIR insulation had.
13	this fire?	13	At this stage, in terms of your preliminary view,
14	A. Because one determines the rate at which it spreads, the	14	can you give an overall view as to whether you think it
15	other determines how long it's going to be burning. So	15	had a contribution and, if so, broadly in what respect?
16	while the second one is still burning, dripping and all	16 .	A. It clearly did have a contribution, but I would not be
17	sorts of other potential interactions that can happen	17	able to say what kind of a contribution it had, if it
18	between the two of them can extend the duration of	18	was very significant or mildly significant. But clearly
19	burning at any localised space. So effectively it's	19	there is burning of the PIR and there's evidence that it
20	that interaction, that one is determining the speed at	20	had been contributing to the energy that is being
21	which it's propagating, the other one is basically	21	released.
22	keeping that area burning.	22	But to quantify that to the extent of being able to
23	Q. Just briefly, because we'll get into testing in much	23	say how important that was is still not very clear.
24	more detail at Phase 2, Professor Bisby has drawn	24	Q. In terms of the state of the building after the fire,
25	attention to the DCLG tests after Grenfell which	25	would you attach any significance to any areas where,
	Page 125		Page 127
1	compared PIR with mineral wool insulation but using	1	despite extensive charring of the insulation, the ACM
2	otherwise similar materials to Grenfell.	2	remains intact? Does that tell us anything?
2 3	otherwise similar materials to Grenfell. Do you agree that a complex but different	2 3	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those
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2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	otherwise similar materials to Grenfell. Do you agree that a complex but different interaction will also apply to a system incorporating a mineral fibre insulation and a PE-cored ACM? A. Yes. It will be a different interaction because the mineral material will not burn by itself. Nevertheless, it still has the capacity of insulating; in other words, it can support the continuous burning of the ACM, and also it can absorb dripping fuel and it can serve as a wick to keep things burning. So there will be other forms of interactions that the mineral wool will have with the ACM that could potentially lead to no difference or a significant difference, depending on the characteristics of the assembly. Q. Would you say that the current evidence is inconclusive on the precise role played by the presence of the PIR at Grenfell and that further testing would be helpful?	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those situations where the complexity of the interactions is such that there might have been a convergence of different things that effectively led to an area where the insulation burnt first and then the ACM never caught fire. So that is a possibility. A very good example would be areas that were wetted by the firefighters, for example. Q. Yes, I was going to ask you. For example, on level 3 it's been suggested that there were some areas where there was deep widespread charring to the insulation but where damage to the ACM panels were much more minor, insignificant. That's level 3. Does that tell you anything? A. The only thing that I could probably conclude from that is that there was some element of cooling going on, and that would have the cooling wouldn't get to the
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	otherwise similar materials to Grenfell. Do you agree that a complex but different interaction will also apply to a system incorporating a mineral fibre insulation and a PE-cored ACM? A. Yes. It will be a different interaction because the mineral material will not burn by itself. Nevertheless, it still has the capacity of insulating; in other words, it can support the continuous burning of the ACM, and also it can absorb dripping fuel and it can serve as a wick to keep things burning. So there will be other forms of interactions that the mineral wool will have with the ACM that could potentially lead to no difference or a significant difference, depending on the characteristics of the assembly. Q. Would you say that the current evidence is inconclusive on the precise role played by the presence of the PIR at Grenfell and that further testing would be helpful? A. Yes, I think that while it is clear that some level of	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those situations where the complexity of the interactions is such that there might have been a convergence of different things that effectively led to an area where the insulation burnt first and then the ACM never caught fire. So that is a possibility. A very good example would be areas that were wetted by the firefighters, for example. Q. Yes, I was going to ask you. For example, on level 3 it's been suggested that there were some areas where there was deep widespread charring to the insulation but where damage to the ACM panels were much more minor, insignificant. That's level 3. Does that tell you anything? A. The only thing that I could probably conclude from that is that there was some element of cooling going on, and that would have the cooling wouldn't get to the insulation, so the insulation might still have been
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	otherwise similar materials to Grenfell. Do you agree that a complex but different interaction will also apply to a system incorporating a mineral fibre insulation and a PE-cored ACM? A. Yes. It will be a different interaction because the mineral material will not burn by itself. Nevertheless, it still has the capacity of insulating; in other words, it can support the continuous burning of the ACM, and also it can absorb dripping fuel and it can serve as a wick to keep things burning. So there will be other forms of interactions that the mineral wool will have with the ACM that could potentially lead to no difference or a significant difference, depending on the characteristics of the assembly. Q. Would you say that the current evidence is inconclusive on the precise role played by the presence of the PIR at Grenfell and that further testing would be helpful? A. Yes, I think that while it is clear that some level of interaction exists, it is not really clear exactly what	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those situations where the complexity of the interactions is such that there might have been a convergence of different things that effectively led to an area where the insulation burnt first and then the ACM never caught fire. So that is a possibility. A very good example would be areas that were wetted by the firefighters, for example. Q. Yes, I was going to ask you. For example, on level 3 it's been suggested that there were some areas where there was deep widespread charring to the insulation but where damage to the ACM panels were much more minor, insignificant. That's level 3. Does that tell you anything? A. The only thing that I could probably conclude from that is that there was some element of cooling going on, and that would have the cooling wouldn't get to the insulation, so the insulation might still have been burning through the cavity, while the external part of
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	otherwise similar materials to Grenfell. Do you agree that a complex but different interaction will also apply to a system incorporating a mineral fibre insulation and a PE-cored ACM? A. Yes. It will be a different interaction because the mineral material will not burn by itself. Nevertheless, it still has the capacity of insulating; in other words, it can support the continuous burning of the ACM, and also it can absorb dripping fuel and it can serve as a wick to keep things burning. So there will be other forms of interactions that the mineral wool will have with the ACM that could potentially lead to no difference or a significant difference, depending on the characteristics of the assembly. Q. Would you say that the current evidence is inconclusive on the precise role played by the presence of the PIR at Grenfell and that further testing would be helpful? A. Yes, I think that while it is clear that some level of interaction exists, it is not really clear exactly what is the level of interaction that is occurring, and it's	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those situations where the complexity of the interactions is such that there might have been a convergence of different things that effectively led to an area where the insulation burnt first and then the ACM never caught fire. So that is a possibility. A very good example would be areas that were wetted by the firefighters, for example. Q. Yes, I was going to ask you. For example, on level 3 it's been suggested that there were some areas where there was deep widespread charring to the insulation but where damage to the ACM panels were much more minor, insignificant. That's level 3. Does that tell you anything? A. The only thing that I could probably conclude from that is that there was some element of cooling going on, and that would have the cooling wouldn't get to the insulation, so the insulation might still have been burning through the cavity, while the external part of the ACM was being protected by the water from the
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	otherwise similar materials to Grenfell. Do you agree that a complex but different interaction will also apply to a system incorporating a mineral fibre insulation and a PE-cored ACM? A. Yes. It will be a different interaction because the mineral material will not burn by itself. Nevertheless, it still has the capacity of insulating; in other words, it can support the continuous burning of the ACM, and also it can absorb dripping fuel and it can serve as a wick to keep things burning. So there will be other forms of interactions that the mineral wool will have with the ACM that could potentially lead to no difference or a significant difference, depending on the characteristics of the assembly. Q. Would you say that the current evidence is inconclusive on the precise role played by the presence of the PIR at Grenfell and that further testing would be helpful? A. Yes, I think that while it is clear that some level of interaction exists, it is not really clear exactly what is the level of interaction that is occurring, and it's actually even less clear what would've been the outcome	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those situations where the complexity of the interactions is such that there might have been a convergence of different things that effectively led to an area where the insulation burnt first and then the ACM never caught fire. So that is a possibility. A very good example would be areas that were wetted by the firefighters, for example. Q. Yes, I was going to ask you. For example, on level 3 it's been suggested that there were some areas where there was deep widespread charring to the insulation but where damage to the ACM panels were much more minor, insignificant. That's level 3. Does that tell you anything? A. The only thing that I could probably conclude from that is that there was some element of cooling going on, and that would have the cooling wouldn't get to the insulation, so the insulation might still have been burning through the cavity, while the external part of the ACM was being protected by the water from the firefighters.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	otherwise similar materials to Grenfell. Do you agree that a complex but different interaction will also apply to a system incorporating a mineral fibre insulation and a PE-cored ACM? A. Yes. It will be a different interaction because the mineral material will not burn by itself. Nevertheless, it still has the capacity of insulating; in other words, it can support the continuous burning of the ACM, and also it can absorb dripping fuel and it can serve as a wick to keep things burning. So there will be other forms of interactions that the mineral wool will have with the ACM that could potentially lead to no difference or a significant difference, depending on the characteristics of the assembly. Q. Would you say that the current evidence is inconclusive on the precise role played by the presence of the PIR at Grenfell and that further testing would be helpful? A. Yes, I think that while it is clear that some level of interaction exists, it is not really clear exactly what is the level of interaction that is occurring, and it's actually even less clear what would've been the outcome in the absence of one or the other.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those situations where the complexity of the interactions is such that there might have been a convergence of different things that effectively led to an area where the insulation burnt first and then the ACM never caught fire. So that is a possibility. A very good example would be areas that were wetted by the firefighters, for example. Q. Yes, I was going to ask you. For example, on level 3 it's been suggested that there were some areas where there was deep widespread charring to the insulation but where damage to the ACM panels were much more minor, insignificant. That's level 3. Does that tell you anything? A. The only thing that I could probably conclude from that is that there was some element of cooling going on, and that would have the cooling wouldn't get to the insulation, so the insulation might still have been burning through the cavity, while the external part of the ACM was being protected by the water from the firefighters. Q. What about any evidence on the corner columns where
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	otherwise similar materials to Grenfell. Do you agree that a complex but different interaction will also apply to a system incorporating a mineral fibre insulation and a PE-cored ACM? A. Yes. It will be a different interaction because the mineral material will not burn by itself. Nevertheless, it still has the capacity of insulating; in other words, it can support the continuous burning of the ACM, and also it can absorb dripping fuel and it can serve as a wick to keep things burning. So there will be other forms of interactions that the mineral wool will have with the ACM that could potentially lead to no difference or a significant difference, depending on the characteristics of the assembly. Q. Would you say that the current evidence is inconclusive on the precise role played by the presence of the PIR at Grenfell and that further testing would be helpful? A. Yes, I think that while it is clear that some level of interaction exists, it is not really clear exactly what is the level of interaction that is occurring, and it's actually even less clear what would've been the outcome	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	remains intact? Does that tell us anything? A. Not really. I mean, once again, it is one of those situations where the complexity of the interactions is such that there might have been a convergence of different things that effectively led to an area where the insulation burnt first and then the ACM never caught fire. So that is a possibility. A very good example would be areas that were wetted by the firefighters, for example. Q. Yes, I was going to ask you. For example, on level 3 it's been suggested that there were some areas where there was deep widespread charring to the insulation but where damage to the ACM panels were much more minor, insignificant. That's level 3. Does that tell you anything? A. The only thing that I could probably conclude from that is that there was some element of cooling going on, and that would have the cooling wouldn't get to the insulation, so the insulation might still have been burning through the cavity, while the external part of the ACM was being protected by the water from the firefighters.

