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Grenfell Tower Inquiry

Day 288

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Phone: 02045152252
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(10.00 am) Wednesday, }8\mathrm{ June 2022
(10.00 am)
SIR MARTIN MOORE-BICK: Good morning, everyone. Welcome to
    today's hearing. Today we're going to hear some expert
    evidence on the provision of water for firefighting
    purposes.
    Yes, Mr Kinnier.
MR KINNIER: Sir, may I call Dr Ivan Stoianov.
SIR MARTIN MOORE-BICK: Thank you.
            DR IVAN STOIANOV (sworn)
SIR MARTIN MOORE-BICK: Thank you very much. Now, please
    sit down and make yourself comfortable.
THE WITNESS: Thank you.
                (Pause)
SIR MARTIN MOORE-BICK: All right?
            Yes,Mr Kinnier.
            Questions from COUNSEL TO THE INQUIRY
MR KINNIER: Thank you, sir.
            Would you please confirm your name for the record.
A. Yes, my full name is Ivan lordanov Stoianov.
Q. Good morning, Dr Stoianov. Thank you very much for
    attending to give evidence this morning. It's much
    appreciated.
            Now, my questions are intended to be short and
    simple; sometimes it doesn't play out that way. If they
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    are in any way unclear, please say so and I' II rephrase
    them.
        Secondly, if at any stage during the giving of your
    evidence you require a break, please say so, that's not
    a problem.
        Thirdly, could you please remember that the
    stenographer is trying to capture everything you say and
    everything you say accurately, so if you could go at her
    pace, that would be much appreciated.
            Also, please, where you mean to indicate "Yes" or
    "No", say "Yes" or "No", rather than nod or shake your
    head as the case may be.
A. Yes.
Q. Now, you have provided two reports to the Inquiry. Your
    report entitled, "The provision and use of water for
    fighting the fire at Grenfell Tower on 14 June 2017",
    dated 20 July 2021, can be found at {ISTRP00000001}.
        Is that your report?
A. That's correct, yes.
Q. And you provided a supplementary report dated
    29 March 2022, which can be found at {ISTRPS00000001}.
A. Yes, correct.
Q. And that's your supplemental report?
A. Yes.
Q. Can you confirm that the facts and matters set out in
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Q. Now, if we look at the bottom of page 6

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\{\text { ISTRP00000001/6\} at line } 28 \text {, you say that your }
$$ expertise covers four things, and I quote:

"1. The design, operation and control of water distribution systems.
"2. Applied and fundamental research in the hydraulic modelling, pressure control and optimisation methods for water distribution networks.
environmental engineering by Imperial College; is that also right?
A. Correct.
Q. Can you help us, what was the subject of your doctoral research?
A. My work was very much focused on a phenomena in water supply networks known as pressure transients, so the work was based on mathematical modelling of this phenomena and also an extensive experimental work, and part of that work was in collaboration with Thames Water at the time.
Q. Thank you.

Is it right that you are currently a reader in water systems engineering at Imperial, and you hold a five-year fellowship in water systems engineering from the Engineering and Physical Sciences Research Council?
those two reports are true to the best of your knowledge and belief?
A. Yes, I confirm so.
Q. Is it correct that you have provided the reports in the same way that you would have provided an expert report to a court?
A. Yes, correct.
Q. Do your reports set out your opinions on the matters that are relevant to this Inquiry?
A. Yes, correct.
Q. Now, if we can go to $\{$ ISTRP00000001/6\}, we see here, at section 1.2 , you set out your expertise. If I could briefly just go through some of those matters.

First of all, you hold a diploma, a Bachelor of Engineering and an MSc, in civil engineering from the Faculty of Hydrotechnics at the University of
Architecture, Civil Engineering and Geodesy in Sofia,
Bulgaria, and those degrees were awarded in 1995; is
that right?
A. That's correct.
Q. And in 1998, you were awarded an MSc in environmental engineering by the Imperial College of Science,
Technology and Medicine here in London; is that right?
A. Correct.
Q. And in 2003, you were awarded a PhD in civil and

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"3. Pressure transients analysis in water
distribution networks."
Turning over the page \{ISTRP00000001/7\}:
"4. Experimental research in water distribution
networks that combines laboratory experiments and field
studies in complex networks."
Is that a fair summary of your expertise?
A. Yes, it is .
Q. You also lead a research group at Imperial called InfraSense Labs, which you founded in 2009, which focuses on the design, optimisation and control of water supply networks; is that right?
A. That's right.
Q. Am I right that you have no expertise in relation to firefighting, emergency planning or incident response?
A. Correct.
Q. If we could go to $\{$ ISTRP000000001/5\}, we see, midway down
the page at line 13 , section 1.1.2, where we find the heading "My Instructions". There you describe the questions which you were asked to address in your report, and I' II read them into the record so that they are known to everyone:
"1. How much water did London Fire Brigade (LFB) use during the Grenfell Tower fire both internally and externally, including:

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"a. the type of equipment available, the flow rate needed for optimal operation of each piece of equipment and the difficulties encountered in achieving the necessary flow rate.
"b. the number of water jets.
"c. their time of use.
"d. the duration of use.
"2. What were the locations of fire hydrants from which LFB supplied water for firefighting and their flow rate, discharge characteristics and conditions? Were there alternative water sources that might have been utilised by LFB?
"3. Based on evidence gather in the context of questions 1 and 2 , and using simulations created using that evidence, what was the water flow and pressure in Thames Water (TWUL)'s water supply network on the [night] of the 14th of June 2017? Was operational pressure consistent with the minimum pressure requirements?
"4. What was the response of TWUL, and was it effective ?"

Is that a complete summary of your instructions?
A. Yes, it is.
Q. Your supplementary report addresses two particular matters: first, your understanding of a meaning of
a British Standards document referred to in your main report; and, secondly, the conclusions of an LFB report testing some of its equipment. In broad terms, is that right?
A. That's right.
Q. Now, it's clear from these instructions, and it will become clear throughout your evidence, that your report inevitably touches upon actions taken by and decisions made by the LFB on 14 June 2017. Is it right that, while your report comments and draws conclusions about the Brigade's actions from a water or hydraulic perspective, you do not seek to draw conclusions on matters of operational firefighting or strategy, as these are outside your expertise and so outside the scope of your instructions?
A. That is correct. I made observations but, as you point out, these observations are by no means conclusions on the necessary actions for firefighting .
Q. Could we go to $\{$ ISTRP00000002/5\}, and line 24. You see there you say this:
"Where relevant to my instructions, investigation and conclusions, I have commented on the actions and statements of a number of individuals, including LFB firefighters and officers, Network Service Technicians and other TWUL employees. None of this analysis is

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intended, nor should it be taken, as personal criticism of the individuals concerned. I have no doubt that they acted to the best of their ability in the extremely difficult circumstances on 14 June 2017."

Am I right in understanding that's a point you'd particularly wish to emphasise before starting your evidence?
A. That's correct.
Q. Could we stay on this page, and we see in section 2.2, at the foot, you summarise there the various materials that you relied upon for the purposes of producing your report. I won't go through everything, but is it right to say that the materials identified in section 2.2 , which starts at page 5 and goes over to page 6 $\{$ ISTRP00000002/5-6\}, is the accurate summary of the evidence you've considered in reaching the conclusions set out in your report?
A. Yes, it is.
Q. Now those preliminaries are dealt with, Dr Stoianov, can I turn to deal with some basics that we probably need to establish before we turn to more of the detail.

The first element of the basics l'd like to discuss with you today is the water distribution network itself. A. Yes.
Q. Now, if we can go to $\{$ ISTRP00000003/5\}. Now, in this
chapter, in broad terms, you describe the water distribution network and its functions.

Now, in summary, is the water distribution system a complex network of pipes and valves used to transport water from storage, such as reservoirs and water towers, to customers and hydrants, either by force of gravity and/or with the assistance of pumps?
A. Yes, it is. It is a complex system.
Q. And the emphasis on the word "complex"?
A. Correct, and "system" as well.
Q. Secondly, the water distribution network's purpose is to provide water in an appropriate quantity at the appropriate pressure and of the appropriate quality, with minimal water leakage; is that, again, a fair summary of its purpose?
A. Yes, absolutely, with a slight correction: at minimum cost. Clearly leakage is part of these components of wastage we are trying to minimise, but actually the provision of these key variables needs to be done at minimum cost.
Q. Finally, your report refers variously to the water distribution network, to the water distribution system and to the water supply system. Am I right in understanding those to be interchangeable terms meaning the same thing?

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[^0]Q. And the water source could also be a pumping station; is that right?
A. That's right.
Q. The blue lines represent the water pipes or mains; is that right?
A. That's right.
Q. The black symbol with a red dot at its centre is a fire hydrant?

## A. Correct.

Q. We can see the red pumping appliance, which people would ordinarily know as the fire engine; is that right?

## A. That's right.

Q. At the top right we can see a building, a building with a dry rising main through which water is made available for internal firefighting ; is that right?

## A. That's right.

Q. And, finally, we can see in the bottom right a firefighter holding a handheld firefighting jet, which is known as a branch; is that right?

## A. Correct.

Q. Again, this is an example, and you might instead have depicted, for example, an aerial appliance or a ground monitor, which we will come on to discuss later in your evidence.
A. Absolutely. The purpose of this diagram schematic was

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very, very broad, just to highlight the different appliances, and, as you said, branches can be fed from the pump appliance.
Q. Thank you.

Now, in simple terms -- and apologies if this is too simplistic -- water travels from the source, through the system of pipes to a hydrant; the Fire Brigade can then use hoses to supply water from the hydrant to that pumping appliance, from which the water can then be pumped on through further hoses to firefighting equipment; is that a fair summary?

## A. Correct.

Q. You describe the water distribution network at Grenfell in chapter 6 of your principal report. For that purpose, could we go to $\{$ ISTRP00000008/8\}, and look at line 17. There you say this:
"Grenfell Tower is located within the Barrow Hill Zone ... which is part of the London Water Resources Zone operated by Thames Water Utilities Ltd (TWUL). TWUL is the statutory water undertaker for a large geographic region, which includes the whole of Central and Greater London ..."

First of all, does that remain a correct summary?
A. That's right.
Q. Now, if we can stay in this chapter but go to page 10
$\{$ ISTRP00000008/10\}, we can see there, in the top part of that page, you list five sources of water which can supply water to the Barrow Hill zone in which the tower was found: we have the Barrow Hill reservoir, the Willesden reservoir, the Hammersmith pumping station, the Holland Park shaft and the Barrow Hill shaft.

Now, is it right that the two reservoirs supply water by gravity; in other words, they store water at a higher altitude than the buildings and customers they supply, so there is no pumping arrangement required?
A. Yes. The set-up is a little bit more complex, and I have another figure which explains this. The way this set-up operates in that particular system is water is pumped from a pumping station in Hammersmith. From there, it supplies water during the day, both in terms of the very large set of water transmission mains and distribution mains, and during periods of low demands, the reservoir balances that supply and demand. So it could be that sometimes it's pumped water, so it's pressurised ; it could be that, at nighttime, when the pumps are turned off, then the actual water from the reservoirs is fed by gravity into the same distribution networks.

So there is this notion of flow reversals across these water transmission mains. It depends on

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balancing, again, that supply and demand.
Q. Apologies, again, I may be making matters too crudely simple, but, in essence, the Hammersmith pumping station, the Holland Park shaft and the Barrow Hill shaft supply water by pumping it from the Thames Water ring main; is that essentially correct?
A. Yes, and again, a slight sort of distinction here. I know these are small technical details probably, but the actual Hammersmith pumping station can feed water from the London ring main, but equally directly through a set of transmission mains from the pumping station in the west of London.
Q. Now, could I turn on to the three key factors for the provision of water for firefighting.

To that end, could we go to $\{$ ISTRP00000003/17\}. We can see, at section 3.1.4, you say that:
"From a hydraulic perspective, three key factors affect the provision of water for firefighting ..."

Is it right that you include the qualification "from a hydraulic perspective" because there may well be other factors outside your knowledge and expertise which are relevant for a fire service from an operational perspective?
A. Correct.
Q. Whereas here you focus strictly on the physical
requirements for the supply of water; is that right?
A. That's right, yes. There are other factors which, as you highlighted, is beyond the hydraulic control.
Q. Thank you.

Now, the first key factor you identify for this purpose is at point 1 , and it is the available quantity of water; put bluntly, the amount of water that is stored in tanks or elevated reservoirs within the water distribution network accessible through hydrants. Again, essentially, is that correct?
A. That's right.
Q. Now, you have mentioned water from tanks and reservoirs here, but presumably that would also include water available from pumping stations?
A. That's right. I mean, it's a complex system of all these storage facilities, such as reservoirs, service reservoirs, et cetera, but equally they are supplied by pumping stations, treatment works, et cetera. So it's part of this large complex system.
Q. Again, at its simplest, in relation to the water distribution system at Grenfell, this would include water available from all the sources we have been discussing: Barrow Hill and Willesden reservoirs, Hammersmith pumping station, and the Holland Park and Barrow Hill shafts; is that right?

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## A. That's right.