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1	the panels, suggesting that the fire was burning behind	1	any kind of correlation between them because one of the
2	the panels rather than on the exterior? Does that have	2	terrible things about most of these incidents is that
3	any significance in terms of the contribution of the two	3	they were very poorly investigated, and none of the
4	materials?	4	information was ever made public. So it's very
5	A. Well, it's significant in the sense that it actually	5	difficult to come up with a good correlation of what was
6	does show that the PIR at least to a certain extent can	6	in each of these events.
7	actually burn in the absence of the ACM.	7	Q. Do you know whether any of them featured mineral fibre
8	Now, the real question is I mean, you might have	8	insulation as opposed to a PIR-type insulation?
9	soot deposition after the fact, but that could've just	9	A. I wouldn't know.
10	simply been from a very, very short period of burning.	10	Q. Let's move on, then. I want to ask you some questions
11	So the PIR could have extinguished very rapidly and we	11	about the white window infill panels for a moment.
12	would not have been able to tell that unless we did	12	Just, again, to orientate ourselves as to what we're
13	a very systematic analysis of cross-sections to see the	13	talking about, can we look at a figure in your report,
14	charring thickness.	14	figure 24, that's JTOS0000001 at page 62. If we can
15	Q. Do you think it would be helpful or, indeed, practicable	15	focus on figure 24 at the top of that, it's the
16	to do a survey of the insulation to try to work out what	16	right-hand image.
17	remained after the fire versus what remained of the ACM	17	So the white infill panels we're talking about are
18	or other components? Do you think that would be a	18	the ones we can see down on the bottom right-hand side;
19	helpful exercise?	19	is that right?
20	A. I do believe so, because in many ways the interactions	20	A. Yes.
21	between the two materials or the two systems are	21	Q. That are in between the windows in each of the flats.
22	relatively unknown, and it will be very important to be	22	These were extruded polystyrene, is that your
23	able to establish if one can burn without the other one	23	understanding?
24	and to what extent that can happen. All those details	24	A. Yes.
25	can only be done with a very detailed and general survey	25	Q. Often referred to as XPS, extruded polystyrene?
	Page 129		Page 131
1	of the remnants of the insulation.	1	A. Yes.
1 2	of the remnants of the insulation. Q. Is that something you think could be done at Phase 2,	1 2	A. Yes.Q. Dr Lane has estimated in her report that these panels
		1	
2	Q. Is that something you think could be done at Phase 2,	2	Q. Dr Lane has estimated in her report that these panels
2 3	Q. Is that something you think could be done at Phase 2, based on the existing evidence?	2 3	Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external
2 3 4	Q. Is that something you think could be done at Phase 2, based on the existing evidence?A. Well, I mean, I think if the insulation was available	2 3 4	Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23.
2 3 4 5	Q. Is that something you think could be done at Phase 2, based on the existing evidence?A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be	2 3 4 5	Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding?
2 3 4 5 6	Q. Is that something you think could be done at Phase 2, based on the existing evidence?A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done.	2 3 4 5 6	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes.
2 3 4 5 6 7	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. 	2 3 4 5 6 7	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his
2 3 4 5 6 7 8	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we 	2 3 4 5 6 7 8	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of
2 3 4 5 6 7 8 9	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire 	2 3 4 5 6 7 8 9	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C
2 3 4 5 6 7 8 9	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM 	2 3 4 5 6 7 8 9	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct?
2 3 4 5 6 7 8 9 10	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? 	2 3 4 5 6 7 8 9 10	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes.
2 3 4 5 6 7 8 9 10 11	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately 	2 3 4 5 6 7 8 9 10 11 12	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just
2 3 4 5 6 7 8 9 10 11 12 13	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires	2 3 4 5 6 7 8 9 10 11 12 13	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right?
2 3 4 5 6 7 8 9 10 11 12 13 14	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from 	2 3 4 5 6 7 8 9 10 11 12 13 14	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low
2 3 4 5 6 7 8 9 10 11 12 13 14 15	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. 	2 3 4 5 6 7 8 9 10 11 12 13 14 15	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've played a role in terms of the vertical flame spread we
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and there's details of all the materials in there, and the	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've played a role in terms of the vertical flame spread we saw at Grenfell Tower?
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and there's details of all the materials in there, and the report is publicly available	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've played a role in terms of the vertical flame spread we saw at Grenfell Tower? A. I mean, the issue with those white window infill panels
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and there's details of all the materials in there, and the report is publicly available Q. Is that the same as the Lacrosse fire? 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've played a role in terms of the vertical flame spread we saw at Grenfell Tower? A. I mean, the issue with those white window infill panels is the cover. The nature of the cover was slightly
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and there's details of all the materials in there, and the report is publicly available Q. Is that the same as the Lacrosse fire? A. Yes, the Lacrosse fire, yes. 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've played a role in terms of the vertical flame spread we saw at Grenfell Tower? A. I mean, the issue with those white window infill panels is the cover. The nature of the cover was slightly different to the rest.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and there's details of all the materials in there, and the report is publicly available Q. Is that the same as the Lacrosse fire? A. Yes, the Lacrosse fire, yes. Q. Yes. 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've played a role in terms of the vertical flame spread we saw at Grenfell Tower? A. I mean, the issue with those white window infill panels is the cover. The nature of the cover was slightly different to the rest. Now, clearly because they have an infill of
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and there's details of all the materials in there, and the report is publicly available Q. Is that the same as the Lacrosse fire? A. Yes, the Lacrosse fire, yes. Q. Yes. A. So I wouldn't be able to say off the top of my head 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23. Again, is that consistent with your understanding? A. Yes. Q. Professor Bisby has set out the properties of XPS in his report, that it has a melting temperature of 230 degrees C, compared to, for example, 130 degrees C of PE; is that correct? A. Yes. Q. There's no figure given for thermal inertia, it just says that they melt; is that right? A. Yes, they tend to melt. They generally have a very low thermal inertia. Q. Do you think these white window infill panels could've played a role in terms of the vertical flame spread we saw at Grenfell Tower? A. I mean, the issue with those white window infill panels is the cover. The nature of the cover was slightly different to the rest. Now, clearly because they have an infill of a combustible material, they will play a role, and if it
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	 Q. Is that something you think could be done at Phase 2, based on the existing evidence? A. Well, I mean, I think if the insulation was available and properly catalogued, yes, something that could be done. Q. We could to do that, yes. Going back to the other international fires we looked at earlier, the Dubai fires and the Lacrosse fire an Australia, did those other fires involve PE-cored ACM panels? A. That's difficult to know. I think that unfortunately the information that is available in most of these fires is generally quite inaccurate, most of it coming from the media. There are reports on all the details of the one that is well investigated is the Docklands fire, and there's details of all the materials in there, and the report is publicly available Q. Is that the same as the Lacrosse fire? A. Yes, the Lacrosse fire, yes. Q. Yes. A. So I wouldn't be able to say off the top of my head exactly what was the insulation material, but we 	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	 Q. Dr Lane has estimated in her report that these panels made up approximately 13 per cent of the external surface between levels 4 and 23.

1		1	
	Q. When you talk about the cover, is what you're talking	1	being the ones driving the burning, they were just
2	about the fact that there's two skins of aluminium	2	burning a little bit later than everything else.
3	A. Exactly.	3	But I think that the same way this image is there,
4	Q and then the XPS inside?	4	I believe there's others where you will see slightly
5	A. Yes.	5	different processes.
6	Q. The aluminium skins, I think, are 1.5 millimetres thick.	6	So it's something that I think, again, the
7	A. Yes.	7	interactions between the systems is quite complex. So
8	Q. Something like that.	8	in some cases you will get one side burning faster, in
9	So you're saying that the fact that you've got those	9	other cases you will get another side burning faster.
10	skins on the outside affects the potential for them to	10	Q. Is it possible that one of the mechanisms by which these
11	contribute to vertical flame spread?	11	ignite and then melt is that you then get a pool of XPS
12	A. Yes. This is the basic concept of encapsulation. So	12	formed at the base of the panels which could then
13	when you have a combustible material that is exposed to	13	ignite? Is that a possible mechanism of failure?
14	the outside, it is encapsulated, and the thickness, the	14	A. It could potentially be, but generally XPS is a very low
15	characteristics of the encapsulation you put is going to	15	density material. So when it actually melts, it
16	make it more or less susceptible to engage in the flame	16	produces very, very little liquid fuel. It's mostly
17	spread.	17	air.
18	Eventually, given the nature and size of the fire,	18	So, in principle, the exact density is not very
19	it is quite clear that they would have participated in	19	clear, what was the exact density of these materials,
20	the process. How late or how early would've been	20	but in principle, as a pool fire, probably the
21	determined by the capacity of the aluminium layer to.	21	contribution will be secondary.
22	MS GRANGE: Protect them from the flames.	22	Q. Do you think that these panels could've contributed to
23	Q. Dr Lane has an image in her report which she says	23	the total heat release rate during the fire on the
24	potentially shows vertical flame spread through those	24	facade?
25	Aluglaze panels. That's BLAS sorry, actually, before	25	A. Well, everything would have.
	Page 133		Page 135
	1 agc 133		1 agt 133
1	we go to this, can I give a warning that I'm about to go	1	Q. Yes.
2	to an image of the tower on fire, so if anybody's going	2	A. But keep in mind that their mass is relatively small
3	to be distressed by that, they should leave now.	3	compared to everything else, so the total amount of
4	(Pause)	I .	
-		4	energy they can release is actually less.
5	Sorry, I should have given a warning before the last	5	energy they can release is actually less. Q. These window panels are mentioned in three of Dr Lane's
6	Sorry, I should have given a warning before the last image of the burnt-out tower.		
		5	Q. These window panels are mentioned in three of Dr Lane's
6	image of the burnt-out tower.	5 6	Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the
6 7	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it	5 6 7	Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and
6 7 8	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it now.	5 6 7 8	Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and then this route, which is vertically across the panels
6 7 8 9	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it now. MS GRANGE: So BLAS0000010, then page 39, figure 10.37.	5 6 7 8 9	Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and then this route, which is vertically across the panels up the length of the tower.
6 7 8 9 10	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it now. MS GRANGE: So BLAS0000010, then page 39, figure 10.37. In fact, the corrected time for this is 1.29 am, not	5 6 7 8 9	Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and then this route, which is vertically across the panels up the length of the tower. Do you agree that those are potential mechanisms by
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6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it now. MS GRANGE: So BLAS0000010, then page 39, figure 10.37. In fact, the corrected time for this is 1.29 am, not 1.26, although I don't think that matters at all. Dr Lane has highlighted there with little blue dots where the insulating panels were on the building. This is on the east face. Do you think that that potentially shows that we are seeing some vertical fire spread across those Aluglaze panels, particularly in the higher levels of the building? A. Well, we are seeing them burn. If you look at those images, what you see is that the panels are burning to	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	 Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and then this route, which is vertically across the panels up the length of the tower. Do you agree that those are potential mechanisms by which these panels could've contributed to the flame spread? A. They're all clearly potential mechanisms, but given the nature of the protective aluminium plate, I would imagine that anything that is vertical will be a mechanism that we should need to consider. For this type of materials horizontal or downward might be a very minor mechanism of spread. Q. Can I just ask you briefly, then, a different material, the EDPM membrane. That's the damp-proof membrane
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it now. MS GRANGE: So BLAS0000010, then page 39, figure 10.37. In fact, the corrected time for this is 1.29 am, not 1.26, although I don't think that matters at all. Dr Lane has highlighted there with little blue dots where the insulating panels were on the building. This is on the east face. Do you think that that potentially shows that we are seeing some vertical fire spread across those Aluglaze panels, particularly in the higher levels of the building? A. Well, we are seeing them burn. If you look at those images, what you see is that the panels are burning to the left of the the burning has reduced.	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	 Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and then this route, which is vertically across the panels up the length of the tower. Do you agree that those are potential mechanisms by which these panels could've contributed to the flame spread? A. They're all clearly potential mechanisms, but given the nature of the protective aluminium plate, I would imagine that anything that is vertical will be a mechanism that we should need to consider. For this type of materials horizontal or downward might be a very minor mechanism of spread. Q. Can I just ask you briefly, then, a different material, the EDPM membrane. That's the damp-proof membrane A. Yes.
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6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it now. MS GRANGE: So BLAS0000010, then page 39, figure 10.37. In fact, the corrected time for this is 1.29 am, not 1.26, although I don't think that matters at all. Dr Lane has highlighted there with little blue dots where the insulating panels were on the building. This is on the east face. Do you think that that potentially shows that we are seeing some vertical fire spread across those Aluglaze panels, particularly in the higher levels of the building? A. Well, we are seeing them burn. If you look at those images, what you see is that the panels are burning to the left of the the burning has reduced. So just by looking at the image, I could possibly say that, in this particular case, the panels were	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	 Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and then this route, which is vertically across the panels up the length of the tower. Do you agree that those are potential mechanisms by which these panels could've contributed to the flame spread? A. They're all clearly potential mechanisms, but given the nature of the protective aluminium plate, I would imagine that anything that is vertical will be a mechanism that we should need to consider. For this type of materials horizontal or downward might be a very minor mechanism of spread. Q. Can I just ask you briefly, then, a different material, the EDPM membrane. That's the damp-proof membrane A. Yes. Q that's there on the columns between the windows and the columns. So after you've got the insulation, you've
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	image of the burnt-out tower. SIR MARTIN MOORE-BICK: That's all right. You've given it now. MS GRANGE: So BLAS0000010, then page 39, figure 10.37. In fact, the corrected time for this is 1.29 am, not 1.26, although I don't think that matters at all. Dr Lane has highlighted there with little blue dots where the insulating panels were on the building. This is on the east face. Do you think that that potentially shows that we are seeing some vertical fire spread across those Aluglaze panels, particularly in the higher levels of the building? A. Well, we are seeing them burn. If you look at those images, what you see is that the panels are burning to the left of the the burning has reduced. So just by looking at the image, I could possibly say that, in this particular case, the panels were igniting, they were contributing to the burning, but the	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	 Q. These window panels are mentioned in three of Dr Lane's potential flame spread routes: horizontally across the edges, top and bottom, vertically along the sides, and then this route, which is vertically across the panels up the length of the tower. Do you agree that those are potential mechanisms by which these panels could've contributed to the flame spread? A. They're all clearly potential mechanisms, but given the nature of the protective aluminium plate, I would imagine that anything that is vertical will be a mechanism that we should need to consider. For this type of materials horizontal or downward might be a very minor mechanism of spread. Q. Can I just ask you briefly, then, a different material, the EDPM membrane. That's the damp-proof membrane A. Yes. Q that's there on the columns between the windows and the columns. So after you've got the insulation, you've got the EDPM membrane, a thin, black membrane, then

1 1 Have you done any work to look at whether that a duct when you expect that your propagation is within 2 2 could've contributed to vertical flame spread? the duct. 3 3 If you put combustible materials outside the cavity A. That would have contributed, as all the other 4 components. In this particular case, it is thermally 4 barrier, the cavity barrier actually has no meaning, 5 5 because effectively the burning can happen around the thin, so this would've been a material that would've 6 spread quite rapidly. Its particular location, might 6 cavity barrier. 7 7 Obviously the cavity barrier will result in not necessarily be as effective for vertical flame 8 spread but, nevertheless, it's a material that will 8 potentially slowing what is going on, because it will 9 prevent part of the burning, but it's not going to stop burn, its density is not low, so it will have 10 10 the spread. a significant amount of mass, and it will contribute to 11 11 Unfortunately, the cavity barriers, once they've 12 12 been overcome, then melting material can actually Q. I now want to come on to talk about the role of cavity 13 barriers in the facade. 13 deposit on the cavity barrier and the cavity barrier in 14 Can we just remind ourselves again, just to 14 itself can become a mechanism of spread. 15 orientate ourselves, what these looked like on site. 15 So in this particular type of scenario, the 16 I'm going to show you some pictures of the open state 16 fundamental principle behind why we put cavity barriers 17 horizontal cavity barriers. If you go to an image in 17 is inappropriate because we have combustibles at both 18 Dr Lane's report, BLAS0000008 at page 42, figures 8.45 18 ends. So it is not blocking any path of propagation. 19 and 8.46. 19 O. So is it right that you think any non-conformity of 20 20 So the image at the bottom is taken from the cavity barriers would not have significantly affected 21 manufacturer's literature in terms of these cavity 21 the rate of vertical flame spread we saw at 22 barriers, and then at the top we see an example of the 22 Grenfell Tower? 23 installation of one of these, I think underneath one of 23 A. If you look at the photographs up there, what you see is 24 the spandrel panels here. 24 that the spaces that are left open -- and let's assume 25 25 Can you explain in general terms what a cavity those are the non-conformities -- are generally a small Page 137 Page 139 barrier is? 1 1 fraction of the overall space. Given the fact that the 2 A. Yes. When you have a cavity, and particularly if that 2 cavity barrier has already been misused by principle, 3 3 cavity has combustible materials, there is a possibility I don't believe that all those non-conformities will 4 4 that a chimney effect can be formed that will actually have a very significant effect in altering the outcome. 5 maintain spread through the cavity. 5 Q. You've talked about concerns about these barriers where 6 The cavity barrier in principle is a mechanism by 6 you've got combustible materials potentially either 7 7 which you try to stop, so you close the barrier in such side, and certainly with an ACM panel you've got it on 8 a way that you prevent the flames from progressing from 8 the outside. 9 9 one place to another. A. Mm. 10 Q. Is it right that this kind of cavity barrier has 10 Q. Is it relevant that you can get deflection and warping 11 an intermittent strip that expands with heat to close 11 of the aluminium panels? How does that affect the 12 the gap? 12 operation of the barriers? 13 A. Yes, potentially, some of the solutions that we apply 13 A. It's the same thing. If the aluminium panels warp, 14 14 deform or fall off, then the whole concept of a cavity when we have intricate geometries and the cavity barrier 15 cannot be cut exactly with the geometry of the material, 15 barrier doesn't apply. 16 you will put the strips of intumescent material. The 16 Q. Professor Bisby has said in his report that horizontal 17 intumescent material with heat, will expand, and it will 17 cavity barriers are considered important within 18 allow the cavity to close. 18 rainscreen cladding systems, particularly when 19 Q. In your report, you say that no matter how well designed 19 combustible cladding and insulation products are used. 20 or implemented, you do not think the cavity barriers 20 Would you agree with that statement? 21 could've prevented vertical or lateral flame spread at 21 A. I do agree with the statement if they are applied in 22 Grenfell Tower; is that right? 22 a way such that they meet their objectives. So, yes, of 23 23 course, cavity barriers are a mechanism that we have to 24 Q. Can you just explain why you're of that view? 24 try to control a fire, but we do have to do it in 25 25 A. A cavity barrier is a system that is designed to close a manner such that effectively we're delivering what we Page 140 Page 138

1 allowing vertical flame spread? 1 want. 2 2 So, for example, if I have the cavity barrier and A. Look, when you start looking into all those details of 3 3 I have the cladding sitting on top of it so that the the cavity barriers, the conclusion you immediately come 4 barrier actually crosses and produces a true barrier 4 up to is that the system that was designed could not be 5 built correctly. So effectively you have penetrations, 5 that cannot be jumped through, then of course they 6 actually are a very important aspect of the problem. 6 complex geometries, all sorts of different things that 7 7 The cavity barrier is a tool that we have to try to by themselves rendered any possible interpretation of 8 reduce the spread of a fire, and the tool has to be used 8 them in reality very, very difficult. 9 appropriately. So if it's used appropriately and within So I think in this case we're talking more about 10 the bounds of what we want it for, then of course it is 10 taking a step back and saying this should've been 11 a good tool that we can put in place. 11 designed better so that it could be implemented 12 12 appropriately so that the cavity barriers could actually Q. So you think there might be circumstances in which it 13 could work but it would all depend on the configuration? 13 deliver it's objective. 14 14 Q. Do you think these gaps and these rails could've played A. It's the design. 15 Q. Do you think it can ever work where your combustible 15 a role in terms of either convective or conductive 16 material is external to the barrier? 16 transfer of heat from level to level? 17 17 A. Well, then it will not be used as a cavity barrier, it A. They would play a role; the question, once again, is to 18 will be used simply as a mechanism of trying to 18 what extent that was a significant role, and that's not 19 decelerate a process, but not necessarily under the 19 20 20 principles of a cavity barrier, because it is not So everything will play a role, but the significance 21 a cavity barrier anymore if it actually has combustible 21 of these elements I think is questionable, because, 22 materials outside. 22 again, these are relatively small gaps compared to the 23 23 area that is covered, so how much a flame can actually Q. Do you think at Grenfell Tower that the cavity barriers 24 wouldn't have been rendered as ineffective if they'd 24 creep compared to the flames actually burning on the 25 25 outside would affect the ultimate outcome. been positioned differently? So, for example, if they'd Page 141 Page 143 1 been put at the base of the spandrel panels rather than 1 I do think that this is probably a secondary role. 2 partway up, do you think that could've affected the 2 Q. Do you think that it would be helpful to do some further 3 3 situation? investigations to better understand the reasons for some 4 4 A. I think that a better design would've perfectly been different flame spread rates, including by reference to 5 possible that would've resulted in a better outcome. 5 cavity barriers? Is that work you think would be useful I think it's difficult to say, "If I did this, I will 6 6 to do? 7 get a better outcome". I think in this particular case 7 A. This is one of those cases where I do not believe so. 8 we have to be extremely careful because, as I said 8 I think a system that is poorly designed, it is poorly 9 Q before, the cavity barriers by themselves are just designed by definition, so taking a step back and trying 10 a tool. 10 to understand it in detail from a forensic perspective 11 So yes, but I do believe that if you use them 11 might help us design something better, but only in that 12 appropriately and do an appropriate design, I do think 12 sense, not necessarily in the sense of trying to 13 that they could improve the way in which the system 13 establish if it would've affected the rate of spread. 14 14 behaves. The system in itself is so complex that trying to 15 Q. What about in stabilising the panels themselves, is that 15 fully understand that system to try to correlate it to 16 a role they might be able to perform? 16 flame spread rates is going to be extremely complex, 17 A. Well, I mean you can grant them a structural role but 17 almost, I would say, impossible to achieve. 18 18 they're not generally designed for that purpose. You Nevertheless, doing a detailed analysis of the role 19 could design them for that purpose if that's what you 19 of a cavity barrier so that we can actually design 20 needed, but it is not the conventional use of a cavity 20 things better might be a very fruitful path to go. 21 21 barrier. Q. Just pausing there and thinking about the windows, we 22 Q. At Grenfell, what we saw was that the fixing rails for 22 established earlier that there were no cavity barriers 23 the cassettes, that the cassettes were fixed to, 23 around the windows. That's something that Dr Lane and 24 24 Professor Bisby have both identified. penetrated the cavity barriers, so you have these gaps. 25 25 Do you think that may have played a role in terms of Do you agree that cavity barriers do play a useful Page 142 Page 144