Q. Is it right that the available quantity of water is fundamental because, in plain terms, if there is not enough water available, that diminishes the adequacy of firefighting efforts?
A. That's right. One of the components is the availability . Clearly, as we see, there is other components later probably in the discussion, but yes, availability is number one.
SIR MARTIN MOORE-BICK: When we're talking about quantity available here, are we really looking at the total volume of water in the system?
A. So generally we try to satisfy particular physical laws, and these physical laws for us is the conservation of mass, so I need to have a certain volume of water which I need to use. The second question is: can I use it at the right time and the right place? But as far as the storage is concerned, that system had infinitely larger storage than it was required for firefighting.
SIR MARTIN MOORE-BICK: Well, that's rather what I had in mind, but all right, you have explained that. Thank you very much.
MR KINNIER: Now, the second key factor you identify there, at point 2 on page 17 \{ISTRP00000003/17\}, is the water flow rate delivered from fire hydrants to pump

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appliances.
    In layman's terms, when we talk about flow rate from
    a hydrant, we are referring to how much and how quickly
    that hydrant can supply water to the pump appliance; is
    that right?
A. Correct.
Q. If we stay on page 17, you highlight three particular
    things on which the flow rate from a hydrant to a pump
    appliance depends. We can see a, starting at line 17
    there. First of all, the water pressure in the pipe
    which supplies the hydrant.
    Can you help us, what is the difference between
    water flow rate and water pressure?
A. Well, these are fundamentally different variables. So
    pressure, in our case, this is the force which the water
    would apply on the pipe wall, and that force we
    generally -- we define as water pressure. We can
    express water pressure in different terms, in different
    units.
    Flow rate will be the volume of water going across
    a section over a certain period of time. So if I, in
    a very simplistic term, open a tap at home to have
    a shower, the flow rate will be, let's say, 100 litres
    per minute or so, and that is kind of the volumetric
    flow going over a particular time over that particular
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## cross-section.

So these are two fundamentally different variables.
SIR MARTIN MOORE-BICK: Well, presumably you can have a high pressure and a very low flow rate, as when you puncture a garden hose, (inaudible) --
A. Yes. Let me explain with this bottle, for example. If I squeeze this bottle, I will increase the pressure into the bottle. If I have a very tiny hole into that bottle, I will get a very little flow rate, irrespective of how much I squeeze this. So the actual flow discharge, whether it's through a fire hydrant, whether it 's through a branch, whether it's through a leak, they're all governed by the same physical phenomena, which is a discharge through an orifice, and that discharge through an orifice depends on the discharge characteristics of that orifice and the differential pressure. In other words, if I'm discharging to the atmosphere, that will depend at the pressure at the inlet to that nozzle or pipe or fire hydrant, et cetera.
SIR MARTIN MOORE-BICK: Thank you.
MR KINNIER: Thank you. I'm relieved the top was on your bottle as you demonstrated that.
A. Yes, no, I made sure that that's the case.
Q. The higher the water pressure in the pipe serving the hydrant, the higher the flow rate from the hydrant; is

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A. It is correct.
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Q. The second point you identify at point $2 b$ at line 19 is the flow coefficient of the hydrant. We will return to flow coefficients in detail later on, but in layman's terms, is it right to say that a hydrant's flow coefficient is a measure of how great a flow rate the hydrant can provide, given the pressure of water it receives?
A. Correct. This is very much as I just mentioned about these fundamental principles of flow discharge through an orifice. It depends on the characteristics of this orifice, which in this case will be expressed by the flow coefficient, and the differential pressure across that orifice.
Q. Again, just to sort of flow from that point, for want of a better phrase, the flow coefficient is important because if a hydrant has a very low flow coefficient, even if it is provided with good water pressure, it will provide a low water rate. In essence, is that right?
A. That is correct. I mean, if you look at the flow discharge across an orifice, we would have this kind of flow coefficient multiplied by the square root of this differential pressure, or the pressure. That means that, in very simple mathematical terms, if I increase

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the pressure twice, that will be the square root of this number 2 , which would be -- so it gives me $40 \%$ increase in the flow rate across that orifice. So, consequently, the flow coefficient is a very key part for me to reach the final objective, reaching particular discharge across that hydrant or branch or whatever.
Q. Thank you.

The third point we see at point $c$ at line 21 is the energy or pressure losses between the hydrant and the pump appliance, and pressure losses can be caused, for example, by kinked hoses due to increased friction; is that right?
A. Correct. I mean, the other -- as I earlier stated, you know, water in a conduit or a flow in a conduit will be governed by certain physical laws, and part of it is this kind of notion of pressure loss or pressure head loss. That is a lot to do with the conditions of the pipe and the conduit, there will be a lot to do with a certain additional turbulence that might be occurring. So in the example you just highlighted, for example kinked hoses or even hoses with a larger length with a lot of interconnections, couplings, that can introduce additional head loss into that particular system.
Q. Thank you.

If we could stay in this chapter but go to page 20
\{ISTRP00000003/20\}, at the top of the page, at section 3.2.5, you explain the concept of continuity of flow. In lay terms, the flow rate delivered from the hydrant to the pump appliance is important, because if it is not high enough to maintain continuity of flow, the pump's tank will gradually empty, which means that the water supply to firefighting equipment will be paused whilst waiting for the tank to refill. Again, is that a fair summary?
A. Yes. I mean, water is not compressible, so, as a result of that, whatever we get into that tank, that's the same volume we'll be able to get out of that tank, and the actual pump appliance has a storage tank which is not very large, it 's only about roughly 1.4 cubic metres of water, so it's about 1,400 litres storage capacity, and you have to balance. Whatever comes into that tank needs to be equal or greater to whatever comes out of that tank which goes through the centrifugal pump installed on the pump appliance.
Q. Thank you.

If we can go back to page 17 \{ISTRP00000003/17\}, we see at line 25 the third key factor you identify which is the provision of water for firefighting is the flow rate and pressure at the branch, nozzle, monitor, aerial appliance or dry rising main.

Again, in simple terms, that means the flow rate and pressure at the end piece of the firefighting equipment; in other words, whatever it is that actually projects the jet of water; is that right?
A. That's right.
Q. And the higher the pressure and the higher the flow rate of the water going into a piece of equipment, the higher the volume and/or distance of water it can project; again, in its basics, is that right?
A. It is. I mean, the water jet, ultimately, we need to kind of transform certain kinetic energy into that water jet, and that kinetic energy will be a function of the volumetric mass of a certain confined volume, and equally the velocity of that flow rate. So that's why any forms of branch or a nozzle has these optimal operational specifications, and this operational specification takes this trade-off between safety, safe operation of that nozzle, and equally maximising flow rate and reach of the jet projected from that nozzle.
Q. Thank you.

I now want to turn to the second part of the examination today, which is water deployment on 14 June 2017.

Now, this subject is addressed in chapter 5 of your report \{ISTRP00000006\}, where you set out a detailed
Q. So, put in layman's terms, each piece of equipment will have a pressure rating and a flow rating which describe

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the maximum water pressure and the maximum flow rate at which the equipment can be safely used. Is that right in its essentials?
A. It is right, because that balances the notion of the maximum effectiveness of the use of that equipment and its safe operation.
Q. Where do the rated pressure and flow figures come from? What's the source of that information?
A. So generally the source of that information is based on the manufacturer's specifications. Ultimately, the manufacturer, it's their obligation to be able to identify, through testing and validation, the balance of these trade-offs, and probably there will be some safety factors, so in other words these figures might not fully represent the actual capabilities of this equipment because they need to allocate for some unsafe potential use of that equipment, and the safety factors take into account those particular conditions.
Q. Is it right that the rated flow and pressure figures are also sometimes referred to as the nominal or optimal flow or pressure figures?
A. That's the general use in the engineering language and kind of applications, but I have not been able to identify that into the LFB documents.
Q. Now, in your report, you calculate the utilisation rate

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paragraph 3, you there identify difficulties encountered in supplying water for firefighting from the water distribution network. Finally, at paragraph 4, you deal with alternative water supply sources that might have been used by the LFB.
Is that a fair summary of the structure of chapter 5?
A. That's right. So in chapter 5 I tried to systematically look at the utilisation of water jets, as the first instance, so $I$ had access to a number of visual --
Q. I'm sorry to interrupt.
A. Yes.
Q. We'll come on to that.
A. I apologise, yes.
Q. I was really inviting you just to confirm that was the structure.
A. I confirm, yes.
Q. Okay.
If we can go to $\{$ ISTRP00000006/4\}, over the page, the report states, and I think this is the point you were coming on to:
"The evidence presented in this Chapter has been gathered from sources including witness statements, video footage provided by the National Police Air Service ... video footage from body-worn cameras
of firefighting equipment by comparing the flow rate that the equipment received on the night with its rated flow figure; is that right?
A. Correct. So I strongly believe in this sort of notion of cumulative gains. So, in other words, if you want the final outcome, which is to project a water jet at its maximum reach and its maximum flow rate, because that will be the best chance to offset particular heat release rate, that means that that equipment needs to be operated as close as possible to the specified rated values.
Q. Just giving a practical example in layman's terms of the point you have made, if a particular piece of firefighting equipment had a rated flow of, say, 1,000 litres per minute, but received an actual flow rate of 500 litres per minute, you would describe that handheld branch as being 50\% utilised or as having received $50 \%$ of its rated flow. Is that a practical example of the point you're making?
A. It is, because that will have ultimately the impact on the reach which that water jet can reach, and equally it will have an impact on the ability to stop certain heat flux occurring on a particular ignited surface.
Q. Now, if we can go back to the page on the screen, which is page 3 \{ISTRP00000006/3\}, and we see, at line 22 ,

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provided by the Metropolitan Police Service ... and other sources as referenced in the report."

Is that a fair summary of the materials you have relied upon?
A. Correct, and that material provides very high granularity in terms of time on the utilisation of the water --
Q. Now, you refer to other sources in addition to those listed here. Those other sources include documents, disclosure from the LFB and from manufacturers relating to firefighting equipment; is that right?
A. Correct.
Q. You also refer to evidence given by firefighters during Phase 1 of this Inquiry; is that right?
A. Correct.
Q. Is it right that there are also some limited instances where you've relied upon photographs of the tower taken by members of the public or press on the day of the fire which have been published online?
A. Correct.
Q. Now, taking those sources together with those listed at the top of page 4 of chapter 5 , does that represent a comprehensive summary of all the sources you reviewed for these purposes?
A. It does.

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Q. Now, if we can stay in this chapter but go to page 7 \{ISTRP00000006/7\}, we can see, starting at line 16 onwards, you list the external jets, which you have labelled jets A through to J, which were deployed by the LFB on 14 June from the first arrival of the Brigade until about 1 o'clock in the afternoon; is that right?
A. That's correct.
Q. Now, what I'll do, Dr Stoianov, is I' II go through each of these jets with you.
A. Okay.
Q. First of all, jet A, which was a handheld branch on the east side of the tower which was first projected at 01.15 hours.

Now, a handheld branch is simply what one might describe as a handheld firefighting hose; is that right? A. That's right.
Q. Now, we can see an example in your report of handheld branches used.

Before we look at that, I should say that there is a trigger warning for people in the room and who are watching. We are about to see some still images which show the fire on the exterior of the tower, so anybody who feels uncomfortable about that should take steps to leave the room or the live stream now, or otherwise protect themselves. I will wait a few moments to allow

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people to do that if needed.
            (Pause)
        So if we can go to figure 5-17 on page 27 of this
    chapter, which is page 37 with the Opus reference
    {ISTRP00000006/37}, we can see, in figure c, there is
    a green oval symbol at the bottom right of that, and
    that is a photograph of a handheld branch being held by
    two firefighters; is that right?
A. Correct.
Q. This is what you refer to as jet A?
A. Correct.
Q. If we can turn over the page to page 38
    {ISTRP00000006/38}, we find figure 5-19, which is the
    second set of images on that page, and here we see three
    types of handheld branch used by the Brigade; is that
    right?
A. Correct. The video and any evidence I have come across
    very much indicates the first two branches. I have not
    seen any evidence that the third one, Delta Attack
    400-S-Pro, has been used.
Q. Thank you.
    Now, if we could go back to page }7\mathrm{ {ISTRP00000006/7}
    and the list of jets you helpfully provided, we see
    at b, at line 17, jet B, which you describe as the
    Alpha 213 turntable ladder east, was utilised
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    continuously between 01.47 hours and 02.05 hours, with
    about 60% of its rated water flow of 2,000 litres per
    minute.
        Now, am I right in understanding that this was the
        first of the three aerial appliances deployed by the LFB
        at Grenfell?
A. Correct. Again, we need to be careful by stating three,
    because the second aerial appliance, A245, actually was
    never deployed as a -- the monitor of that aerial
    appliance was not deployed. There was a high-pressure
    hose stuck to that particular appliance. So just to
    kind of be very accurate with that statement, I would
    say out of the probably two deployed aerial ladder
    platforms.
Q. Okay.
    Now, again, just dealing with basics, aerial
    appliances are fire engines with a ladder or a cage
    which is capable of being extended; is that right?
A. Correct.
Q. Now, you noted here that Alpha 213 received only
    approximately 60% of its rated flow. We will come on to
    that later, but I just want to sort of put a place
    marker for that particular point here now.
    Next, jet C, which you describe as a ground monitor
    on Grenfell Walk, which you note is to the south and
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east of the tower, which was used intermittently between 02.41 hours and 11.30 hours.

Now, just looking at basics for these purposes at the moment, Dr Stoianov, a ground monitor is a water nozzle which sits in a frame, enabling it to be placed on the ground and aimed in a particular direction without the need for firefighters to hold it as if they were holding a normal firefighting branch. Is that an accurate description?
A. Correct.
Q. We can see an illustration of a ground monitor to remind people, which is at page 21 in this chapter $\{$ ISTRP00000006/21\}, at figure 5-6. Thank you. That's what we're referring to here.
A. Yes, and just for clarity, that ground monitor can be used with different nozzles, and that sort of figure also indicates the use of these different nozzles. One of them is the Mercury adjustable flow nozzle, and the other one is the plain deluge tip, or what we refer to normally as a smooth bore nozzle.
Q. Thank you.