1 A. Yes. 1 role around window openings to delay both break-out and 2 2 Q. Then propagate upwards? 3 3 A. I think that that is absolutely correct, and I think A. Yes. 4 given the context in which we are operating, but I think 4 Q. Is that why on some of the faces we see almost 5 5 a diagonal effect. We see it particularly acutely on you have to keep in mind that we do not protect 6 the west face, for example? 6 buildings from fires exiting the building. So the 7 7 concept of protecting the frame requires us 8 8 understanding that we have a cavity behind that O. You believe the dominant mechanism is the crown melting 9 and dripping and then lower fires making their way up? 9 effectively is going to bring the fire back into the 10 building. So in the context in which we're operating, 10 A. Yes. I believe that that sets the pace of the 11 absolutely it is a fundamental problem, but in the 11 propagation. So the crown is the one that defines at 12 12 context of design, I think we have to take a step back what rate it's propagating, and that mechanism you just 13 and first think, effectively: what are we protecting? 13 described is exactly the mechanism that I believe is 14 14 setting the speed at which the lateral spread is We've never considered the idea of protecting the exit 15 path of a fire; we always consider the problem of the 15 happening. 16 16 re-entry path of a fire. So we have to be very careful Q. Let's look at the crown in a bit more detail. This is 17 a parapet of strips of ACM, kind of C-shaped columns, or 17 when we state that, but I agree, given the context, it's 18 18 fundamental. some people have described them as "fins", vertical fins 19 Q. Let's move now, then, to stage 3 of your analysis, which 19 installed right at the top of the building to hide the 20 previous concrete parapet; is that right? 20 you say is characterised by lateral flame spread and 21 then internal migration of smoke and fire. 21 A. Yes. 22 22 This is between approximately 1.30 and 2.30 am. Q. We can see a useful picture of that in Dr Lane's report. 23 23 This is at BLAS0000010, page 69, figure 10.73. You've explained that Grenfell Tower is unusual in 24 that horizontal spread enveloped the entirety of the 24 So here we see the crown at the very top, and what 25 25 building in less than 3 hours; is that right? we see are these vertical fins. They are made of Page 145 Page 147 1 A. Yes. 1 aluminium composite ACM panels; is that correct? 2 Q. You have also said whilst there are multiple pathways 2 3 3 for the fire to spread through the facade system Q. They're mounted on C-shaped aluminium channels that all 4 laterally, none of them really explain the lateral 4 fit into one another --5 propagation of the fire that we saw; is that correct? 5 A. Yes. 6 A. Yes. 6 O. -- in rows. Q. Are you still of the view that there is no dominant 7 7 Can you explain why you think it was that the fire 8 pathway conclusively established in terms of explaining 8 spread so quickly round the crown? 9 9 that lateral fire spread? A. I think it's primarily because as the components of the 10 A. Well, there is one that appears as very important, which 10 crown start burning, and the polyethylene starts 11 is the propagation to the crown, and that seems to 11 melting, it pools underneath. I mean, we did 12 12 control, through dripping and dropping of burning a preliminary analysis of the rate, you know, showing 13 debris, the rate at which it propagates. It doesn't 13 a bit of this and -- but I think in the revised report 14 14 necessarily answer the question if it would've of Professor Bisby, this is analysed in much more detail 15 propagated in the absence of the crown. But it does set 15 and I will concur that that is probably the main 16 the pace at which the propagation is occurring. 16 mechanism is the pooling of the polyethylene below the 17 17 Q. So just to be clear what you're talking about there, elements of the crown that effectively serves as 18 what you're suggesting is that the fire propagates 18 a feedback loop that accelerates the burning of these 19 laterally around the crown very quickly -- is that 19 elements. 20 correct? 20 Q. So you're talking about pool fires at the bottom of 21 21 A. Yes. these fins --22 Q. And then you get burning and dripping PE from the 22 A. Yes. 23 crown -- we'll look at its composition in moment -- down 23 Q. -- which then help it propagate laterally --24 on to lower levels, which then establish their own 24 25 25 fires; is that right? Q. -- and then also are dripping down; is that right? Page 146 Page 148

1	A. As they are burning and they start dismembering, you're	1	longer duration at the higher levels because of rising
2	going to have dripping down and pieces falling off, and	2	hot gases and flames, ie the flame plumes out towards
3	that is what effectively starts the fires in other	3	the top of the building?
4	locations.	4	A. That is questionable because it really depends on the
5	Q. Yes. As we'll hear	5	time that is available. So like in the case of
6	SIR MARTIN MOORE-BICK: Can I just ask: am I right in	6	The Torch, for example, the vertical burning happened so
7	understanding that each of these fins has an exposed	7	much faster than any lateral spread that the plume never
8	core along the edges?	8	really opened. It basically remained very, very narrow.
9	A. Yes.	9	Yes, of course it opened a little bit, you can see
10	SIR MARTIN MOORE-BICK: So it's all there waiting to	10	slightly more damage on the top than you have at the
11	propagate from one to the next?	11	bottom, but it's truly almost a vertical plume.
12	A. Exactly.	12	So, in principle, it depends a lot on the capacity
13	MS GRANGE: Exactly. So I was about to take you to that.	13	of the system to sustain burning to the point that you
14	Professor Bisby has highlighted a number of	14	can use that energy to enhance the spread on the upper
15	characteristics which he thinks are important in terms	15	part.
16	of fire propagation around the crown.	16	Q. Do you think that the effect that we saw around the top
17	He refers to the fins as semi-continuous paths for	17	of the crown could simply be explained by the vertical
18	fire to spread. Do you agree with that?	18	flame pluming at the top? Is that an explanation for
19	A. Yes.	19	it?
20	Q. He's highlighted the numerous exposed ACM edges with	20	A. What do you mean exactly by the effect that we
21	exposed polyethylene on the edges?	21	Q. Could the lateral flame spread, the horizontal flame
22	A. Yes.	22	spread that we saw, actually be explained by the shape
23	Q. Again, do you think that's important?	23	of the flames pluming and widening at the top of the
24	A. Yes.	24	building rather than it being about the crown?
25	Q. He's also drawn attention to the fact that they are	25	A. No.
	Page 149		Page 151
1	effectively C-shaped chimneys which in themselves would	1	Q. I just want to take you to a figure in Dr Lane's report,
2	support flame extension and flame spread. Do you agree	2	that's figure 10.47 in her report, BLAS0000010, page 48.
3	with that?	3	This is a diagram of the crown and, just to explain,
4	A. Yes.	4	in the bottom part, what we're seeing is the top of the
5	Q. Also that there's no cavity barriers around the top of	5	building with a Reynobond ACM panel which overlays some
6	the building?	6	insulation which wraps around the top of the building.
7	A. No, it's beyond that. I mean, there's not only nothing	7	Do you see that?
8	to stop it, but also, as it pools down, you have	8	A. Yes.
9	a mechanism to keep pushing it. So any gaps that you	9	Q. Above that, Dr Lane has marked "PPC Aluminium flashing
10	might have are being covered by the pool that is being	10	over top of insulation". As I understand it, that's
11	formed underneath.	11	polyester powder coated aluminium flashing which sat on
12	Q. Does your view remain that the rapid internal	12	top of the ACM and the insulation at the top of the
13	penetration of flats above level 20 can be attributed to	13	building. Then what we see above that are these fins
14	the presence of the crown and the debris that was	14	sitting on top of that.
15	falling from it?	15	Does that make sense?
16	A. Our analysis showed that effectively the rate at which	16	A. Yes.
17	these apartments were being penetrated effectively was	17	Q. It's been suggested that the lateral fire spread we see
18	pretty much the same rate as the progression of the fire	18	at the top of the building might have been more to do
19	in the crown.	19	with the presence of combustible insulation at the top
20	Q. So those flats at the top were particularly prone to the	20	of the building and the Reynobond panels rather than the
21	effects of the melting, the dripping, the heating; is	21	fins.
22	that correct?	22	Would you like to comment on that?
23	A. Yes, yes.	23	A. I mean, you have combustible insulation, you have the
24	Q. But just testing the role of the crown, do you agree	24	Reynobond and you have a platform in which you can
25	that, in any event, the fire would be more severe and of	25	actually pool molten polyethylene. I do not believe
	,,		J x
	Page 150		Page 152

1 A. Yes. that there is any conclusive evidence that would show 2 2 that this is coming from the insulation, and, in Q. That's what you were talking about earlier when you said 3 3 principle, an exposed pool fire is clearly a much more actually you think that is a real candidate to explain 4 severe form of heating than any heating that could come 4 why the fire at Grenfell Tower spread laterally so 5 5 from that insulation that is covered at all ends. quickly. 6 Q. It's also said that the aluminium coping that we see 6 A. Yes. 7 7 over the top there, which had projected, some of it had Q. Is that substantiated by the mapping out of the lateral 8 not melted, it had not melted across the top, but it had 8 flame spread that you've done in each direction? So in 9 9 your figure 35 -- let's just go to that, that's melted a bit on the face of it. 10 Again, would you attach any significance to that? 10 JTOS0000001 at page 78. 11 A. Absolutely, because if you have melted polyethylene --11 You have depicted the lateral spread, as 12 12 I understand it, from top to bottom -keep in mind that the polyethylene is going to melt at 13 a very low temperature, so the polyethylene is going to 13 14 start gasifying at 300-something degrees, which is way 14 Q. -- for each face in time; is that right? 15 below the melting temperature of aluminium, so will not 15 A. Yes. 16 16 let the aluminium heat up beyond that temperature until Q. Can you just explain how that supports the analysis that 17 17 we get this debris falling down and igniting other fires it's fully consumed. 18 18 So, effectively, the fact that you don't have that then go up? 19 melting of the aluminium shows that you have something 19 A. So if you look at the top symbols, you will see as they 20 20 else that is acting as a heat sink, that is taking the are progressing, we're changing the shape and colour of 21 21 the symbol. So, basically, the top symbols reach the energy away and keeping it at a low temperature. It's 22 22 like boiling water, it will not change above 100 until end faster than anything else. So that will be the top 23 23 you finish boiling all the water. It's exactly the same of the building. So that's the progression that is 24 in the case of the polyethylene. It will not reach the 24 driven by the crown. 25 melting temperatures of aluminium. 25 Then what you will see is once -- for example, if Page 153 Page 155 1 you take the yellow triangle, you will see the fire 1 And it's quite telling, the fact that the exposed 2 area where you don't have that molten material is the 2 reaches the yellow triangle at about 110 minutes. 3 3 Q. That's right in the middle of that top diagram. We see one that disappears, while all the area that is covered 4 4 the yellow triangle at the top. is the one that remains unmelted. 5 5 Q. Is it significant that the fins were not backed by any A. Yes. 6 Q. So it's hit the top of the building --6 insulation? Does that change your view about the role 7 7 A. Yes. of the crown? 8 A. I think in this particular case, I believe it's driven 8 Q. -- at that point. That's west 5, yeah? 9 A. Yes. So then debris falls, it ignites the fire in the 9 by the pool fire. I think that that clearly needs to be 10 studied in a lot more detail. 10 next one, which is the 120, and very rapidly progresses 11 But I do think that under those circumstances, 11 up again. So you can see the three triangles. So in 12 12 a period of 10 minutes it's gone down and then all the probably having insulation in the back would have had 13 a very minor impact. 13 way come up. 14 14 If you look where the next triangles are, so you Q. Let's come on to lateral flame spread at lower levels of 15 the tower. Again, we've touched on this. 15 will move all the way down now to about 145, and you can see that a piece of debris falls all the way down and 16 You've said that smoke plumes and heat plumes from 16 17 17 lower down the building will widen with height and then it creeps up. 18 So each of those columns represents a piece of 18 preheat other sections of the cladding, facilitating 19 19 debris that landed below and then it spread up again. later ignition. 20 You've highlighted that a key mechanism for lateral 20 Q. Once it's gone below and landed and then is going up 21 21 vertically, do you agree with Dr Lane that there's then flame spread further down the building is that we have 22 burning debris falling from the areas already on fire 22 a number of vertical pathways through which the fire 23 23 and then accumulating on horizontal surfaces, igniting could then spread across the facade? 24 new localised fires which then spread upwards; is that 24 A. Yes. I mean, you can see that there's a multiplicity of 25 25 right? vertical pathways and it's hard to determine which one