Could we go back to page 7 \{ISTRP00000006/7\}, and if we could look at $d$, which is at line 22 , you identify jet $D$, and you describe it thus:
"A245 Aerial Ladder Platform ([on the] East [side of

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the tower]) was utilised for less than one minute at 02:13 hrs, and then continuously between 03:28 hrs and 09:45 hrs (with a pause between 06:57 hrs and 07:14 hrs)."

Aerial ladder platform, or ALP, 245 was, I think,
the second of the three aerial appliances deployed, and if you could bear with me in saying there were three deployed just for the sake of clarity in establishing basics first, before going into detail.

Is that right?
A. Correct.
Q. Now, at the bottom of page 7, at paragraph 1e, it says this:
"Jet E: S13A1 Surrey Aerial Ladder Platform ([on the] East [side of the tower]) was utilised after 10:47 hrs ..."

Now, jet E is, I think, another aerial appliance, which you refer to as the Surrey aerial appliance; is that right?
A. Correct.
Q. If we turn over the page to page 8 \{ISTRP00000006/8\}, line 3, we have:
"Jets [as in the plural] F: multiple handheld branches for extinguishing burning debris on the East side (utilised intermittently)."

Here again, apologies for asking you about what may be the obvious, but burning debris refers to ignited material that was falling from the tower to the ground; is that right?

## A. That's right.

Q. So these jets were aimed not at the tower, as such, but at burning debris on the ground surrounding the tower; is that right?
A. Correct.
Q. We have next:
"Jet G: a handheld branch for burning debris on the South side."

We then have, going down the page to line 11 :
"Jet H: a covering water jet from a handheld branch initially , which was later (after $\sim 05: 00 \mathrm{hrs}$ ) replaced with a ground monitor (Northwest corner). The water jet was projected intermittently between $\sim 02: 43 \mathrm{hrs}$ and ~10:52 hrs."

Can you help us here, what do you mean by a covering water jet?
A. So that's a water jet which was projected from the ground monitor onto the tower, and that specific one, it 's the water jets on the northwest corner.
Q. Next, jet I, which is dealt with at line 15 :
"A covering water jet from a handheld branch

$$
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$$

(West side). The water jet was projected intermittently between $\sim 02: 45 \mathrm{hrs}$ and 03:45 hrs."
Is that right?
A. Correct.
Q. Finally:
"Jet J: a covering water jet from a handheld branch (West side [again]). The water jet was projected intermittently between $\sim 03: 20$ hrs and $\sim 10: 52$ hrs."

Is that all the jets that you have identified for the purpose of the report?
A. Correct, and just to say I believe I have high confidence into that list based on the very high granularity of the visual data which was provided to me.
Q. Now, these ten jets, A through to J, describe all of the external water jets deployed at Grenfell from the start of the fire until about 1.00 in the afternoon; is that right?
A. Correct.
Q. Just going back to basics, so we know what we're dealing with in this chapter, this chapter also describe the supply of water to the dry rising main, as we can see at page 8 \{ISTRP00000006/8\}, point $k$, a hose you refer to as supply K , which was also used to supply water to the inside of the tower.

Is it right, though, that the focus of your analysis
A. Correct. So supply K, I think we have to -- this was --
particular emphasis was the north and west sides of
Grenfell Tower. Clearly, the supply of the dry riser
main was done through the south side, where the actual
breeching valve was placed, so that's not explicitly
mentioned into this list.
Q. Thank you.
Now, each of the jets deployed at Grenfell, whether
a handheld branch, a ground monitor or aerial appliance,
was supplied by a pump appliance; is that right?
A. Correct.
Q. Now, we don't need to go to them, but at pages 10
through to 11 of this chapter \{ISTRP00000006/10-11\}, you
identify the six pump appliances which were used to
supply the jets deployed, and they were pumps Golf 271,
Golf 272, Alpha 241, Sierra 13 Police 1, Hotel 421 and
Alpha 431; is that a fair summary?
A. That's right.
Q. Those pump appliances were, in turn, supplied with water
from a total of four hydrants. First of all, let's deal
with the basics: is that right?
A. Yes, it is.
Q. Now, if we can stay in this chapter but go to page 6 $\{$ ISTRP00000006/6\}, and if the map could be expanded,

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that is a map of the area immediately surrounding
Grenfell Tower, and the tower itself is the bright green box labelled "GT". Is that right?
A. Correct.
Q. The four larger circles highlighted in yellow show the four hydrants used to supply water on the night; is that right?
A. Correct.
Q. If we can take these in turn.

First of all, H 1 is a fire hydrant located to the southeast of the tower under Grenfell Walk; is that right?
A. Correct.
Q. H3 is a fire hydrant located on the intersection of Grenfell and Bomore Roads; is that right?
A. That's right.
Q. H8 is a fire hydrant located on Bramley Road; is that right?
A. That's right.
Q. And hydrant $\mathrm{WO} / \mathrm{H} 5$, seen here to the right of the tower, is located next to the Kensington Leisure Centre; is that right?
A. That's right, it 's between the Kensington Leisure Centre and the Aldridge Academy.
Q. Just so people understand, the letters WO are important
here, and we will discuss their importance later, but WO stands for wash-out; is that right?
A. That's right.
Q. Finally, this figure also shows, with the smaller red and blue circles, other fire hydrants in red and wash-out hydrants, which are in blue, situated in the vicinity of Grenfell Tower, but which were not used on the night; is that right?
A. That's right.
Q. Now - -
A. Just going one $--I$ apologise. One extra thing here I just wanted to emphasise is the private hydrant which is in close proximity to H 1 . That private hydrant was labelled the most appropriate hydrant in the ORD for the pre-determined attendance specification.
Q. Thank you. We will come on to these matters in due course.

Can we first, though, before we come on to those other topics, low flow rates, and I'd like to turn in particular to your conclusions about that topic and the flow rates delivered to aerial appliances and ground monitors on 14 June.

If we can go in this chapter to page 236
\{ISTRP00000006/236\}, at point 2 you conclude as follows:
"Of the three aerial appliances and two ground
monitors which projected water jets onto Grenfell Tower on 14 June 2017, none were supplied with their rated water flow rate."

If we go on further, between pages 236 and 238 \{ISTRP00000006/236-238\}, you go on to describe the specific details of each aerial appliance and ground monitor's rated flow figure compared with the flow rates which you estimate that they received on the night.

We don't need to go through all of that detail which is set out on the next three pages, but can I summarise that content and see whether you agree with the summary or not.

First of all, Alpha 213 received about $60 \%$ of its rated flow; is that right?
A. Correct.
Q. Alpha 245 received between $16 \%$ and $20 \%$ of its rated flow; is that right?
A. That's right.
Q. Thirdly, Sierra 13 Alpha 1 received between $12 \%$ and $19 \%$ of its rated flow.
A. Correct, but for Sierra 13A1, we should also bear in mind that the actual monitor has a minimum flow rate, and that minimum flow rate was not reached. So although I can provide a value of whatever percentage was delivered, we should bear in mind that the actual flow
Q. Now, what I'd like to deal with next is how you calculated the flow rate figures.

Now, first of all, the mathematical model was provided by Thames Water, which you then validated with practical testing carried out in 2018 and with data available from the night of the fire to ensure that it could accurately predict the flow and pressure

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conditions in the network at different times and locations during the fire. That in turn allowed you to estimate the flow rates delivered to the various pieces of firefighting equipment.

Now, that's high level, but is that, in its essence, a correct summary of the approach you took?
A. It is, and I just want to add to that that clearly these mathematical models, as we call them, hydraulic models, we have very high confidence into these models. These are not just some abstract, highly uncertain -- we commonly use them in a number of incident management and it 's commonly used by the UK water industry as a whole.
Q. Modelling has its critics.
A. Yes.
Q. Can you briefly $--I$ emphasise the word "briefly" -describe why you think the results are reliable, or at least tolerably reliable?
A. Because in terms of the actual model, I have taken a very robust approach towards the validation through -used a lot of experimental work, so I have very high confidence in the model, in the hydraulic model, and equally through the testing of the flow coefficients of the hydrants, I have now very good understanding about their discharge characteristics. In combination with understanding of the pressure and flow within the
network and the flow coefficients of the hydrants, I can derive very -- pretty accurate estimates of the flow rates coming out of these hydrants.
Q. Now, can I turn on to the next topic, which is the consequences of low flow rates.
A. Sure.
Q. Now, your report describes three consequences of low flow rates delivered to the aerial appliances and the ground monitors, and I just want to identify them at the start, Dr Stoianov, and then we'll come to deal with the detail in due course.

First of all, they limited the vertical reach of the jets projected onto the tower; is that right?
A. Correct.
Q. Secondly, the low flow rates caused interruptions to the jets; is that right?
A. Correct, so the jets were not consistent.
Q. Thirdly, the low flow rates meant that some equipment could not be deployed as intended; is that correct?
A. Correct.
Q. Can I deal with the first one of those consequences, which is limited vertical reach.

Now, as you've confirmed, the low flow rates limited the vertical reach of jets. Now, before we go any further, again dealing with basics, vertical reach
simply refers to the maximum height reached by the projected water jet; is that right?
A. Correct.
Q. Your analysis identified that the three aerial appliances deployed at Grenfell Tower --I use that phrase advisedly, but for the sake of clarity -- which were able to reach higher than any other jets, achieved maximum vertical reach of approximately 35 metres, which is 13th floor; 47 metres, the 17 th floor; and 52 metres, the 19th floor, respectively; is that right?
A. That was on the night of the fire, yes, as used.
Q. Now, if we can go to page 238 \{ISTRP00000006/238\} and look at paragraph 3, you conclude this:
"A213 [turntable ladder], A245 [aerial ladder platform] and S13A1 [aerial ladder platform] were capable of projecting water jets to the full height of the tower $(64.5 \mathrm{~m})$ if supplied with their rated flow and nozzle pressure from the pump appliances."

Now, if we could turn back to page 52 in this chapter $\{$ ISTRP00000006/52\}, we find, at figure 5-29, an annotated graph, and this graph is provided by the manufacturer of one of the aerial appliances, I think Alpha 213, and you have added the writing in blue. Are those points correct?
A. They are.
Q. Now, we don't need to go through the graph in detail, but I'd like to look in particular at your blue markings and comments on the graph.
A. Yes.
Q. Now, you note that the graph shows that, when provided with the correct flow rate of 2,000 litres per minute, this appliance can project water to a maximum height of 35 metres from the nozzle, and adding the maximum height of 30 metres at which the nozzle can be positioned using the appliance's cage, that comes to a total of approximately 65 metres. That is the basis for your conclusion that this particular aerial appliance, Alpha 213 , had a maximum possible vertical reach of 65 metres, which you note is to the top or thereabouts of Grenfell Tower.

Is that a fair summary of your conclusion annotated there?
A. Correct.
Q. Now, Grenfell Tower is 65.4 metres high, slightly more than 65 metres. Is it right, put differently and in lay terms, that the maximum vertical reach of Alpha 213 is there or thereabouts the total height of the tower?
A. Correct. Just to add to that, clearly, is that the manufacturer provides what they call the effective reach, clearly, and that effective reach is based on,

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again, specific consideration about safety and et cetera. That's an orifice discharge. So if we can actually provide $10.5,11$ bars, even a very small deviation on that particular appliance or that particular monitor, that can even reach a little bit higher.

The other thing is that that water jet will be affected by environmental conditions. We know that on the night of the fire the wind was very low, we have the information from the weather stations. So as far as the environmental conditions go, my assumption is, my hypothesis is, that they had very little impact.

So, in summary, yes, 65 metres is my estimate, but that sort of 40 centimetres you're referring to here, it's certainly probably within the maximum reach, not the effective reach. The effective reach is normally about $10 \%$ of the maximum reach.
Q. Just picking up the variables that are in play here, achieving the maximum possible height depends not just on supplying the appliance with the rated flow rate, but also on the jet itself being projected at the optimal angle. Is that right?
A. That's correct, yes, and equally, I'm sure we'll touch later, but the actual experimental results which I have been provided very much substantiate these results.

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Q. Just looking at this graph, what we see is the tallest
    blue line -- or, rather, I think this is what it
    shows - - is for a jet aimed at a 30-degree angle, but if
    the jet is pitched at a shallower angle, for example
    40 degrees, the green line on this graph, the maximum
    height reached by the jet falls, at least to the lay
    eye, quite significantly ; is that right?
A. Correct.
SIR MARTIN MOORE-BICK: Can we just make sure we've
    understood this correctly. The angle of attack is the
    angle at which you are directing the jet; is that right?
A. Correct.
SIR MARTIN MOORE-BICK: And it looks to me as though the
    blue line is an angle of attack at 75 degrees; is that
    right?
A. Well, it depends how we measure the angle, but yes. So
    I think you're absolutely right, the angle of attack
    here on the blue line would be }75\mathrm{ degrees.
SIR MARTIN MOORE-BICK: So you've got to point it as high as
    possible --
A. Correct.
SIR MARTIN MOORE-BICK: -- to get that extent of jet reach
    in the vertical plane?
A. That's right. But when you look at just very basic
    trigonometry here in terms of angle, distance, where the
        45
    actual aerial appliance was positioned, I don't think
    that was an obstacle, to project that water jet at that
    particular angle.
SIR MARTIN MOORE-BICK: Well, you may well be right, I just
    wanted to ensure that we'd understood the colours
    correctly.
A. Yes.
SIR MARTIN MOORE-BICK: But since I've now broken into
    Mr Kinnier's line of questioning, I might ask one
    further question.
        The horizontal reach shown on the graph --
A. Yes.
SIR MARTIN MOORE-BICK: -- what is that telling us?
A. So clearly that shows us what is the furthest away reach
    which a jet can outreach. So if, let's say, this
    monitor is deployed in a situation where potentially the
    objective is to outreach the fire on an industrial
    estate or whatever, you probably want to be at a safe
    distance but have that outreach in terms of horizontal
    distance and consider that horizontal distance. So
    that's the variations between the angle of projection
    and also the reach and the trajectory of that water jet.
SIR MARTIN MOORE-BICK: Is this graph telling us that in
    order to project a jet 35, let's say, metres above the
    nozzle --
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A. Yes.

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A. Yes.
SIR MARTIN MOORE-BICK: -- you've got to be only }20\mathrm{ metres
SIR MARTIN MOORE-BICK: -- you've got to be only }20\mathrm{ metres
    horizontally from the point at which you want that to be
    horizontally from the point at which you want that to be
    achieved? Is it telling us that?
    achieved? Is it telling us that?
A. No, no. This is --
A. No, no. This is --
SIR MARTIN MOORE-BICK: Ah.
SIR MARTIN MOORE-BICK: Ah.
A. No. So if you want to project it as -- so that's why
A. No. So if you want to project it as -- so that's why
    I'm saying it's very basic trigonometry. So if you take
    I'm saying it's very basic trigonometry. So if you take
    a triangle and I want to project at -- and I have the
    a triangle and I want to project at -- and I have the
    angle and I have the distance, I can very much
    angle and I have the distance, I can very much
    sort of -- the calculation in that particular case is
    sort of -- the calculation in that particular case is
    probably about 8 to 9 metres distance, in answer to your
    probably about 8 to 9 metres distance, in answer to your
    question, I can achieve -- from the object where I want
    question, I can achieve -- from the object where I want
    to project it, I' |l be able to achieve that 75% angle.
    to project it, I' |l be able to achieve that 75% angle.
SIR MARTIN MOORE-BICK: Well, let me ask my question in
SIR MARTIN MOORE-BICK: Well, let me ask my question in
    a slightly more practical way.
    a slightly more practical way.
            How close to the building would you need to be in
            How close to the building would you need to be in
        order to project a jet }35\mathrm{ metres from the top of the
        order to project a jet }35\mathrm{ metres from the top of the
    ladder?
    ladder?
A. About }8\mathrm{ metres.
A. About }8\mathrm{ metres.
SIR MARTIN MOORE-BICK: Ah.
SIR MARTIN MOORE-BICK: Ah.
A. But, equally, if you bear in mind that the way Alpha 213
A. But, equally, if you bear in mind that the way Alpha 213
    was positioned, it was positioned very close to the
    was positioned, it was positioned very close to the
    building, but equally the projection was not done in
    building, but equally the projection was not done in
    that direction (indicated), most of the time the
    that direction (indicated), most of the time the
                                    4 7
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                                    4 7
    ```
projection was done along the building. In other words, we didn't have that exact constraint. The actual ladder could have been even pulled a little bit more along the east side and, again, the projection could reach to the top of the building without these constraints. And equally, A245, in terms of distance, was the ideal distance to achieve that projection.
SIR MARTIN MOORE-BICK: Yes, that's helpful. Thank you very much.
Yes, Mr Kinnier.
MR KINNIER: Just flowing from the Chairman's questioning, can we go to \(\{\) LFB00123672 \}. As we can see on the screen, this is a report prepared by the LFB dated 12 November 2021, entitled, "Flow tests conducted on aerial appliance types used at Grenfell Tower fire".
If we go to page 2 of this document \(\{\) LFB00123672/2\}, we see, in the third paragraph, the report says this:
"The flow tests summarised within this report were designed to assess the operational capability and performance of LFB equipment within the optimal working parameters as provided within the Dr Stoianov Report, to ascertain whether the calculated provision of water could be achieved in an optimised working environment (with equipment in service at the time of the Grenfell Tower Fire)."
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Now, in simple terms, the report seeks to test
vertical reach of the aerial appliances could be achieved in practice. Was that your understanding of the overall point of the LFB's tests?
A. Correct.
Q. Now, if we can go to the final paragraph of this introduction on page 2 , which is immediately above the emboldened heading "Turntable Ladder ... and monitor",
it explains that the testing was carried out on
25 August and 6 September 2021 and, looking at the middle of the second line of that paragraph, and I quote:
"All of the equipment assessed as part of the performance tests was produced by the same manufacturer and of the same model as that which attended the Grenfell Tower Fire on 14 June 2017."

We can see from the bottom of page 2 that the LFB tested a turntable ladder, and if we go over to page 3 \{LFB00123672/3\}, what's described there is an aerial lift platform, sometimes described as an aerial ladder platform as well, and an Akron Mercury quick attack monitor, otherwise known as a ground monitor; is that right?
A. Correct. The only thing I would like to add to this --

## Q. Yes.

A. -- is that all of this equipment is described, the report does not explicitly specify the serial numbers of the monitors and the nozzles used into these tests.
Q. And why is that important?
A. Well, generally we can even further validate with the manufacturer whether these specific serial numbers have gone through the kind of testing which the manufacturer provides, and that gives additional reassurance. Also, it 's important for us to really cross-reference the tests which LFB have done, which I think implicitly, the statement is, the assumption is, that these are exactly the same equipment, or very similar equipment, similar branches, as used during the Grenfell Tower fire. I would have liked to see the serial numbers of the equipment used on the Grenfell Tower fire and the serial numbers and exact models of the equipment, of branches and nozzles, used into these particular tests.
Q. Thank you.

Now, can we go to page 16 \{LFB00123672/16\}, which sets out the results of the tests under the heading "Conclusion", roughly a third of the way down that page. It sets out the maximum jet height that was achieved for each piece of equipment tested, which for the aerial appliances were 49,60 and 62.3 metres respectively.

The report then concludes in the paragraph below in the following terms:
"For all of the flow tests undertaken within optimised practical working conditions, the maximum throw of water achieved, using equipment available at the time of the Grenfell Tower incident, it was not possible to exceed 62.3 meters[sic] in vertical water throw."

Now, put differently, the LFB concludes that the LFB aerial appliances' theoretical maximum vertical reach figures were not achievable in practice, and that those aerial appliances were not capable of reaching the top of the tower.

Now, before we turn to your response, was that your understanding of the LFB conclusions in this report?
A. That's very much my understanding of what LFB concluded, yes.
Q. Now, you address the LFB's testing in page 21 of your supplementary report, which we can find at
\{ISTRPS00000001/21\}. We can see at paragraph 47, which is in the bottom third of that page, you conclude thus:
"Save for Performance test 3b [which we don't need to go into for present purposes], I do not agree that the LFB test results above are representative of the maximum achievable vertical reach of a projected water

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jet for the equipment tested. In relation to
Performance tests 1, 2 and 3a, the LFB did not supply the tested monitors/nozzles with their rated inlet pressure and/or flow rate. Consequently, the vertical reach of projected water jets observed by LFB in those performance tests is lower than the maximum achievable vertical reach of the tested monitors/nozzles."

Now, you say at the beginning of that paragraph,
"Save for Performance ... 3b". Just so people know, that was one of the LFB's tests of the ground monitor; is that right?
A. That's right, and just to note, the ground monitor here has achieved 41.2 metres vertical reach, which actually exceeds my conservative estimates of about 35 metres.
Q. You have excluded performance test 3b from your conclusion because that is the only test which you say did actually supply the correct pressure and flow rate.
A. Correct.
Q. Yes.

Now, if we can put that ground monitor test to one side, is it right that you do not accept the LFB's conclusions in relation to the aerial appliances because the appliances -- and I put this in lay terms -- weren't supplied with the correct water pressure and flow rate that would have allowed them to achieve their maximum

## jet height?

A. That's correct, and this to me was very surprising, given the fact that LFB had my recommendations in place.
Q. Now, could we stay in this report but go to page 22 \{ISTRPS00000001/22\}. We can see -- and we don't need to go through it in detail now -- at pages from 22 through to 25 , you set out your detailed analysis about why the correct pressure and flow wasn't provided to the aerial appliances.

Can you help the panel, in brief, what is your essential conclusion on that point, why the correct pressure and flow wasn't provided to the ALPs?
A. Well, as you said, the most critical variables here is the nozzle inlet pressure and the flow rate which these monitors and nozzles needs to be provided, and this nozzle inlet pressure will depend on the pump discharge pressure and also the pressure head losses across the connections, the hoses, the different connections for these hoses. So, consequently, if one does not have the right set of hoses which we would expect LFB to take these into a place, there's no way they can provide the actual nozzle inlet pressure required to perform these tests which achieves that rated nozzle inlet pressure.

The other thing, my view is that we do a lot of experimental research, and experimental research is

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extremely critical to be able to go in a systematic way to validate your measurement equipment, make sure that specific measurement is put in place, and, to my view, LFB did not follow even basic standards in performing experimental tests. For example, one very simple approach would have been, as I highlighted in my response, to just measure the nozzle inlet pressure at that particular point, and that would have given us a lot of confidence in the repeatability and analysis of these tests, and that was not done.
SIR MARTIN MOORE-BICK: So, to put it simply, is it your view that, to put this rather crudely, I suppose, LFB used the wrong nozzles?
A. No, that's not the case. They used the right nozzles, because the nozzle is the actual part of the monitor, but what they did is they didn't supply the nozzle inlet pressure which I specified in my recommendation, which is part of this rated nozzle inlet pressure. So, in other words, the pressure at the inlet to that nozzle was significantly lower, and I've kind of justified that, than that they should have provided for the purpose of these tests.
SIR MARTIN MOORE-BICK: So they used the right nozzle but without the maximum input pressure?
A. Correct, to that nozzle.

## SIR MARTIN MOORE-BICK: I see.

A. So, to me, I wasn't --I can't say whether this is -it 's really puzzling, from my perspective, whether that was lack of basic knowledge in pipe hydraulics or there were other factors in place.
SIR MARTIN MOORE-BICK: Thank you.
MR KINNIER: For that reason, the contents of the LFB's testing does not cause you to doubt or qualify or amend the conclusions you reached?
A. Not at all. Even if I look at the ground monitor, if you go back to the LFB results and if you look specifically at the ground monitor, the ground monitor with the Mercury nozzle, even though it doesn't get the nozzle inlet pressure, has a much higher performance than the actual performance test 1 a which is coming from the LFB, and broadly they have very similar nozzles, and that sort of very clearly indicates to me - again, reaffirms my hypothesis that simply they didn't provide the correct nozzle inlet pressure.
Q. Just to give people a bite-size summary --
A. Okay.
Q. - - you don't agree because the LFB testing failed to account for various pressure losses due to friction and gravity which occurred between the pump and the appliance where the LFB monitored the pressure and flow

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rate and the nozzle of the aerial appliance being tested?
A. Correct, and to me that has a big impact on any policies LFB can derive from these tests.
Q. Secondly, the LFB didn't use state-of-the-art equipment to monitor pressure or flow and instead relied on physically looking at mechanical gauges and manual recording.
A. Correct.
Q. Thirdly, the testing was carried out using a single fire hydrant as a water source with a flow rate of 2,000 litres per minute, which was less than the required flow rate of 2,400 litres per minute; is that right?
A. Correct.
Q. I don't want to take this too crudely or simplistically , but those are the three principal reasons why you are not persuaded by the results the LFB gathered as a result of their testing.
A. That's right.
Q. Can we look at matters slightly differently, from a different perspective now, and look at the issues that arise out of your own estimates of the jets' vertical reach. I'd like really to discuss and identify the limitations of your own estimates.

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A. Sure.
Q. First of all, your estimates are just that: they're
    estimates based on desktop calculations which have not
    been replicated in the practical, real-life situations;
    is that a fair point to make?
A. It is a fair point.
Q. Secondly, there could be other factors which are not
    included in your calculations and which may lie outside
    your expertise, but which may affect an aerial
    appliance's achievable vertical reach; again, is that
    a fair, generic observation?
A. I would like to know how you describe these other
    factors, so --
Q. Shall we go through --
A. - - for me to be able to agree.
Q. Well, let's go through them, because some of the ones
    you identified earlier in your evidence.
            First of all, weather conditions.
A. Correct. But, again, as stated, I cross-referenced the
    weather conditions from the Meteorological Office
    stations, and, equally, that was done by other experts,
    such as Professor Luke Bisby, and the impact on the
    weather conditions and wind on, let's say, the
    fire spread, and their conclusion is that that was
    minimal, and equally the same conclusion I can draw for
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        the projection of the water jet.
Q. Dr Stoianov, could I ask you to take matters more
    slowly.
A. Okay.
Q. The stenographer is finding it difficult just to keep
    up.
A. Thank you.
Q. Another factor which may need to be put into the balance
    here is the performance of the appliance itself, which
    may have declined to some extent since factory
    conditions due to continuing use. Is that a legitimate
    point to bear in mind as well?
A. So we have several factors here, clearly. We have the
    pump discharge pressure, and I specifically asked for
    all maintenance records for the centrifugal pumps to be
    made available to me, and these maintenance records
    indicate that the performance of these pumps were well
    within the expected specifications of these pumps. So
    any other equipment that might deteriorate somehow is
    the actual nozzle geometry or some of the components of
    the nozzle. But, again, I would find that difficult to
    believe. So my assumption is that, actually, this
    equipment should have performed to its operational
    specification.
Q. Perhaps, as your answer indicates, performance of the
A. Sure
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There may also be operational firefighting reasons which factor into decisions about the use, placement or projection angle of an aerial appliance at a firefighting incident; to give a practical example, burning debris falling off a building and having to avoid that.
A. Correct, I fully agree, but equally we see the example of Alpha 245, which clearly was at a distance to the building.
Q. We don't necessarily have to go to it, but the LFB report noted that water at the highest peak of the maximum jet height fell very sharply downwards and created a significantly wider, more dispersed cone of water with reduced energy. That, in the report author's professional judgement as a firefighter, would have significantly reduced the effect on firefighting operations due to the dispersed nature of water at that height. That is a legitimate consideration to bear in mind; would you accept that proposition?
A. Yes, I would. However, again, probably that will go

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beyond the scope of my investigation, but it seems that we do have evidence to suggest that even small amounts of water can very effectively deal with the heat flux on these specific ACM panels.
MR KINNIER: Sir, that is the end of my questions on the first consequence of low flow rate, which is probably a reasonable place to stop for the moment.
SIR MARTIN MOORE-BICK: I think it is, yes.
Well, Dr Stoianov, we have a break during the morning in any event, and this is a good time to take it. So we'll stop there. We'll resume, please, at 11.35 , and I have to ask you, while you're out of the room, not to discuss your evidence or anything relating to it with anyone else. All right?
THE WITNESS: Thank you.
SIR MARTIN MOORE-BICK: Thank you very much. Would you go
with the usher, please.
THE WITNESS: Thank you.
(Pause)
SIR MARTIN MOORE-BICK: Thank you very much. 11.35, please.
MR KINNIER: Thank you, sir.
(11.20 am)
(A short break)
(11.35 am)

SIR MARTIN MOORE-BICK: All right. Ready to carry on?