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1	is more important than the other.	1	became quite evident and none of other mechanisms seemed
2	Q. She has the columns as the first one, and then along	2	to play any significant role.
3	window edges and edges of the white infill panels.	3	So, again, within the error bars that you can expect
4	Would you agree with that?	4	in this type of analysis, I don't seem to believe that
5	A. In some parts of the building, potentially that's	5	I found any case where I could unequivocally ascertain
6	correct; in other parts of the building, I think there	6	that the flame was spreading in opposed mode, either
7	might be other different mechanisms of spread.	7	laterally or downwards, in any significant way.
8	It's not very clear when you look at the progression	8	Q. Do you agree, though, that there are some pathways
9	of the fire when each mechanism dominates. It many	9	laterally that it could have followed, albeit slowly?
10	times depends to the proximity of the column, where the	10	A. Oh, absolutely.
11	debris landed. There's a number of different factors	11	Q. So, for example, on the tops and bottom of the windows,
12	that are going to affect what is the mechanism that	12	along edges of the ACM cassettes where, for example,
13	dominates.	13	there may have been exposed edges, or, indeed, along the
14	But I think in some areas, yes, she's correct.	14	window infill panels?
15	Q. In terms of the lateral flame spread, you talked earlier	15	A. Yes. I mean, once again, I go back to this issue that
16	about opposed-flow flame spread. Professor Bisby	16	these are incredibly complex systems, and I would not be
17	explained about this in his presentation back in June	17	surprised that there would be some places in which the
18	with reference to the match and looking at the match	18	flames actually creep under a cavity that was
19	going much slower sideways.	19	horizontal, that could've possibly happened. But it was
20	A. Yes.	20	by no means a dominant mechanism.
21	Q. Do you think there's any role for opposed-flow flame	21	Q. What about the potential contribution of the cut edges
22	spread in terms of what we see at Grenfell?	22	of the PIR insulation? Is it possible that that
23	A. I think it's very minor to negligible.	23	could've played a role, either because debris was
24	Q. Because you think the primary mechanism is this burning	24	falling down and by that time it was hitting that, or
25	debris down	25	because it was burning along the edge?
	D 457		D 450
	Page 157		Page 159
1	A. Yes.	1	A. Well, I mean, again, you go back to the same point. In
1 2			A. Well, I mean, again, you go back to the same point. In such level of complexity, yes, it is possible that it
	A. Yes.Q with fires then going upwards, as opposed to it just migrating laterally across the building?	1 2 3	such level of complexity, yes, it is possible that it
2	Q with fires then going upwards, as opposed to it just migrating laterally across the building?	2	such level of complexity, yes, it is possible that it played a role, but would that be considered one of the
2 3	Q with fires then going upwards, as opposed to it just	2 3	such level of complexity, yes, it is possible that it
2 3 4	 Q with fires then going upwards, as opposed to it just migrating laterally across the building? A. Yes, so if you look at the dots, for example, if you see at 50 minutes, you look at the yellow dots, you will not 	2 3 4	such level of complexity, yes, it is possible that it played a role, but would that be considered one of the dominant factors for the lateral spread? I don't believe so.
2 3 4 5	Q with fires then going upwards, as opposed to it just migrating laterally across the building?A. Yes, so if you look at the dots, for example, if you see	2 3 4 5	such level of complexity, yes, it is possible that it played a role, but would that be considered one of the dominant factors for the lateral spread? I don't believe so. Q. Finally on this topic, you've explained that
2 3 4 5 6	 Q with fires then going upwards, as opposed to it just migrating laterally across the building? A. Yes, so if you look at the dots, for example, if you see at 50 minutes, you look at the yellow dots, you will not see progression to the right. So a little bit later, you will not see another dot appearing. The dot has to 	2 3 4 5 6	such level of complexity, yes, it is possible that it played a role, but would that be considered one of the dominant factors for the lateral spread? I don't believe so. Q. Finally on this topic, you've explained that internationally there are some exceptions in terms of
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		1	1 1 1 1 1 1
1	a possibility that that had an effect.	1	we have seen in the evidence.
2	But, again, this is an example where you can see	2	In section 7.4 of his report, Professor Bisby has
3	a systematic line of lateral flame spread that is very	3	drawn attention to a large number of witnesses who
4	different to what you see in Grenfell.	4	comment specifically on the early failure and ignition
5	Q. You've also drawn attention to the Monte Carlo Casino &	5	of the extract fans unit and the surrounding XPS panels.
6	Hotel fire in 2008, where the fire spread laterally	6	So you have the extractor fan we looked at the
7	across a parapet.	7	kitchen window earlier in the middle, it's got
8	Can we just look at that. Figure 32, JTOS0000001,	8	a panel surrounding it, which is extruded polystyrene;
9	page 75.	9	is that correct?
10	So these are images of the Monte Carlo Casino &	10	A. Yes.
11	Hotel fire.	11	Q. And Professor Bisby has drawn attention to that as
12	Can you explain why you think this has particular	12	a potential route for ingress. You've also highlighted
13	parallels with the fire at Grenfell?	13	that mode of failure in your report.
14	A. Well, I mean, I think that this particular case, the	14	Many of these that Professor Bisby has drawn
15	upper part of the building is a thick layer of	15	attention to were in the flat 6s on the east face of the
16	combustible material that is rendered with	16	tower.
17	a non-combustible protection.	17	Do you think that this evidence is potentially
18	The rendering of the non-combustible of	18	significant in terms of the route of fire spread back
19	protection, performed very poorly, so it effectively	19	into apartments?
20	exposes the material quite rapidly, so it allows the	20	A. Potentially. I think that, once again, when we think of
21	combustible material to propagate laterally quite	21	the design of a window, we are designing a window
22	rapidly.	22	keeping in mind that we don't want fire spreading from
23	An interesting aspect of this one you can see it	23	one building to another one. So we set a certain
24	in figure (D) is that this material drips down and	24	criteria, which is 12.6 kilowatts per metre squared as
25	basically deposits in the edges that you can see, and	25	being the criteria that is used for the design of all
	Page 161		Page 163
1	that's really the mechanism that continues propagating	1	the window components.
1 2	that's really the mechanism that continues propagating the fire.	1 2	
	the fire.		So, in principle, there is no expectation that any
2	the fire. So what you get is molten material depositing in	2	So, in principle, there is no expectation that any of these components will withstand anything above
2 3	the fire. So what you get is molten material depositing in that ledge, and that pool that forms in there is the one	2 3	So, in principle, there is no expectation that any of these components will withstand anything above 12.6 kilowatts per metre squared.
2 3 4 5	the fire. So what you get is molten material depositing in that ledge, and that pool that forms in there is the one that keeps igniting the material forwards. So in that	2 3 4	So, in principle, there is no expectation that any of these components will withstand anything above 12.6 kilowatts per metre squared. So, in principle, yes, I wouldn't be surprised that
2 3 4 5 6	the fire. So what you get is molten material depositing in that ledge, and that pool that forms in there is the one that keeps igniting the material forwards. So in that sense, it does show some similarities with Grenfell.	2 3 4 5	So, in principle, there is no expectation that any of these components will withstand anything above 12.6 kilowatts per metre squared. So, in principle, yes, I wouldn't be surprised that one of these elements is weaker than the others. We
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some of these. 1 1 migration. 2 2 Gaps in the window framing. Many residents have Q. It's been suggested that double glazed units are 3 3 referred to gaps and draughts around the windows after resistant to fire attack and that it's by no means 4 the refurbishment, and some have actually referred to 4 certain that they will fail during a fire; would you 5 5 agree with that? fire directly ingressing through those window surrounds. 6 Again, do you think that might have had a role to 6 A. No. 7 7 Q. Spray foam. Professor Bisby has identified the use of play? 8 A. It would've had a role. I mean, clearly, if there is 8 spray foam to seal gaps around the windows to provide 9 9 a final airtight seal. He has considered this to be a gap, in as much as there could be a window open or 10 something like that, then there would be no barrier, so 10 potentially significant in terms of the ingress of fire 11 that delay that you would have from the moment the 11 and smoke around the windows. 12 12 flames arrive until the smoke starts getting in -- and Do you think that the presence of spray foam 13 also, early on -- I mean, from the perspective of smoke 13 could've exacerbated the ingress on the night? 14 migration, it could've been significant because smoke 14 A. I mean, it would have, like everything else, but I do 15 goes up and envelops the building, so you could have 15 think, again, this falls in that category where I would 16 16 areas where, effectively, you have no heat, but you not be able to establish a ranking between all of this 17 17 actually have smoke. So the smoke could've easily because they will all fail in a very short period of 18 penetrated through those gaps. 18 time. 19 So from the perspective of smoke migration, I think 19 O. What about whether any of the internal compartment fires 20 20 it might have a significant role, but from the themselves on the night, once they're burning, could've 21 perspective of re-entry of flames, that's probably not 21 contributed to the external flame spread, the extent or 22 22 as significant. the severity of the external flame spread, is that 23 23 Q. Just to be clear, I was going to come on to open window a possibility? 24 in a moment. I was talking here about -- we know the 24 A. That is actually a true fact. Clearly if you have 25 25 windows were pushed out during the refurbishment and a fire that starts in a compartment, the compartment has Page 165 Page 167 there were gaps down the side that were filled with 1 1 a fuel load, so it has a significant amount of energy 2 insulation, and residents have talked about draughts 2 that is being released, and that energy is going to 3 3 round those gaps, or some have. partially spill out, particularly if doors are closed. 4 Just to be clear, do you think that's a potential 4 So it's going to spill out and it is going to contribute 5 path of fire or smoke spread back in? 5 to the energy that is being released. 6 A. Any gap is a potential path for smoke. Any potential 6 Now, clearly, again, the interplay between how fast 7 path for spread requires a condition of failure, and 7 it is spreading and how fast you reach conditions in 8 that condition either is ignition of the insulation, 8 which this internal fire starts contributing is what 9 9 heat flux sufficient to break it, heat flux sufficient really matters. But, effectively, once you start 10 to melt something. So then because you require 10 releasing that energy, that energy has to go somewhere, 11 a condition for failure, and your heat insult is so much 11 and part of it is going to go out and going to 12 12 higher than it was designed for, then I think that's contribute to the process. 13 what makes the difference minor. Because at those heat 13 Q. Do you think there are any times in the fire or 14 14 fluxes, everything will fail very rapidly. particular aspects of the burning we see on any of the 15 Q. We've also heard instances of the softening and the 15 facades where you think that's happening? 16 melting of the uPVC and then entry. I mean, that's a 16 A. There's nothing in particular. I mean, I think there's 17 17 similar route. Do you agree? obviously certain areas, like as is explained by Dr Lane 18 18 and Professor Bisby, the areas around the 12th floor, 19 Q. You've talked about thermally induced breakage of window 19 where you have particularly unusual burning, where 20 glazing. 20 potentially what is happening inside is having more 21 Then open windows. Do you think they may have 21 effect on the rest. But those seem to happen generally 22 played a role? It was a hot night, windows being open, 22 after the fire has passed, and if they are contributing, 23 23 flame spread going up, is that -they're contributing to the heat that is in the plume 24 A. I think, again, more than flame spread, the role of 24 and, thus, contributing to what is happening much, much 25 25 windows is probably more significant in regards to smoke further. Page 168 Page 166

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1	MS GRANGE: I'm now going to move to a separate topic, so	1	you have done a 999 call analysis, haven't you, of
2	this might be a good moment for a break.	2	people reporting smoke in certain areas?
3	SIR MARTIN MOORE-BICK: I was going to say, would that be	3	You've said:
4	a good time?	4	"There are multiple 999 calls during Stage Two
5	MS GRANGE: Yes.	5	(01:05:57 - 01:30:00) reporting smoke in the lobbies, as
6	SIR MARTIN MOORE-BICK: Well, professor, I think we'll have	6	the fire spread vertically up the building from Flat 16
7	a break now for 10 minutes.	7	on Level 4 to the roof above Level 23. Most of these
8	Go with the usher. No talking about your evidence,	8	calls centre around the middle of the building, with
9	please, and be back at 3.20.	9	smoke in lobbies reported by callers on Levels 10, 11,
10	All right, 3.20, please.	10	12, and 14 timed between 01:25:16 and 01:28:26 Of
11	(3.10 pm)	11	these reports, only Level 14 is clearly reported as
12	(A short break)	12	having a significant amount of smoke. Prior to this
13	(3.20 pm)	13	there is also a report of a smoke-filled lobby higher up
14	SIR MARTIN MOORE-BICK: All right, professor? Ready to go	14	the building on Level 22 at 01:21:24 This latter
15	on?	15	report is likely to be due to internal spread of smoke,
16	THE WITNESS: Yes.	16	as the fire had not reached Level 22 by this stage."
17	SIR MARTIN MOORE-BICK: Yes, Ms Grange.	17	So, there, is it right that you're mainly
18	MS GRANGE: Just one question relating to that last topic	18	highlighting what the pattern of the 999 calls were
19	about ingress through windows.	19	showing
20	We were talking about the fact that given you've got	20	A. Yes.
21	a 120-kilowatt per metre square fire going up	21	Q in terms of the spread of smoke?
22	vertically, weaknesses in the window arrangement may not	22	You say this in your third paragraph:
23	have made much difference in terms of ingress, given you	23	"From the onset of Stage Three (01:30 — 02:00), 999
24	get glazing failure anyway.	24	callers consistently report thick black smoke considered
25	What about downward flame spread? So the primary	25	unpassable by residents in the lobbies. These include
	Page 169		Page 171
1	mechanism you were talking about earlier of melting and	1	the 12th, 14th, 16th, 18th, and 21st to 23rd Level
2	dripping debris which then accumulates on ledges or	2	lobbies within the period 01:30 — 01:40 alone
3	window ledges and themselves create smaller fires which	3	Further 999 calls for the rest of Stage Three report a
4	go up, is it possible in that situation that weaknesses	4	similar situation on the 10th, 11th, 19th and 20th
5	in windows, whether it's the extract fan unit or other	5	Levels Some of these also report smoke in the
6	weaknesses around the sides, could've then played	6	stairwell itself. It is clear that, from the onset of
7	a role, or a more significant role?	7	Stage Three, internal smoke spread is fairly ubiquitous
8	A. Yes. I think that if you have debris then obviously you	8	above Level 10."
9	have much less insult from the fire on the external	9	Is that correct?
10	part, and weaknesses in the window design would've had	10	A. Yes.
11	a more significant impact on potential ingress of the	11	Q. You've noted the levels there in terms of smoke spread.
12	flames.	12	Do you think there's any significance in terms of
13	Q. I now want to move to consider the internal migration of	13	where smoke's being reported at that point in the
14	smoke and fire, and at this point I think it's important	14	building?
15	to draw attention to your addendum to your Phase 1	15	A. Can you extend a bit, what do you mean?
16	report, where you've essentially highlighted that	16	Q. Well, you've highlighted certain parts of the building,
17	there's a need to do a lot of further work at Phase 2,	17	12th, 14th, 16th, 18th, 21st to 23rd, effectively the
18	specifically to correlate the firefighter activity and	18	middle of the building and then the top of the building.
19	the smoke spread during both stages 2 and 3 of the fire;	19	A. Mm-hm.
20	is that correct?	20	Q. Do you think that's significant in terms of the pattern
21	A. Yes.	21	of what we're seeing?
22	Q. Can we just go to what you've said in your addendum. So	22	A. Well, it is significant in the sense it's somehow
23	if we bring that up, that's JTOS0000002 at page 1.	23	unusual that you have concentrated calls in certain
24	I just want to highlight a couple of paragraphs here.	24	areas of the building, which clearly show you that there
25	In the second main paragraph, you've said because	25	was something unusual that was happening in there, and
l			
	Page 170		Page 172

			distribution last 1
1	we have not been able to gather the complete amount of	1	that the doors had to be open as opposed to the doors
2	information to be able to establish exactly what is	2	having failed because of an event.
3	going on.	3	Q. Because what you're saying is there is no flame front
4	Q. What caused those, yes.	4	there
5	You've highlighted some examples in your report from	5	A. Yes.
6	the available footage that we have of the tower of smoke	6	Q on the west face to cause a flame-induced failure of
7	emerging from flats on the opposite side of the tower to	7	the doors.
8	the fire front, the flame front of the east side.	8	A. Yes.
9	Can we just have a look at those images, but before	9	Q. So you're deducing from that that it must have been
10	we do, I probably ought to issue another trigger	10	smoke spreading through an open door?
11	warning. We're going to be looking at images of the	11	A. Yes.
12	tower. We're just looking at smoke spread through the	12	Q. That was left open by a fleeing occupant?
13	tower, it's not the tower on fire, but some people may	13	A. Well, that could potentially be the case. It could
14	find these images upsetting or distressing, in which	14	potentially be firefighting intervention. These are the
15	case they should leave now.	15	kinds of things that I think before any conclusions are
16	(Pause)	16	drawn, we have to be very, very careful that all the
17	Those images are figures 48 to 52. That's	17	available information is correlated.
18 19	JTOS0000001, starting on page 88, if we can bring that	18 19	Q. There's also some factual evidence that firefighters found considerable smoke in certain lobbies very early
	up.		· · · · · · · · · · · · · · · · · · ·
20 21	So these are images, my understanding is, on the west face of the facade.	20 21	on in the fire, for example Firefighter O'Beirne, who goes up and finds smoke in the lobbies as early as 01.20
			Ţ - 1
22	A. Yes.	22	in some areas.
23	Q. We see, as early as 01.57/01.58, that there is smoke	23	You're aware of that? A. Yes.
24 25	emerging.	24	
23	Just explain to us, the top image, where is the	25	Q. In the light of that and your analysis of the 999 calls
	Page 173		Page 175
1	smoke emerging from on that image?	1	that you've done I realise this is only a preliminary
2	A. You can see	2	analysis do you agree that the lobbies appear to have
3	Q. Where are you referring to?	3	been compromised on a number of floors very early in the
4	A. You can see a darker colour	4	fire, for example by 01.20 and certainly by 01.25/01.26?
5	SIR MARTIN MOORE-BICK: Would you like to get up and point	5	A. Yes. I mean, there is sufficient evidence to say that
6	it out to us?	6	there was a level of compromising of the lobbies quite
7	A. So these are the types of images that you can see.	7	early on. I think it's really not 100 per cent certain
8	MS GRANGE: You can see it very clearly on that bottom	8	to me the exact timings because we do not always have
9	image. On the top image	9	exactly the times, for example, when the firefighters
10	A. It's hard to tell, but it would be somewhere in there.	10	were in different places.
11	SIR MARTIN MOORE-BICK: Thank you.	11	SIR MARTIN MOORE-BICK: Is it possible that that was
12	MS GRANGE: So this is west face, 1.57/2.00 am. You say	12	a result of what we've called the flat 6s being exposed
13	that the significance of this is that that movement of	13	to fire, and therefore smoke, and then people leaving
14	smoke would only be possible if compartmentation is	14	the flat 6s and the doors not being closed?
15	breached for two units; is that right?	15	A. Yes, absolutely.
16	A. Yes.	16	SIR MARTIN MOORE-BICK: Because that would compromise the
17	Q. So it's got through one flat, into the lobby, through	17	lobby in each case, wouldn't it?
18	the lobby, and into another flat?	18	A. Absolutely. I think that that is a possibility and that
19	A. Yes.	19	would imply that the self-closing mechanisms were not
20	Q. Is that correct?	20	working and that people didn't close the doors. So
21	A. Yes.	21	I think clearly that is a possibility that needs to be
22	Q. Why did you think it was so important to highlight that?	22	evaluated very carefully.
23	A. Because the conditions are such that the doors	23	MS GRANGE: Is that the kind of detailed work you'd want to
24	themselves would've not failed. The flats on the west	24	do at Phase 2
25	facade were not on fire yet, so that clearly tells you	25	A. Yes.
	Page 174		Page 176
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1	Q which is to try and look very specifically about	1	self-closing.
2	occupant egress, door condition, firefighter activity,	2	Q. Is it therefore right to assume that the
3	floor by floor, flat by flat	3	compartmentation separating each flat from the
4	A. Yes.	4	neighbouring flats should be capable of resisting any
5	Q to try and piece it together?	5	significant passage of smoke, heat and fire from one
6	A. So you can make a correlation to gain certainty on all	6	flat to another?
7	the timings and, in particular, the level at which they	7	A. Yes.
8	had been compromised by smoke.	8	Q. That's the case even in the event of a very significant
9	Q. Given that you have said you want to do much more	9	external facade fire?
10	detailed work at Phase 2, at this stage what I'm	10	A. Eventually you might end up having a problem, but the
11	proposing to do is just explore some of the broad themes	11 12	compartmentation in principle should be designed to a level in which it withstands the fire for a very
12 13	that you have identified in your report which are potentially important in terms of internal smoke spread.	13	significant period of time. And compartmentation, as
14		14	I said, is designed on the basis of a post-flashover
15	Just before we get to that, it's right to note that you've emphasised, again, the importance of maintaining	15	fire. So you already have the time that it takes for
16	these internal compartmentation lines of defence.	16	the fire to enter, the time that it takes for the fire
17	A. Yes.	17	to transition to flashover, and then the time that you
18	Q. You've said that internal smoke spread, particularly	18	have for the failure of the compartmentation under those
19	into the lobbies and stairwells, correlates strongly	19	conditions.
20	with past fire events that do result in a high number of	20	So you have all these significant delays that, in
21	casualties; is that right?	21	principle, should allow people to migrate to the lobby
22	A. Yes.	22	and then from the lobby to the stair. So you have
23	Q. So in contrast, some very large international fires with	23	already two layers of compartmentation that you have to
24	comparable internal fire spread have not resulted in	24	breach.
25	penetration of smoke and flames into the lobby or	25	So, in principle, compartmentation is a very robust
25	penetration of smoke and rames into the rootly of		so, in principle, compartmentation is a very rosust
	Page 177		Page 179
1	stairs; is that right?	1	way of giving a very significant amount of time for
1 2	stairs; is that right? A. Yes.	1 2	way of giving a very significant amount of time for people to enter the stairs and be safe in the stair for
1 2 3	A. Yes.	1 2 3	people to enter the stairs and be safe in the stair for
2	A. Yes. Q. I know it's very difficult in general terms, but can you	2	people to enter the stairs and be safe in the stair for an even longer period of time.
2 3	A. Yes.	2 3	people to enter the stairs and be safe in the stair for an even longer period of time. Q. Moving to some themes we can pick up. I want to discuss
2 3 4	A. Yes.Q. I know it's very difficult in general terms, but can you give us an indication of why in those events it didn't	2 3 4	people to enter the stairs and be safe in the stair for an even longer period of time.
2 3 4 5	A. Yes. Q. I know it's very difficult in general terms, but can you give us an indication of why in those events it didn't penetrate into the lobby and the stairs? What was it	2 3 4 5	people to enter the stairs and be safe in the stair for an even longer period of time. Q. Moving to some themes we can pick up. I want to discuss door failure by fire for a moment. We'll come to
2 3 4 5 6	A. Yes. Q. I know it's very difficult in general terms, but can you give us an indication of why in those events it didn't penetrate into the lobby and the stairs? What was it about those buildings that was potentially different to	2 3 4 5 6	people to enter the stairs and be safe in the stair for an even longer period of time. Q. Moving to some themes we can pick up. I want to discuss door failure by fire for a moment. We'll come to penetration of smoke in a moment, but concentrating on
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1 going to fail due to internal fire? 1 those that were trapped in flats that there was smoke 2 2 spread coming through the doors --A. Yes. 3 3 Q. You've highlighted in your report that, despite major A. Yes. 4 damage in many of the flats, a significant number did 4 Q. -- in terms of their ability to survive in those flats 5 not attain flashover. You also say in your addendum 5 or potentially be rescued; is that correct? 6 report that fire-induced door failure could be 6 A. Yes, that's correct. 7 7 a contributing factor in the latter part of stage 3. Q. It's fair to mention there are some instances of doors 8 8 A. Yes. apparently performing slightly better on the night. So 9 Q. Is that correct? 9 take Antonio Roncolato, who was there until 06.00 in the 10 A. Yes. 10 morning, potentially Natasha Elcock, another example, 11 Q. But you don't think it's going to be a significant 11 some examples of it performing more effectively. 12 contributing factor during stage 2 or earlier; is that 12 What do you think is the potential significance of 13 right? 13 that in terms of the overall pattern that we're seeing, 14 A. Yes. 14 or is it too early to say? 15 Q. Does that remain your view? 15 A. Well, I think it is actually very difficult to 16 16 A. That remains my view. ascertain, because clearly we, in theory, should be 17 Q. Let's turn, then, to penetration of flat doors by smoke. 17 operating under the assumption that the doors are all 18 18 We know from Dr Lane's report that there are homogeneous and, therefore, every flat should've been 19 a number of difficulties with many of the flat doors, 19 designed in a fairly similar manner, and it should've 20 including that they don't comply with relevant cold 20 been maintained and kept, and that generally is not the 21 smoke leakage requirements and an absence of test 21 case. What we get is significant variance in the level 22 22 evidence which correlates with those doors. of maintenance and the care that these things are given, 23 Is it your view, based on what you've seen and the 23 even the way in which they're designed or built. 24 general themes emerging, that the doors failed to 24 So variations are expected, both in the use and in 25 maintain compartmentation in terms of smoke spread? 25 the construction. So I believe that that is probably Page 181 Page 183 1 1 A. Yes, that's possible. one of the main reasons why you find some differences in 2 Q. You have noted yourself in your report, reports of smoke 2 what people observe. 3 coming through flat doors, for example at 01.25 and 3 Q. Occupant egress. You have also discussed -- and you've 4 01.26, just based on the 999 calls. 4 already mentioned it a number of times -- the effect of 5 5 A. Yes. occupant egress on compartmentation. 6 Q. What do you think is the significance of that in that 6 Does it remain your view that that would have 7 7 a negligible effect unless the doors are not closed early stage? 8 8 A. Again, it goes back to the problem of multiple breaches behind people when they leave? q 9 of compartmentation. So if there is a call that 10 indicates that smoke is coming into that flat through 10 Q. You think just the opening and closing of a flat door 11 the door, that basically means that the flat is not on 11 onto a lobby is unlikely to affect the overall pattern 12 12 of smoke spread significantly; is that right? fire and the smoke is coming through the lobby, and that 13 must have come through from another apartment. So 13 A. Yes. I think if you think of the process of egress, if 14 14 people are evacuating, that basically means that the effectively you have again this path where you have 15 multiple levels of failure before it starts entering the 15 smoke that they're exposed to within their apartment is 16 16 still not the type of smoke that will threaten their apartment. 17 17 So I think this needs to be explored in very lives. 18 18 significant detail, because given the long period of So whatever is coming into the lobby from people 19 time that people spent in those places, it is 19 evacuating their own apartments will be very far from 20 fundamental to try to understand what were those 20 tenability, and so I would not expect that that will 21 21 breaches. have a significant impact on the lobby itself. 22 Q. I was going to draw attention to that, that obviously 22 Now, if the door is left open, then there will be 23 it's right, isn't it, any door will fail after a certain 23 a significant delay under which conditions can actually 24 amount of time, or may fail after a certain amount of 24 change, and then you can actually have a different kind 25 time, but here it may have been very significant for 25 of smoke entering the lobby area. Page 182 Page 184