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THE WITNESS: I am, thank you.
SIR MARTIN MOORE-BICK: Good, thank you very much.
        Yes, Mr Kinnier.
A. Mr Kinnier, before we continue, may I just revisit your
    question before the break with regards to the
    uncertainties associated?
MR KINNIER: Yes.
A. I would just -- again, on reflection, I mean,
    absolutely, I think all these uncertainties you have
    identified, rightfully they should be raised. But this
    is, again, the reason why this experimental validation
    is supposed to address these uncertainties and bring
    better clarification. In the examples which, let's say,
    Thames Water -- we ran these experiments jointly, we had
    an agreed protocol of how to run the experiments on
    collecting hydraulic data from the network, on the basis
    of which we can have the discussion. Unfortunately,
    with LFB, we did not have that interactions in terms of
    running the test and agreeing on processes, procedures
    and measurements, so at the end of the day it's very
    difficult for me to use these validation results to
    really address some of the uncertainties you mentioned.
Q. Please don't worry, Dr Stoianov, you have made your
    point very clear and you have re-emphasised it now.
A. Thank you.
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Q. Could I now turn to the second consequence of the low flow rates you identified in your report, and that was, in broad terms, interruption to jets.

If we can go to $\{$ ISTRP00000006/236\}, this sets out some of your conclusions from chapter 5 of your report. If we could look at the end of line 10 in paragraph 2 , you say this:
"The insufficient flow rates into the on-board tanks of pump appliances also resulted in frequently stopping the operation of the on-board centrifugal pumps to allow the tanks of the supplying pump appliances to be refilled. Managing the water deficit between the inlet flow rate into an on-board water tank of a pump appliance and the outlet flow for a projected water jet resulted in continuous variations in the jets' flow and reach."

Now, earlier we discussed the concept of continuity of flow, and that is what was essentially lacking here, in broad terms. Is that the point in a nutshell?
A. Yes.
Q. Less water was going into some pump appliance tanks than was being pumped out of them to firefighting equipment, so the tanks would repeatedly empty, the jets had to be stopped to allow refilling, and then start up again, and that's the essence of the problem.
A. Correct, and I believe we have very good cross-reference of this by firefighters on the night in their witness statements.
Q. Now, in some cases, jets could be deployed for less than a minute before the pump tank ran out, requiring the jet to be paused for 20 seconds or so before the tank refilled and the jet could be restarted; is that right?
A. Correct.
Q. One partial solution which firefighters were able to improvise to prevent these interruptions was to turn down the pump settings so that less water was pumped out to the firefighting equipment to match the limited flow of water coming into the tank. It's right that that's what was attempted on the night, wasn't it?
A. That's right, and we can look very closely at the pump characteristics to see that behaviour, and the moment you start reducing the flow rate, you're reducing the pump discharge pressure, and that has an impact on the nozzle inlet pressure.
Q. That's the big downside to that particular approach, isn' $t$ it, because in order to ensure continuous or near continuous supply of water, you would have a much weaker, diminished jet of water?
A. Correct, and this is very much -- these are variable speed pumps, the pump appliances have very powerful

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variable speed pumps, and the relationship between pump
discharge pressure and flow rate is very well represented there.
Q. Can we now turn to the third consequence of low flow rate that you identified, which was, in essence, that some equipment could not be deployed.

Now, as you identified in earlier evidence, and I said we'd come on to, there were problems with Alpha 245, an aerial appliance, in that the water flow rate it received was insufficient effectively to project a jet of water from its higher capacity nozzle. In a nutshell, is that right?

## A. Correct.

Q. Again, to use a horticultural analogy, it's a bit like a large garden hose receiving only a small stream of water, such that the water dribbles out and isn't projected any distance from the hose.
A. I agree, although I would like to use a more scientific explanation, but yes.
Q. In essence, that's the problem?
A. That's right.
Q. Firefighters again had to improvise, which they did by strapping a lower capacity fire hose to the cage of the aerial appliance to produce a jet which could reach the tower; is that a fair summary of what was attempted on

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    the night?
A. That's right.
Q. Again, apologies for using the garden hose analogy, but
    that's equivalent to pinching the opening of the hose
    with your thumb to produce the longer but necessarily
narrower stream of water?
A. Correct.
Q. Having identified those consequences, can we now turn to
    the topic of the causes. For that purpose, can we stay
    in chapter 5 but go to page 238 {ISTRP00000006/238}, and
    in particular could we look at paragraph 6. Here you
    provide a neat summary of the causes for us, and you
    said this:
    "The reasons for the low flow rate extracted from
    the hydrants at Grenfell Tower include:
        "a. The low flow (discharge) coefficient of the used
        hydrants (see Chapter 6).
            "b. In the case of A245 ALP and S13A1 ALP, the use
        of a wash-out hydrant (H5), which was wrongly labelled
        fire hydrant. A wash-out hydrant is not designed for
        the supply of water for firefighting ...
            "c. Lack of coordination between LFB and TWUL. This
        also included the continued pressure reduction in the
        water distribution system by TWUL ...
"d. Pressure losses between the hydrants and pump
A. That's right
that's equivalent to pinching the opening of the hose
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    appliances."
        Now, what I'd like to do, Dr Stoianov, is go through
        each of those causes with you.
            First of all, can we deal with the hydrants' low
        flow coefficients, which will necessarily bring in
        a question of interpretation of the relevant
        British Standard.
            Now, if we can go to \(\{\) ISTRP00000008/72 \(\}\). Now, at
        lines 19 to 20 at page 72 , you explain that:
            "... the flow coefficient of a hydrant is a measure
        of the flow rate that a hydrant can provide in relation
        to the pressure at that point in a distribution
        network."
            Now, in layman's terms, is the flow coefficient
        essentially a measure of how efficient the hydrant is,
        in that it measures how good a flow rate the hydrant can
        supply, given the pressure of the water the hydrant
        receives from the network?
    A. Correct.
Q. So the higher the flow coefficient of a hydrant, the
better?
A. Absolutely. I mean, if you scroll up that page, we
can - - it's no more than GCSE maths here, but if you
scroll up that page, you would very much see the flow
discharge equation from an orifice, and clearly if that
coefficient is higher -- so this is the equation 6.2 , for example. This is the actual calculation of the flow coefficient, but equally --
Q. Dr Stoianov, I don't think we need to go into --
A. Okay.
Q. Possibly to save my blushes about GCSE maths, but just for --
A. Okay.

SIR MARTIN MOORE-BICK: Likewise.
MR KINNIER: - - conveying the essential of the consequence we need here.
A. That's fine.
Q. I think we agree --
A. I shall follow your advice.
Q. Your report sometimes refers to the flow discharge coefficient of hydrants. Is that because the terms "flow coefficient" and "discharge coefficient" are both used and are interchangeable, at least in this context?
A. That's right.
Q. Now, your report distinguishes between the flow coefficient of a standalone hydrant -- and I'd like to emphasise that word "standalone" - - and the composite flow coefficient of a hydrant. In lay terms, can you explain for us the difference between the two?
A. So the difference between the two is that one is -- if

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one looks at the flow coefficient of discharge of a hydrant, one could imagine that this just correlates to the hydrant in isolation. So, in other words, I can take a hydrant, put it on a pipe rig at Imperial, and I can test this hydrant and look at specific flow coefficient or discharge characteristics of that fire hydrant. Now, if I take this fire hydrant and install it in an operational network, the connecting pipeline or the connecting piping around that hydrant might significantly differ than these kind of ideal piping arrangements under which l've tested that particular fire hydrant.

That becomes very important in urban environments where, you know, when you dig a street to install a fire hydrant, there is a whole set of different infrastructure, and in order to avoid that infrastructure -- and I have shown pictures of actually excavation of hydrants in London -- you might have a number of elbows, different connecting pipe and et cetera, so suddenly that hydrant which performed extremely well in my lab, when I actually put it in real operational conditions, because of the connecting pipework, might have very different performance characteristics as a whole, and ultimately that impacts the outcome of how much flow I can discharge. is in the title: the flow coefficient of only the hydrant tested in factory settings without the connecting pipework?
A. So in general, yes, but again, as we saw in my response, even the testing of these hydrants under any forms of standard includes a small section of connecting pipework, and they are explicitly taken into account. So we're not just testing the hydrant as a hydrant; the test, even according to British Standards, they include certain connecting pipework, and that's very explicitly described.
Q. Can we say that a hydrant's composite coefficient is likely to be lower than its standalone coefficient due to inevitable pressure losses introduced by pipes and bends connecting the hydrant to the rest of the network?
A. Correct, it would be equal or less than.
Q. Now, you touched in your answer and I touched in the

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introduction to British Standard 750:2012, which is entitled "Specification for underground fire hydrants and surface box frames and covers". We find that standard at $\{\mathrm{BSI} 00001767\}$.

Can we go to paragraph 10.2 , which is on page 13 $\{$ BSI00001767/13\}. We will see here, under the subheading "Hydraulic characteristics", paragraph 10.2 stipulates that:
"When fitted with a standard round thread outlet ... the fire hydrant shall have a Kv value of not less than 92."

Now, the reference to Kv value here is shorthand for flow coefficient; is that right?
A. Correct.
Q. Now, you say in chapter 4 of your report -- and it might be useful to go to it. \{ISTRP00000005/19\}. Thank you. If we could look at line 9 , bearing in mind that $\mathrm{K} v$ value, you said this:
"It is not entirely clear whether the 92 [units] ... flow coefficient requirement in BS:750:2012 refers to the hydrant as a standalone valve or when installed in a water distribution network."

In other words, it is not entirely clear whether the 92 requirement relates to the standalone flow coefficient or the composite flow coefficient of
A. That's true, because if we don't have that understanding of the composite values, and that needs to be interpreted by a professional who understands these pitfalls and the ambiguity of the standard, then we have
a hydrant. Is that the essential query you're raising here?
A. Correct.
Q. You go on to say that your view is that it refers to the composite flow coefficient; is that right?
A. That's right.
Q. Now, if we can just look at the British Standard, because it's a topic which you considered in your supplemental report.

Can we go to that report, $\{$ ISTRPS00000001/6\}. If we look at paragraph 17, you set out here your belief that the 92 requirement in the standard refers to the installed hydrant with connecting pipework, in other words to the composite flow coefficient, for four reasons, and you go through these reasons at length over the next 15 pages. I don't want to go through those points in detail, but could I summarise them and see whether you agree that I've summarised them correctly.

The four reasons you rely upon for your interpretation of the standard are these:

First, it follows an integral principle in systems engineering, ie that, in engineering, you're less concerned with individual performance of an isolated part of a system, and you are more concerned with the performance of the system as a whole; is that a fair

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summary of that reason?
A. Yes, it is .
Q. Secondly, you refer to BS EN 60534-2-1, which is a related standard which describes that the process of testing and certifying the flow coefficient, that's the Kv value, of a valve -- a hydrant's a valve -- includes the connected pipework; is that the second reason you rely upon for your interpretation?
A. Correct.
Q. Thirdly, you note that evidence from relevant stakeholders suggests a common understanding that the Kv requirement of 92 refers to an installed hydrant and connecting pipework; again, is that a fair summary of the third reason you rely upon?
A. That's right, because a lot of the stakeholders, they refer to a particular pressure and particular flow rate for a hydrant on the basis of which we can then refer back to that value of 92 .
Q. Finally, you refer to the absence of a meaningful standard if an alternative view is taken. Again, have I summarised at least the essence of that correctly?
no alternative. I can connect that hydrant with a garden hose, using your example, and I would still pass all the British Standards.
Q. Now, can I examine your reasoning in more detail of that latter, fourth point, and it's something you set out in detail at page 15 of your supplemental report \{ISTRPS00000001/15\}, if we could go to that. In essence, what you say is that if the 92 requirement refers to a standalone hydrant in factory conditions, there would be no standard or requirement governing the performance of an installed hydrant, and hydrants could therefore be installed very poorly without breaching any relevant standards. I put that crudely, but is that the essence of what you're saying?
A. Yes, it is .
Q. Now, your supplemental report acknowledges factors which may be read as pointing in the opposite direction and for an alternative interpretation of the standard. To this end, can we turn over the page to page 16 \{ISTRPS00000001/16\} and look at paragraphs 38 and 39.

Dr Stoianov, it's probably easier if I read these out. Paragraph 38 reads thus:
"38. I have described above my reasons for adopting what, in my judgement, appears to be the most appropriate interpretation of the requirement, that it
relates to an installed hydrant with connecting pipework in a water distribution network. I have also explained that the alternative 'standalone' (manufacturing only) interpretation would lead to a surprising absence of legal requirements relating to the installation and real - world efficiency of hydrants.
"39. However, given the ambiguity in the wording of BS 750 , I cannot go so far as to say that the standalone interpretation is a wholly unreasonable interpretation of BS 750. Elements of the wording of BS 750 may be taken to lend some support to that interpretation. The scope section of BS 750 states that: 'This British Standard applies to underground fire hydrants to be installed in a water supply system ...' ... Following the description of the $K v$ requirement of 92 , BS 750 adds: 'The Kv value of the fire hydrant shall be specified in the manufacturer's literature' and there are a number of other references to the manufacturer. These references may be taken to mean that the standard applies to standalone hydrants in manufacturing or factory conditions."

Now, bearing in mind what you say there, would you also agree that the absence of a minimum standard relating to a hydrant's flow coefficient, which would exist if the standalone interpretation of $B S 750$ is
adopted, while perhaps unsatisfactory, does not mean that we should read British Standard 750 in such a way to bridge that gap?
A. I agree. It's ... yes. If I look at it, scrutinise from a very, as you said, legal perspective, yes, the description is very ambiguous. If I look at it from the perspective of a hydraulic engineer, I would have sufficient knowledge to recognise that ambiguity and take it into account.
Q. Looking at what you say in paragraph 39, and where you say that the standalone interpretation is not a wholly unreasonable interpretation of that standard, could we look at it slightly differently, ignore the double negative, and accept that the standalone interpretation is a reasonable one, albeit one with which you don't agree?
A. Well, as I said, if I am not technically competent, I would find this as a reasonable explanation.
Q. Thank you.

Can we now look at a separate topic, which is the flow coefficients of the hydrants at Grenfell Tower.

As part of your investigation into the water supply to the tower, you carried out testing in July and September 2018 which enabled you to calculate the composite flow coefficients of some of the hydrants at

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the tower, including those that were used to supply
firefighting efforts on the night. Is that correct?
A. Correct.
Q. We can see the detailed results of those calculations at \{ISTRP00000008/100\}. If that table could be slightly expanded.

Hydrant H 1 had a flow coefficient of 74 ; is that right?
A. Correct.
Q. H3 had a flow coefficient of 50 ; is that right?
A. Correct.
Q. Wash-out hydrant H 5 had a flow coefficient of 31 ; is that right?
A. Correct.
Q. And hydrant H 8 had a flow coefficient of 50 ; is that correct?
A. Correct.
Q. Now, if your preferred interpretation of BS 750 is adopted, those hydrants should have a composite flow coefficient of no less than 92, so that each of the four on these figures fell well short of that standard; would that be right?
A. That's right.
Q. However, if the alternative interpretation is adopted, that the 92 requirement refers only to the standalone
hydrant, is it right to say that you wouldn't be able to conclude from your testing that the hydrants fell short of that standard because you were only able to test their composite flow coefficient?
A. That's right, but the ultimate goal here is to deliver water for firefighting, so, you know, having a coefficient of a hydrant which delivers no water is of no use to anyone.
Q. Can we go back to your supplemental report, \{ISTRPS00000001/16\}, and we can see at paragraph 40, which is at the very foot of that page, you say this, and it just flows from the point that you have made:
"Even if the alternative view were adopted, that the Kv [flow coefficient ] standard of 92 in BS 750 relates to a standalone hydrant, one would expect the installation of hydrants to be carried out in such a way that the Kv [the flow coefficient] of the hydrant installed in the water distribution network remains as close as possible to (or exceeds) 92, by minimising any possible performance loss from the installation setup and connected pipework."

Mindful of what you have said there, regardless of which interpretation of the British Standard is preferred, would you have expected the flow coefficients of the hydrants installed at Grenfell to be higher than
they turned out to be on the basis of the figures you've identified?
A. This is correct, because, again, that has an implication on the flow rate which can be delivered to the London Fire Brigade to perform their duties.
SIR MARTIN MOORE-BICK: I think what we would find it helpful to know, and I think this is the thrust of Mr Kinnier's question, is: if we look at the figures we've got in the table we had up a little earlier, are they, in your experience, typical?
A. Well, so let me take a step back. The only way we can identify whether it's typical or not is by doing flow tests of hydrants, and flow tests of hydrants are not carried out by the water utilities or by the London Fire Brigade.

I would like to refer to a paper which was published a year before the Grenfell Tower fire which was by a firefighter in southwest London. He did carry out something along the lines of 600 flow tests to fire hydrants in southwest London, and his conclusion was that about $20 \%$ of these tests almost were inoperable, and a very large percentage, almost like over $30 \%$, I believe, based on memory, had flow rates less than 500 litres per minute.

So, in answer to your question, it seems to be --
A. Correct, and that's one of my points I made in chapter 4. In a lot of countries around the world, fire rescue services have this periodic flow test, full flow rescue services have this periodic flow test, full
test of hydrants, because it's not just about the installation conditions, but over a period of time, these things can deteriorate, and that's why this
you know, my sample is not representative out of these
five hydrants to draw an exact conclusion, although all these results show much lower values. But if I extrapolate this to the kind of publications of an active firefighter who has gone and done that test, it seems that this is a very representative sample of what's happening in London, that most of these fire hydrants do not have the discharge characteristics which we expect them to have.
SIR MARTIN MOORE-BICK: Is it possible to say whether the discrepancies between the standalone coefficients and the composite coefficients are likely to be due to the state of the pipework?
A. It's the installation conditions of this, and because we do not - - you know, there is no obligation to flow test these fire hydrants once these are commissioned, we have no information. And the regular testing of these fire hydrants of London Fire Brigade does not include flow testing of these fire hydrants. It's a lottery. We don't know what their discharge coefficients and characteristics would be until LFB have to deliver the required flow rates.
SIR MARTIN MOORE-BICK: One of the things that seems to me
to come out of this, possibly, relates to the
construction of the British Standard that you were

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referring to a moment ago, because unless there are factors at work which we're not aware of, if you look at these figures, it suggests that there can be a difference of almost $50 \%$ between the rated flow rate, so to speak --
A. Correct.

SIR MARTIN MOORE-BICK: -- and the actual flow rate.
A. Correct.

SIR MARTIN MOORE-BICK: Now, I don't know how you can accommodate that within a standard-setting document, because if the operational conditions can have that degree of influence over performance, then how are you going to know whether you've got hydrants which have a coefficient of 92 ? You won't, will you?
A. That was my point, you wouldn't. Unless you test them, you wouldn't know.
SIR MARTIN MOORE-BICK: But you've got to test all of them in operation because they've got to have the connected pipework.

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    periodic flow test of hydrants becomes extremely
    important. And as I pointed out in my results, if
    I know the flow discharge characteristics of
    fire hydrants - - for example, I point out that in France
    they do them every five or three years, depends on
    certain conditions -- and I know the hydraulic
    conditions of this system, I can be very definite in the
    kind of flow rates the water utility can provide to the
    fire rescue service.
SIR MARTIN MOORE-BICK: But this might in turn have
    an implication for how one reads the British Standard --
A. Huge, yes.
SIR MARTIN MOORE-BICK: -- because, well, it may be more
    doubtful that the British Standards Institution is
    setting out to prescribe minimum requirements which
    themselves are dependent on operating conditions. Do
    you see what I mean?
A. This is where, in my response, I tried to track back to
    kind of where these values are coming from, and if you
    start seeing these kind of variations of British
    Standards, I think the overall meaning was lost. So
    clearly we need to define that that component has
    certain specifications, but that we also need to
    recognise that that component, as part of the whole
    system, needs to preserve these specifications, because
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ultimately a firefighter expects, let's say,
2,000 litres per minute to come out of a fire hydrant in
London, and that's the ultimate goal we need to deliver.
SIR MARTIN MOORE-BICK: Of course, the British Standard
refers to the flow rate being stated by the
manufacturer. Now, the manufacturer cannot possibly
state a flow rate which is dependent on operational circumstances, can he?
A. No, he can't, but that's why I was going back to the notion of performance of components.
SIR MARTIN MOORE-BICK: Yes.
A. So that's a very much component performance. But then the person who puts that component into the system needs to be qualified and technically knowledgeable to recognise the pitfalls what might happen with that particular component, and that's why ultimately we also need to have this flow test. So once that hydrant is installed and commissioned, we need to understand what actually happened out there, because there's all sorts of other human factors. I mean, a lot of these installations are done by subcontractors, probably with a very low level of supervision, and I've seen many examples of horrendous installations in that respect.
SIR MARTIN MOORE-BICK: Well, that's helpful, thank you very much.

I'm sorry, I have been responsible for a bit of a digression there.
MR KINNIER: No, it's useful. Thank you, sir.
Can I now turn to another reason for the low flow rate, which was the use of a wash-out hydrant. It's a topic we've touched upon earlier, but I'd like now to turn to it in more detail.

To this end, can we go to \{ISTRP00000006/238\}, and paragraph 6. This is what we looked at slightly earlier, but just to sort of reorientate yourself in your report. The second reason you identified for low flow rates was:
"In the case of A245 ALP and S13A1 ALP, the use of a wash-out hydrant (H5), which was wrongly labelled fire hydrant. A wash-out hydrant is not designed for the supply of water for firefighting ..."

If we can go to chapter 6 of your report, which we find at $\{$ ISTRP00000008/79\}, we find, at the beginning of line 10 , a sort of more detailed explanation of a wash-out hydrant and its differences from a fire hydrant, and you say this:
"H5 is a wash-out hydrant, which is different from a fire hydrant. As explained in Chapter 4, wash-out hydrants are used for operational and maintenance purposes, and enable water companies to flush sediments

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and stagnant water from specific locations. The
flushing is generally done at flow rates significantly lower than the flow rates expected from fire hydrants for firefighting. Wash-out hydrants are not aimed and installed to supply water for firefighting. Wash-out hydrants look identical to fire hydrants and should be clearly marked (e.g. with a 'W') to distinguish them."

Now, although they have a different purpose to fire hydrants, a wash-out hydrant may be structurally the same as a fire hydrant and connected to the water network in exactly the same way as a fire hydrant; is that right?
A. Correct.
Q. If we go to the table at page 100 of chapter 6 , which we find at $\{$ ISTRP00000008/100\}, we see, if we look for H 5 , which is at column 5 , that it has the lowest composite flow coefficient of all the hydrants you tested. That's presumably something you would have expected due to its different function and design?
A. Correct, and I've demonstrated a photograph which shows the installation of hydrants and wash-out hydrants, and we can visually observe the different pipework associated with that.
Q. Are you looking for the photograph?
A. Yes, I don't have the document in front of me, so my

| memory (inaudible) -- | 1 |
| :--- | ---: |
| Q. I don't have the reference. I can turn expectantly to | 2 |
| someone behind me. I don't have that reference | 3 |
| immediately to mind. | 4 |
| A. Okay. | 5 |
| Q. If we could maybe just move on with some text before we | 6 |
| find that photograph. | 7 |
| If we can go back to page 79 of chapter 6, which is | 8 |
| at \{ISTRP00000008/79\}, and if we can see in the next | 9 |
| paragraph, from line 16 onwards, you say this: | 10 |
| "Wash-out H5 is owned by [Thames Water] and it was | 11 |
| installed in February 2014. As I detail in Chapter 5, | 12 |
| wash-out hydrant H5 was mistakenly labelled 'FH' (fire | 13 |
| hydrant) on the metal lid of the hydrant chamber ... | 14 |
| Firefighters would not have known that they were | 15 |
| connecting a pump appliance to a wash-out hydrant on | 16 |
| 14 June 2017. However, the digital maps of the TWUL's | 17 |
| Network Service Technicians had the information that | 18 |
| wash-out hydrant H5 is a wash-out hydrant ..." | 19 |
| Now, having been mislabelled "FH", and as wash-out | 20 |
| hydrants and fire hydrants otherwise look identical, was | 21 |
| there any way for firefighters to identify that H5 was | 22 |
| a wash-out, not a fire hydrant? | 23 |
| A. Not really. I mean, there was a number of factors which | 24 |
| were identified through the witness statements. First | 25 |

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of all, the mobile data terminal of the pump appliance in close proximity was not working. Secondly, we have witness statements which demonstrate that they tried to attach a standpipe to one of the nearby fire hydrants, which I have also identified was inoperable. And then probably in the night, my assumption is that they just stumbled across this additional hydrant which was labelled fire hydrant, so in the urgency of the situation, it would be extremely difficult, I would imagine, to extensively test that this was actually not a fire hydrant but a wash-out hydrant.
Q. Which wasn't practical.
A. Was not practical, that's right.
Q. Going back to your earlier request, if we can stay in this chapter and go forward to page 81 \{ISTRP00000008/81\}, this is a series of photographs of H5, the wash-out hydrant. Was this what you had in mind?
A. Correct. I mean, during my experimental tests, I noticed that -- we sort of went through all the kind of hydrants in the area, and I noticed that, clearly from the evidence, this was the hydrant used by London Fire Brigade on 14 June, and I noticed that that was labelled fire hydrant, while my records in the GIS provided by Thames Water, that was labelled as
a wash-out hydrant. And the other impact of that is that, clearly, LFB would not have been doing any tests on that fire hydrant, even the very basic mechanical tests they were doing.

That sort of brings me to the other hypothesis, that, as we know, London Fire Brigade had problems opening that fire hydrant -- that hydrant fully, and the network service technicians opened that hydrant fully at about 5.30, and even then the flow rate was very low.