1	Q. So if those door-closers are ineffective or not	1	So I think having an enormous reliance on self-closing
2	installed, is it your position that the contribution to	2	mechanisms is probably asking too much of a system that
3	the spread of smoke is going to be greater?	3	is a very secondary means of protection.
4	A. Much more significant, yes.	4	In principle, if the fire would have not emerged
5	Q. Is it also going to be significant in terms of the	5	from the compartment of origin, it would've remained
6	oxygen potentially getting into those flats and the	6	compartmentalised, then all these secondary elements are
7	fires you have in those flats?	7	just extra redundancies that we're putting in place;
8	A. Yes, although I believe that that, in a scenario like	8	they are not truly significant to the fire safety
9	this, will be a secondary effect. I mean, clearly when	9	strategy.
10	you have a post-flashover fire, it's considered to be	10	Now, the problem is that when everything else fails,
11	an under-ventilated fire, so the more oxygen you put in,	11	these are the only things that can pick up the pieces,
12	the more intense it burns. But in this particular case,	12	and then they acquire a significance they were never
13	given that the fire is coming from the outside and you	13	intended to have.
14	have window breakage and so forth, probably the impact	14	Q. I mean, are there other options to door-closers?
15	would be secondary. But yes, of course, it would add	15	A. No, no, we should have them, under the expectation that
16	some more air into the fire.	16	there will be a very significant rate of failure.
17	Q. Imagine you are fleeing a flat 6 and you've seen your	17	That's why it becomes sort of an ultimate redundancy and
18	kitchen window on fire and potentially your kitchen	18	not a primary means of protection.
19	starting to burn. You flee out the door, and the closer	19	SIR MARTIN MOORE-BICK: But the door is the one, as it were,
20	doesn't shut behind you. Is that compartment likely to	20	weak link in the whole compartmentation design, isn't
21	come to flashover quicker because you've left the door	21	it? Because in a building like Grenfell forget the
22	open?	22	cladding for a minute the rest is concrete.
23	A. No, no, actually, it will be the opposite.	23	A. Yes.
24	Q. The opposite?	24	SIR MARTIN MOORE-BICK: So I would've thought that to have
25	A. Yes, because you're going to be losing smoke, so	25	effective self-closers on the doors was pretty much
	12 100, because you 10 going to be losing smone, so	23	crective sen-closers on the doors was pretty fluen
	Page 185		Page 187
	8		0
1	effectively that will delay the transition to flashover.	1	critical to the concept of compartmentation.
1 2	effectively that will delay the transition to flashover. Q. But there will be an easy transmission of smoke from the	2	critical to the concept of compartmentation. A. It is in a certain sense, okay? So, effectively, if the
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2	Q. But there will be an easy transmission of smoke from the flat into the lobby.A. From the flat into the lobby. Then once the flat	2 3 4	A. It is in a certain sense, okay? So, effectively, if the
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2 3 4	Q. But there will be an easy transmission of smoke from the flat into the lobby.A. From the flat into the lobby. Then once the flat	2 3 4 5 6	A. It is in a certain sense, okay? So, effectively, if the compartment fails and people evacuate and leave the door, you would have compromised the lobby, but then you
2 3 4 5	 Q. But there will be an easy transmission of smoke from the flat into the lobby. A. From the flat into the lobby. Then once the flat transitions to flashover, you have a better ventilation 	2 3 4 5 6 7	A. It is in a certain sense, okay? So, effectively, if the compartment fails and people evacuate and leave the door, you would have compromised the lobby, but then you have, from the lobby to the door of the stair, another
2 3 4 5 6	Q. But there will be an easy transmission of smoke from the flat into the lobby.A. From the flat into the lobby. Then once the flat transitions to flashover, you have a better ventilation of the flat, so the fire will be more intense.	2 3 4 5 6	A. It is in a certain sense, okay? So, effectively, if the compartment fails and people evacuate and leave the door, you would have compromised the lobby, but then you have, from the lobby to the door of the stair, another fire resistant door. So you're putting multiple layers
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a public space of the building, the maintenance level of 1 1 the assessment by Dr Lane. 2 the door, the self-closing mechanisms, will be of a much 2 Does it remain your view that there were only minor 3 higher quality than you would expect could happen in the 3 weaknesses in, for example, the stair enclosure in terms 4 interior of a flat. 4 of compartmentation? Have you seen anything that would 5 Q. And because it's a firefighting shaft, it has to have 5 suggest that there were any penetrations that were 6 a higher rating, et cetera, and all of that. We are 6 causing issue with the compartmentation? 7 7 going to explore all of that with Dr Lane on Thursday. A. I think that's correct. 8 A. Yes. 8 Q. Ingress as a result of the smoke control system and the 9 Q. Another topic is firefighter activity -- you've 9 vents onto the lobbies, have you had a chance to 10 highlighted this -- including running hoses through 10 consider appendix J of Dr Lane's report? 11 stairwell doors or breaking down flat doors, for example 11 A. Yes, I have. 12 the breaking down of the flat 16 door. 12 Q. And her concerns, based on some of the factual evidence 13 In terms of the significance of this, what you say 13 that we've heard, about the possible passage of smoke 14 is that this is arguably less significant if you're just 14 via the vents, the dampers, in the smoke control system 15 fighting a one-fire floor. It's kind of what you just 15 between lobbies. 16 said. 16 Do you have any views about the potential 17 A. Yes. 17 significance of that at this stage, or is that something 18 Q. But that becomes really problematic once you've got 18 you'd like to do further work on? 19 multiple floors on fire, if you have doors held open, 19 A. Well, as Dr Lane indicates at the beginning of 20 particularly to the stairs; is that correct? 20 appendix J, the system was designed for a one-floor 21 A. Absolutely, because effectively if the fire remains 21 fire. So while there's a number of non-compliances she 22 within the compartment, the stay-put strategy stands 22 highlights in the appendix, it is clear to me that 23 23 and, therefore, people are not required to evacuate the a system that was designed for a one-floor fire, in 24 building. So the stair, in a way, will not be used 24 particular when we're talking about vertical shafts, 25 until the firefighters establish or deem that the stair 25 fans and dampers, it is very clear that its performance Page 189 Page 191 1 is completely unreliable. So whether it was properly 1 can be used again. So during their operations, the 2 possibility of filling the stair with smoke is real, and 2 designed or improperly designed, it would not surprise 3 3 it is part of the concept of the stay-put strategy. So, me at all that the system didn't perform at all. 4 4 Q. But does it concern you that we have factual evidence in that sense, it is not a very significant problem. 5 5 But if you have multiple-floor fires, then you have where people are reporting smoke coming through those 6 vents straight into the lobbies? Is that concerning? 6 to evacuate people while they are operating. There's 7 7 a convergence of timescales. And then their operations A. Well, the evidence is that the system is performing 8 8 become in conflict with the actions of the occupants of poorly because it's bringing smoke into the lobbies. 9 9 the building. Now, that could have been because of the 10 Q. You also make this point, which is it prevents a change 10 non-compliances, but it could also have been because the 11 of strategy from stay put to evacuation if you've 11 system was designed to basically deal with one floor. 12 already compromised your evacuation route. 12 One of the things that is not clear yet from 13 A. Exactly. It makes it much more difficult to take the 13 appendix J, and I think it should be explored a bit more 14 14 decision of moving from one strategy to another. in detail, was the way in which the dampers were 15 Q. Have you formed any preliminary views about how 15 activated, because effectively the detection of smoke 16 significant the holding open of doors or the battering 16 within a lobby will activate the dampers for that 17 17 down of doors might have been in explaining the early specific floor, but what was the algorithm supposed to 18 egress of smoke onto lobbies or compromise of egress 18 do if you had smoke in ten different floors? 19 19 routes? So the way in which the system is operating -- smoke 20 A. From the preliminary information that we have, it seems 20 management systems are a very precise balance of 21 21 pressures, where you effectively have to push the smoke that the evolution of the conditions of the stairs and 22 22 in some cases the lobbies is very dynamic. So I think in one direction so that you clear another space without 23 23 that this opening and closing of doors and so forth necessarily altering what is happening in a fire. So 24 seems to be a very significant aspect over the problem. 24 many times when you change the equilibrium of the 25 25 Q. Missing or damaged fire-stopping, here you've relied on systems, smoke might end up going in all the wrong

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1	directions.	1	But I think that that's what I referred to as
2	So I think that there is a reason for concern, and	2	tenability, is basically both: conditions that are
3	there is a reason to look into the space, but I think we	3	actually harmful to the individual, but also conditions
4	have to keep in mind that it was a system that was	4	that the individual perceives as harmful and therefore
5	designed for a one-floor fire, and that is a fundamental	5	changes his actions because of them.
6	weakness of the system, not necessarily the	6	Q. Linked to that, can you explain the capacity of some
7	non-compliances.	7	residents to succeed in self-evacuations after 3.00 am?
8	Q. In general, at this stage, before we move to your	8	I mean, we've got numerous examples of people who were
9	untenable stage 4, do you have any more developed views	9	able to get out after 3.00 am down those stairs.
10	about smoke migration in the light of the Phase 1	10	A. Yes, I think it's a combination of both. It's people
11	evidence, or is that something you want to go away and	11	that actually made a better choice, in the sense that
12	look at in more detail?	12	despite perceiving that the conditions were dangerous,
13	A. Yes, I think I'd rather not comment any further because	13	they probably simply took the decision of moving
14	I do think that that requires a bit more detailed	14	through.
15	analysis.	15	But also there is a component and it's quite
16	Q. So your stage 4 you describe as the untenable stage, and	16	clear from the 999 calls the system is very dynamic.
17	you say this is from 2.30 am until extinction of the	17	So there are moments where effectively the stairs seem
18	fire. This marks significantly untenable conditions in	18	to clear up more than other moments. So I think they
19	the fire.	19	might just simply have got the right window.
20	Can you just be clear what you mean by "untenable"	20	So I think it's a combination of both, very
21	here?	21	difficult to ascertain, but I think if we can manage to
22	A. Yes. Untenability is a very complex concept to define	22	pinpoint the way in which smoke is migrating, then we
23	because it is partially perception and partially	23	will be able to at least establish which are the
24	reality.	24	conditions that were acceptable, which ones were not, so
25	An individual that walks into smoke might encounter	25	that then we can ascertain more or less what was the
	Page 193		Page 195
	8	_	8
1	conditions that will not allow him or her to survive.	1	interaction of the people with the smoke.
2	So, in principle, that is the definition of	2	Q. So just to be clear, you think on the evidence you've
2	So, in principle, that is the definition of untenability. So it's when the concentrations of carbon	2 3	Q. So just to be clear, you think on the evidence you've seen at the moment that there probably was real
2 3 4	So, in principle, that is the definition of untenability. So it's when the concentrations of carbon monoxide, of toxics, or even visibility are such that it	2 3 4	Q. So just to be clear, you think on the evidence you've seen at the moment that there probably was real variability in the conditions of the stairs over time
2 3 4 5	So, in principle, that is the definition of untenability. So it's when the concentrations of carbon monoxide, of toxics, or even visibility are such that it disables the individual and eventually leads to its	2 3 4 5	Q. So just to be clear, you think on the evidence you've seen at the moment that there probably was real variability in the conditions of the stairs over timeA. Yes.
2 3 4 5 6	So, in principle, that is the definition of untenability. So it's when the concentrations of carbon monoxide, of toxics, or even visibility are such that it disables the individual and eventually leads to its death.	2 3 4 5 6	 Q. So just to be clear, you think on the evidence you've seen at the moment that there probably was real variability in the conditions of the stairs over time A. Yes. Q in this phase?
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1 MS GRANGE: Two topics, really: first the stair doors and 1 conventional behaviour in a stair. Having a hot zone 2 2 requires having hot gases entering, but at the same time then the roof. On the stair doors, I take it you're aware of 3 3 exiting, because the heat doesn't carry over, it just 4 stops after a certain region. 4 Dr Lane's more detailed investigation into the stair 5 5 So it does require quite an unusual pattern of doors and the fact that they may have actually been as 6 behaviour that needs to be really carefully looked at, 6 low as 20 minutes' integrity, fire resistance; is that 7 7 and it could be potentially associated to firefighter correct? 8 activity. 8 A. Yes. 9 9 Q. Could it be to do with multiple doors being held open at Q. Do you agree with Dr Lane that the stair doors being 10 different levels, thereby allowing the passage of smoke 10 held open or being jammed open, for example, by 11 and then an exiting of the passage of smoke? 11 firefighting equipment or other objects, appears to be 12 12 A. It is most likely necessary that there will be multiple the primary reason for the failure to maintain 13 doors open at the same time. 13 compartmentation as between the lobby and the stairs? 14 14 Q. Finally, there was a refuse chute door off the lobbies A. Well, whatever the reason was why they were left open, 15 with a refuse chute down with doors onto it. Those 15 if the doors were open, that would've been the primary refuse chutes -- is it right? -- were relatively 16 16 mechanism by which the stairs would've been compromised. 17 undamaged? 17 Q. As opposed to any issue about the integrity of those 18 A. Yes. 18 19 Q. Do you think those could've been some kind of refuge in 19 A. As I explained for the doors of the flats, the 20 this fire? 20 temperature at 20 minutes would've been of the order of 21 A. My attitude towards this type of thing is that if you 21 800-and-something degrees. So the lobby would already 22 design a place to be a refuge, then that place shall be 22 have had to be at about 800 degrees for the doors to 23 treated as such. In this particular case, we designed 23 fail. So if the doors were not at the best of their 24 the stair to be such and the stair failed, and so there 24 capabilities, it would've still taken a lot to make them 25 is no guarantee that any of the spaces could have been 25 fail. So I think opening of the doors is clearly a much Page 197 Page 199 1 an appropriate refuge for people. 1 more viable mechanism. 2 MS GRANGE: Professor Torero, that's the end of my 2 Q. Do you think any issues about the integrity to those 3 3 questions. doors are insignificant or do you think that they still 4 The convention is now that we just pause and have 4 have a role? 5 5 a short break to see if there are any more questions A. When we're talking about compartmentation, and, again, 6 6 we've discussed this issue that it is how you gain that I need to absorb. 7 THE WITNESS: Okay. 7 robustness to the system, the moment the doors are not 8 SIR MARTIN MOORE-BICK: We would normally have 5 minutes. 8 of the desired quality, clearly you're losing robustness 9 9 Do you want a bit longer? to your system. 10 10 MS GRANGE: It depends on what the people to my left are The problem with having poor quality doors is that 11 11 planning. We've got the time, so can we have their modes of failure are not necessarily only because 12 10 minutes? 12 of heat; they might sometimes not be placed 13 SIR MARTIN MOORE-BICK: I'll say 4.10. 13 appropriately, so they might introduce leaks. There's 14 14 MS GRANGE: Yes, thanks. numerous other mechanisms by which a poor quality door 15 SIR MARTIN MOORE-BICK: All right, we'll have a break for 15 can actually affect the performance of compartmentation. 16 10 minutes. Would you like to go with the usher, 16 Q. Finally, one question about the roof. 17 17 Based on what you know, had people been able to 18 All right, 4.10, then, please. 18 access the roof, do you think that could have provided 19 (4.00 pm)19 a kind of safe space, a safe refuge? 20 (A short break) 20 A. There is no evidence that evacuation through the roof or 21 (4.10 pm) 21 the roof as a safe haven can actually be appropriate. 22 SIR MARTIN MOORE-BICK: I think a few questions still. 22 I think there's been numerous incidents and there's been 23 23 many people thinking of ways by which you can gain the Yes. Ms Grange. 24 MS GRANGE: Not many, thankfully. 24 benefit of being outside, but it is something that

25

should not be promoted because there is no evidence that

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SIR MARTIN MOORE-BICK: Not many? There we are.

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25

the roof represents a safe space for people.
MS GRANGE: Okay. Those are all my questions. Thank you.
SIR MARTIN MOORE-BICK: Right.
MS GRANGE: I'd like to say thank you very much,
Professor Torero. I know you have put a huge amount of
work into your Phase 1 report, and I'm sure a huge
amount of work is going to go into your Phase 2 report
as well. We are extremely grateful for your time and
commitment to this inquiry. Thank you.
SIR MARTIN MOORE-BICK: Yes, and I'd like to endorse that.
We're really grateful to you for putting your undoubted
expertise at the disposal of the inquiry. You've
produced a very full and comprehensive report for us
already, for which we're very grateful, and now you've
explained certain aspects of it today. So it's been
extremely useful and, may I say, very interesting.
THE WITNESS: Thank you.
SIR MARTIN MOORE-BICK: Thank you very much indeed.
THE WITNESS: Thank you very much.
(The witness withdrew)
MS GRANGE: So, sir, yes, it's Professor Bisby tomorrow at
10.00, and Mr Millett will be taking him.
SIR MARTIN MOORE-BICK: Thank you very much.
Well, that's it for today. We'll break at this
point and resume tomorrow at 10 o'clock.
point and resume tomorrow at 10 0 clock.
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Thank you all very much.
(4.15 pm) (The begins edicumed until Wednesdey, 21 Nevember 2018)
(The hearing adjourned until Wednesday, 21 November 2018
at 10.00 am)
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