So my interpretation of that is because of these mishaps of labelling that hydrant, it was not just the issue of the flow rate, but also there was the issue that there were certain mechanical potential issues with the stem of that particular hydrant.
Q. Thank you. Now --
A. Sorry, I apologise, just to add up. So I kind of notify -- because Thames Water was on site, they were overseeing my work and shadowing my work, I've notified them that this should be a wash-out hydrant, and it seems shortly afterwards that was replaced with a W plate.
Q. Thank you. We're going to come on later to the involvement of Thames Water.
A. Sure.
Q. But could I turn to a further reason for low flow rate,

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and that was pressure losses between the hydrants and the pump appliances.

If I can just start off with something basic so we know what we're talking about here, are you referring to pressure losses caused by friction in the hoses used to transport water from the hydrant to the pump appliance?
A. That's right.
Q. Now, is it right that some degree of pressure loss is inevitable, but that this can be exacerbated by longer hose distances and by bends and kinks in the hoses themselves?
A. Correct.
Q. To what extent did the long distance between some of the hydrants and the tower add to pressure loss on the night of the fire?
A. Well - -
Q. Are you able to answer that scientifically, if I can put it that way?
A. Okay. I mean, clearly, as you said, there is a length of hose which certainly impacts the pressure head losses into that system, and therefore it 's extremely important to set up, like, a tandem of pumping. In other words, you're boosting your pressure. You have one appliance very close to the source of water, to the hydrant, which then pumps to another appliance, and that was done on

## A. Correct.

Q. You also note in this paragraph that, at about 06.00 hours, the LFB was able to mitigate these losses by setting up a pump relay.
First of all, what is a pump relay?

First of all, what is a pump relay?
A. It's a way to boost the pressure within that sort of system of delivering the water for firefighting. So pump relay would be you have multiple pumps which might be, for example, in series or parallel, depending whether you want to boost your pressure or flow rate in that particular case. So if I want to boost my pressure that particular case. So if I want to boost my pressure
to negate the impact of these pressure head losses, you would be setting up this operation of pumps in series. So you have the first pump pumping, in that particular
the northwest side, but it wasn't done on the east side, on the hydrant H3, which was on Grenfell Road and Bomore Road, until very late into the incident, and that had a significant impact. I mean, the empirical evidence for us is that this probably, for that particular -- had an impact of probably another 200/300 litres per minute flow rate into the pump appliance.
Q. Now, we can see, just to give a bit of a practical example, if we turn to chapter 5 of your report, which we can find at $\{$ ISTRP00000006/21\}, at line 7 onwards a section describing the deployment of the ground monitor on Grenfell Walk.

If we turn over the page to page 22 \{ISTRP00000006/22\}, and beginning at line 17 , you say this, and what I think is a practical illustration of the point you've just made. But what your report says is this:
"As with A213 TL, this low flow rate was because of the flow discharge characteristics of the fire hydrant and the long length ( $\sim 115 \mathrm{~m}$ ) of fire hoses between fire hydrant H3 and Pump G272. The pressure losses in the long length of fire hoses between fire hydrant H3 and Pump G272 reduced the flow into the tank of Pump G272 by around $20 \%$ of the available flow rate from fire hydrant

H3. Consequently, the setup of a pump relay between fire hydrant H3 and Pump G272 at around 06:00 hrs increased the flow rate in the tank of Pump G272 from $\sim 1,200 \mathrm{I} / \mathrm{min}(20 \mathrm{l} / \mathrm{s})$ to approximately $1,500 \mathrm{I} / \mathrm{min}$ ( $25 \mathrm{l} / \mathrm{s}$ ); or $\sim 86 \%$ of the ground monitor's rated flow rate of $1,750 \mathrm{I} / \mathrm{min}(29 \mathrm{l} / \mathrm{s})$."

Now, there is a lot of technical detail in that quote, but is the key point that the long length of hose needed to connect the hydrant to the pump appliance over 100 metres away had the effect of reducing the flow rate by about $20 \%$ or so?
case, into the reservoir of the second pump, and that guarantees a higher flow rate into the second pump to then deliver the pump discharge pressure.
Q. So it's a boost between the hydrant and the primary pump appliance?
A. That's right.
Q. Now, the first three reasons you identified for the low flow rates relate to low flow rates extracted from hydrants, whereas this fourth one relates to losses in pressure between hydrants and pump appliances.
A. Correct.
Q. That's a fair summary, isn't it, I think?
A. Correct.
Q. Is it a fair summary of your analysis to say that while these losses between the hydrants and pump appliances were also a significant factor, the principal cause of the low flow rates was the low flow rates extracted from hydrants?
A. That's right.
Q. Thank you.

I'd now like to move away from some of these technical matters and to look at the role of Thames Water itself.

Now, chapter 7 of your report gives a detailed chronology of the actions taken by Thames Water and its

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employees throughout the incident, including communications and other interactions between Thames Water and the LFB.

Is that a fair summary of chapter 7 ?
A. Correct.
Q. That chapter was based on your review of evidence, including statements and documents provided to the Inquiry by Thames Water and the LFB, and transcripts of calls between Thames Water and LFB personnel; is that right?
A. Correct.
Q. Now, the LFB first made contact with Thames Water by telephone at 01.28 ; is that right?
A. That's right.
Q. We can see an extract of the transcript of that particular call at $\{$ ISTRP00000009/9\}. We can at lines 7 to 10 of the table in the top half of that page that the LFB made a request for a water technician to attend and for Thames Water remotely to increase the pressure; is that a fair summary?
A. That's right.
Q. If we stay in this chapter but turn to page 95 \{ISTRP00000009/95\}, we can see, at paragraph 25, that before 11.00 am , Thames Water deployed a total of six network service technicians, NSTs, to attend the

## A. That's right

Q. You refer to the first two as NST1L and NST2D, who arrived at 02.15 hours; NHS4N and NST3A, who arrived later at about 04.15; and, finally, NST5M and NST6R, who arrived at about 07.30 hours; is that right?
A. That's right.
Q. Now, can I next turn to control interventions effected by Thames Water.

If we can stay in this chapter but go to page 85 \{ISTRP00000009/85\} and, in particular, section 7.8 .1 of your report.

Now, you say in subparagraph 1 that Thames Water carried out two control interventions on the night.

First of all, so we understand basic terms, what is your understanding of a control intervention?
A. This is a very broad term, but in that particular case means the opening of a valve, and these are specifically manually operated gate valves.
Q. Now, you identify two control interventions: first of all, the opening of district boundary valve DBV214263, which connected pressure reduced area PBARHT08 with a neighbouring pressure reduced area, PBARHT07, through a 100 -millimetre pipe at about 03.09 hours.

The second intervention was:
"The opening of district boundary valve DBV214521, which provides an additional hydraulic connection within pressure reduced area PBARHT08 through a 100 mm pipe at 11:05 hrs ..."

Now, a district boundary valve is a valve which connects two different areas of the water network. Essentially is that correct?
A. This is correct, and I think it would be really helpful if we can bring some of the schematics I have in chapter 6 - -
Q. If we can take it --
A. -- to really visualise this.
Q. I think if we just take it stage by stage, Dr Stoianov, for these purposes.
A. Okay.
Q. Now, is the rationale for opening boundary valves between different areas to increase the pressure and/or reduce the energy losses in the target area by connecting it to another part of the water network which has its own inlet from water sources, thereby spreading pressure losses more broadly across a larger area?
A. That's the intuition, but this is just an intuition. In reality, that decision cannot be made just by eyeballing a valve and making that decision. That decision needs to be made based on a more rigorous hydraulic analysis
on the operation of the network.
Q. Now, it's really flowing from that point, if we can take things again stage by stage. Stay on this page, page 85, and look at line 22. You say this:
"The hydraulic analysis carried out in Chapter 6 indicates that the opening of the two district boundary valves by TWUL had minimal (no material) impact on increasing the pressure at wash-out hydrant location H 5 , and consequently, the opening of the two district boundary valves had minimal (no material) impact on increasing the flow rate from wash-out hydrant H 5 into the on-board tanks of the connected pump appliances; namely, Pump A241 and later in the incident, Pump S13P1. Both of these interventions by TWUL were made in response to requests by LFB for an increase in the flow rate from wash-out hydrant H 5 .
"The same conclusion can be extended to all four hydrants used by LFB to provide water for fighting the fire ; namely that the interventions by TWUL (e.g. the opening of the two boundary valves by TWUL) had minimal (no material) impact on increasing the flow rates from the four hydrants used by LFB into the on-board tanks of the connected pump appliances."

Now, in layman's terms, you conclude that
Thames Water's actions on 14 June resulted in no

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material improvement in the water supply provided to the LFB's firefighting equipment; as a lay summary, would you accept that?
A. I do.
Q. That is based on the analysis you carried out using the mathematical model of the water distribution network which we discussed earlier in your evidence.
A. That's right.
Q. Now, can we look at other actions taken by Thames Water and, in particular, the actions taken by the network service technicians. I'm going to call them NSTs.
A. That's right.
Q. If we can turn over the page to go to page 86 of your report $\{$ ISTRP00000009/86\}, and if we could look at paragraph 4, which is at the head of that page, there you describe two further actions taken by the NSTs during the incident:
"a. between approximately 06:00 hrs and 06:30 hrs, four NSTs ... assisted with cleaning drains which were causing flooding around Grenfell Tower and preventing LFB firefighters from gaining safe access to the building.
"b. at approximately 06:30, NST4N fully opened a hydrant in use by LFB (most likely wash-out hydrant H5) after noticing it had only been opened half a turn. This
action increased the flow rate from around $380 \mathrm{I} / \mathrm{min}$
(flow rate reported by WM Beale ...) to a flow rate of $450 \mathrm{I} / \mathrm{min}$ to $500 \mathrm{I} / \mathrm{min}$ (flow rate reported by SM Payton ...)"

Now, again, in lay terms, does that mean that the wash-out hydrant was like a half-open tap with a reduced amount of water coming out of it before the NST noticed it and fully opened it?
A. Correct, and I refer to my previous comment, it's because that hydrant was not inspected by LFB, it was not what we call exercised, et cetera, most likely the stem of that valve couldn't operate fully, might have jammed at that point, and that was noticed later by the network service technicians, who opened it a little bit more. Nevertheless, the total flow coefficient of this hydrant remains very low.
Q. Now, given your conclusion about the minimal impact of opening the boundary valves, is it right to say that this action by NST4N was likely the most effective intervention by Thames Water, in your view, during the incident in terms of increasing the flow rate?
A. I mean, this is where I really struggle to derive a conclusion without referring back to the hydraulic model. You know, these are actions taken by the network service technicians without understanding the hydraulics
of the system. That's not something we expect from them, to know in great detail. That's kind of the roles of the network management centre. And we've seen from these examples that they received no feedback and guidance from the network management centre to run these what-if scenarios and provide a competent engineering knowledge of these control actions. So at the end of the day, the control action was pure improvisation on behalf of this network service technician, to the best of his knowledge, but that improvisation had no impact and, secondly, he would have no knowledge to judge what impact that would have had.
Q. Can we leave that topic and come on to a separate one, which is the communications between LFB and Thames Water. It's linked to the points that you have made.

Now, I put this broadly, in chapter 7 you criticise the quality and substance of the communication between the LFB and Thames Water. The summary of your point can possibly be most usefully found at page 93 in this chapter $\{$ ISTRP00000009/93\}. If we look at paragraph 21 , you say this -- and forgive me for reading it out, but it 's possibly quite useful to, bearing in mind what you've said:
"Communication between LFB and the TWUL's NSTs
occurred on an ad-hoc basis and, consequently, the communication was qualitative, imprecise and lacked technical rigour. LFB Control/Incident Command did not articulate, quantify and communicate their water supply and flow rate needs to the TWUL's NMC."

So that's network management centre that you referred to earlier?
A. Correct.
Q. "Such quantitative requests could have included:
"a. A clear statement about the required flow rate for a particular appliance: e.g. the aerial appliance at the East side requires a flow rate of $2,400 \mathrm{I} / \mathrm{min}$ ( $40 \mathrm{I} / \mathrm{s}$ ), and how can this be achieved?"

Then if we can turn over the page
\{ISTRP00000009/94\}, looking at the first $b$ at the top of that page, you say LFB requests could also have included the following:
"Periodic updates by the LFB Control to TWUL's [network management centre] as the mobilisation of appliances with significant water flow requirements progressed. Such updates could have included the required water flow rate on the incident ground: e.g. 'LFB requires " X " I/min in this area, and this includes an aerial appliance on the East side of Grenfell Tower (2,400 I/min), a ground monitor on the South side

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( $\sim 1,900 \mathrm{I} / \mathrm{min}$ ), a water supply to the dry fire main ( $\sim 1,500$ to $2,000 \mathrm{I} / \mathrm{min}$ ) ... These are the approximate locations of the mobilised appliances and equipment; can this flow rate be achieved and how?'
"22. Furthermore, the TWUL's NSTs do not appear to have requested clear quantitative indications of LFB water supply and flow needs which, if not forthcoming from LFB, NSTs could have proactively requested themselves."

Now, having set that out, would you agree that your suggestions here amount to a counsel of perfection, and that you cannot safely comment on whether it was operationally feasible for the Brigade or indeed Thames Water to have detailed quantitative discussions given everything that was going on on the fire ground?
A. I disagree with that assessment. I mean, we know very well from, for example, Watch Manager Beale and a lot of the statements, first of all they had a very good understanding of the flow requirements for their appliances. They also knew exactly where they're connected, certainly they could describe that. So that information presents an opportunity to really kind of have the kind of dialogue I'm describing there.

On the other hand, it's very common --1 mean, I work with many water utilities in England. Their
A. I think they're absolutely essential if both of these
organisations needs to provide safe and secure supply of water for firefighting, yes.
Q. Now, can we turn to page 102 of this chapter \{ISTRP00000009/102\}, where you discuss alternative control options that were potentially available to Thames Water on 14 June, and you've set out four in particular at paragraph 45 . They include the following:
"a. Increasing the pressure in PBARHT08 by switching on the Hammersmith pumps and turning off the pressure reduction control for PBARHT08."

I will call that just "08", just for clarity :
"b. Increasing the pressure in [08] by turning off the pressure reduction control (e.g, by-passing the pressure reducing valves or fully opening these valves).
"c. Opening boxed/closed inlets such as DM18631.
"d. The utilisation of multiple hydrants to provide water for firefighting ."

Now, could we go through each of those four options
incident management procedures include the hydraulic
that purpose to be able to simulate particular demand conditions on the network and very quickly provide a guidance, and that guidance is also taken into account for fire incidents such as this one. In that particular case, I see no examples that any forms of hydraulic modelling has been carried out from these discussions, and any consideration of any data available to Thames Water through their telemetry system was taken into account. So I don't agree with that assessment.
Q. Pushing it slightly further, obviously you have made a number of observations on the effectiveness and efficiency of the communication and co-ordination between the Brigade and TWUL. Now, would you accept that those are largely matters of operational and organisational competence for those bodies which don't obviously fall within the scope of your own experience and expertise?
A. Yes, I broadly agree with that statement. However, we also cannot decouple kind of the hydraulics what we observe without taking into account some of these human factor interactions, and as someone who has worked both as an academic and researcher and practitioner into the water industry in the UK for over 20 years, I find this
highly inadequate, to have that level of discussion to define key requirements for making incident-based decisions.
Q. But the points you raise are points which you would actively encourage both the LFB and Thames Water to consider carefully? keep to one of these figures, because it can tell fully the picture what I'm trying to convey.
Q. Okay. We'll just go through and deal with the basics first.

If we look at paragraph 46 on this page, the normal cycle in June 2017, which was also followed on 14 June, was that these pumps operated during the day, but were automatically turned off at some point between 00.30 hours and 00.45 hours before being automatically turned on again at 05.30 hours; is that right?
A. Correct.
Q. Now, in layman's terms, can you help us, why would turning the Hammersmith pumps back on during that time have increased the water supply to the LFB?
A. Because, again, we are discussing here marginal gains, cumulative gains into the -- increasing the pressure into the network, and that, as we discussed, might have

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a small impact on the discharge of water from the fire hydrants. But, nevertheless, we need to put that into the context: if that discharge of additional 300 , 400, 500 litres per minute on a ground monitor allows us to reach another three floors, that has a significant impact on the night. That's the reason why I'm trying to raise this issue, is that the system continued to be pressure reduced throughout the incident and, in my view, there was absolutely no justification for that pressure reduction to continue during that particular incident.
Q. Bearing in mind your reference in answer there to marginal gains --
A. Yes.
Q. - - are you able to say how significant a difference turning on the Hammersmith pumps would have made to the flow rates delivered from the four hydrants to the firefighting equipment?
A. I would be able to, based on the figures which I present, demonstrate what the pressure at the inlet to these pressure-managed areas is and would be, certainly I can do that, and equally, by turning off the pressure reduction system in place, we can quantify how much extra pressure there will be at these particular hydrants. Then, with regards to the impact of pressure

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and discharge, I would be able to tell you how much
additional flow rate we can get from these hydrants by doing that particular control intervention.
Q. Bearing in mind your reference to marginal gains, can we look at matters adjectivally: is it fair to say that any increase would have been modest at best?
A. That's right. That's a fair assessment. It would be modest, but another 10 metres of pressure head would have increased, as I said, again, the flow rate with the current -- with the existing use of hydrants, but another $2,3 \ldots$ litres per minute, and again, if that means that marginal gain refers to another two/three floors of impeding the spread of fire, to me that was the price worth paying.
Q. Can we look at the second option you refer to in paragraph 45 on page 102 \{ISTRP00000009/102\}, and that was switching off the pressure reduction control which was in place at the time.

Now, if I can just deal with some basic propositions first, Dr Stoianov.

First of all, the tower was situated within a pressure-managed area; is that right?
A. That's right. They are normally --
Q. If we just take it in stages --
A. That's right.

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Q. Good.

Secondly, a pressure-managed area is an area of the
water network in which water companies reduce the water
pressure to reduce the risk of water leaks and pipe
bursts; is that right?
A. They don't reduce the risk, they reduce the leaks, because it's again orifice discharge.
Q. Thank you.

If we could go to $\{$ ISTRP00000008/231 $\}$, we can see at
the end of line 11 , going through to line 13 , you concluded that the pressure reduction scheme in operation during the Grenfell Tower fire resulted in a reduction of pressure of between 7 to 13 metres or, put differently, 0.7 to 1.3 bar throughout the incident; is that correct?
A. Correct.
Q. Is that the basis for your conclusion, which we touched on earlier, that one of the reasons for the low flow rate extracted from hydrants was "the continued pressure reduction in the water distribution system by [Thames Water]"?
A. Correct. But, again, this is the marginal gains that was relatively -- you know, even that sort of 1.3 bar has a small impact, but then if you take a small impact from the pressure reduction, a small impact increasing
the pumps and et cetera, that marginal gain suddenly becomes more tangible and more beneficial for the Fire Brigade, particularly in a situation where you're trying to really maximise both your equipment resources, outreach, et cetera.
Q. I think you have impliedly given the answer to this question, but I will ask it explicitly to get the benefit of your evidence: does it follow that turning off the pressure reduction control during the incident would have resulted in a corresponding increase of 7 to 13 metres or 0.7 to 1.3 bar in pressure?
A. That's my estimate, yes.
Q. Again, you have been very fair in saying we're looking here at marginal increases. Again, would that increase in pressure have been at the modest end of the spectrum?
A. That's right, but you have to take that into two particular directions: one of them is the use of the hydrants as used by London Fire Brigade, and the other one is it demonstrated if London Fire Brigade, with the guidance of Thames Water, was starting using multiple hydrants, that would have had a much bigger impact.
Q. In relation to each of these two options we have been discussing, turning on Hammersmith pumps and turning off the pressure reduction control, you observed in your report that Thames Water did not follow those options

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because of concerns that the resulting increase in pressure could lead to pipe bursts. We don't need to go to it, but it's at \{ISTRP00000009/101\}.

Now, if we can go and look at --
A. May I just say that there were two conflicting statements.
Q. If you can just wait for the question, rather than giving the answer to a question that hasn't yet been asked.

Can we go to $\{$ ISTRP00000009 $/ 106\}$, and if we could look at section 7.8 .7 which, as you will see, is under the emboldened headline, "The risk of pipe breaks from turning on the Hammersmith pumps and/or turning off the pressure reduction control".

You conclude, if we look at line 7:
"... there was a minimal risk of pipe breaks from turning the pumps on at Hammersmith Pumping Station and turning off the pressure reduction control in [08]."

So 08, that's the pressure-managed area in which
Grenfell Tower is found; is that right?
A. That's right.
Q. Sorry, that's a point I should have put to you earlier.

Just so we're absolutely clear about terms that have been used here, "pipe breaks" and "pipe bursts" are synonymous terms, aren't they? They're describing the
same thing.
A. Yes, they are.
Q. Now, your reasoning to support this conclusion is found in the next paragraph. Essentially, to summarise the position -- and please disagree if I've not done this fairly or completely -- (a) the pipes had been in place for a number of years before the pressure-reduction areas were introduced, meaning they already had a track record of operating successfully without pressure reduction; secondly, that the increased pressure would still have been within the rated or recommended levels for those pipes, $82 \%$ of which were relatively new.

Have I fairly summarised your reasons for the conclusion which we've just looked at?
A. That's right. I mean, the network was fairly new. It was part of the Victorian renovation mains programme Thames Water has been running for a while, and that's very unique, in a way. We had pipes -- high-density polyethylene pipes with age less than ten years, so they were certainly within the -- very much their pressure rating was within the pressure operating there. But the other thing is that the pressure-managed scheme was only implemented in April 2017, or two months before the actual incident. So if the pipes had been operated under these conditions for a good eight/ten years, there

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is no reason suddenly to believe that by turning back to the pressure management conditions which were in place just two months ago, suddenly it will increase the risk of pipe failures.
Q. Bearing that in mind, would you agree that increased pressure in the network that would have resulted from turning on the Hammersmith pumps or turning off the pressure reduction control would have increased the stress experienced by pipes in the network, which brought a risk, even if small, of causing a burst in the more vulnerable parts of the network which had older, unreplaced pipes?
A. Again, just referring that clearly these pipes were subjected to this kind of stress just two months before the fire. And the other thing you have to bear in mind is that one phenomena which we haven't accounted for is during the pumping, the operation of these pumps, as we discussed, they were continuously on and off. That sudden discharge was creating a huge level of pressure transients into the system itself. So, as a result of that, these pipes had already been subjected to quite a lot of stress, and my engineering judgement, having dealt with a lot of pipe failures, would be that the risk is actually minimal to go back to a pressure management scheme which was in place just two months
ago.
Q. Just bearing in mind the question that you're asked, would you accept that the increased pressure from turning on Hammersmith pumps, turning off pressure reduction control, would have brought a risk, even if small, of causing a burst in the more vulnerable parts? Could I have an answer to the question?
A. Yes, how can we quantify this?
Q. Well, I think it was put to you as small. Would you accept that?
A. Yes.
Q. Would you agree that a burst in one of the distribution pipes could have led to the loss of substantial volumes of water and wider spread depressurisation of the surrounding network?
A. Yes.
Q. And would you agree that such an event occurring on the night of the fire would have put at risk the entire water supply to the tower?
A. Correct.
Q. Now, the third alternative intervention option you identified at page 102 \{ISTRP00000009/102\}, and if we could go back to that page, please -- apologies for jumping round, Dr Stoianov -- you identified there, we can see at line 10 :

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"c. Opening boxed/closed inlets such as DM18631."
Again, a technical term, but is the opening of
a boxed/closed inlet similar to the opening of
a district boundary valve, which we discussed earlier, with the key difference that while the boundary valves opened by Thames Water simply connected the water network at the tower to other areas which were also undergoing pressure reduction, and here you refer to the opening of a valve or inlet which would have helped to bypass the pressure reduction?
A. That's right. But can I just again point out --
Q. Please do.
A. - - that in my correspondence with Thames Water and questioning Thames Water, we received two contradictory statements. One of the statements was very clearly identified by Thames Water that pumps could have been turned on and pressure reduction could have been turned offer, but a request for that was not received. So it seems that Thames Water contradicts its own assessment post-Grenfell, that one of the responses is, "Yes, we could have done it, we just didn't get the request", and the second version of events or explanation was supporting the logbook on the night of the fire, which basically says, "We perceive a higher risk of pipe burst if we actually implement this control operation in
Q. Now, the final option you refer to in paragraph 45 on page 102 is the utilisation of multiple hydrants to provide water for firefighting. Now, that refers to the use of more than one hydrant to supply a single pump appliance to maximise the flow rate delivered from the network to the pump appliance. Am I right about that?
A. Correct.
Q. Would you accept that Thames Water staff aren't experts in operational firefighting? Presumably you do.
A. Absolutely.
Q. Would you accept that Thames Water staff don't have detailed knowledge of the workings and set-up of pump appliances and other firefighting equipment?
A. Can I just again, the caveat is probably not -- I would not expect the network service technicians to have that knowledge, but I would expect the network management control centre to actually have that knowledge, or at
least have some understanding of how this provision of water for firefighting can be done with the utilisation of multiple hydrants.
Q. When you say "some understanding" ...
A. Yes, I mean, the request is to extract large volumes of water from your water distribution network, and that's subject to, again, running a hydraulic model with a specific loading condition, and it's a very computationally efficient way to do it. One can do it literally within a few minutes.
Q. Would you accept, just looking at it slightly differently, that Thames Water are not well placed to advise a fire and rescue service on what equipment to use, how to deploy it, et cetera?
A. I -- so, yes, and I totally agree with the overall gist of that message. But, equally, as an operator, if you get a request for increase in pressure, et cetera, my engineering kind of training would prompt me to ask questions: what exactly do you want? How much do you want? What flow rate do you want? Et cetera. These are very basic engineering questions to ask to quantify so that I can assess to what extent my system can respond to that and advise you accordingly.
Q. Really your criticism is focused on asking those basic questions, isn't it, and nothing more than that?

## A. That's right

Q. Can I turn now on to a separate topic, which is an assessment of higher flow rates and whether they could have been achieved.

To this end, can we go to $\{$ ISTRP00000008/216\}. If we can look at line 8 , you explain your assessment in the following terms:
"This Assessment investigates whether a higher water flow rate could have been provided from the water distribution network, based on the mathematical modelling of pressure and flow in the water distribution network using the validated hydraulic model of the water described in this chapter.
"The analysis for this Assessment includes the formulation of an optimisation problem, which selects an optimum number of fire hydrants for LFB to connect to, in order to deliver target water flow rates from the water distribution network to efficiently (100\%) utilise firefighting appliances and equipment. The formulated optimisation problem considers the hydraulic (flow and pressure) conditions in the water distribution network, the available fire hydrant locations, their discharge characteristics (flow coefficients) together with the control settings of pressure reducing valves (PRVs) at the inlets of the water distribution network as decision

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variables."
Now, the rest of section 6.8 explains in far greater detail how you carried out the assessment.

In broad terms, is it right to say that the assessment used mathematical modelling to calculate whether, given the hydraulic conditions on the night of the fire, there was an optimum combination of hydrants that could have delivered greater flow rates to firefighting equipment?
A. That's right.
Q. Now, the results of the assessment are set out at the top of page 226 in this chapter \{ISTRP00000008/226\}, which I'd be grateful if we could go to. We can see at the top of the page you say this, starting at line 3 :
"1. It was possible to achieve a flow rate of 7,460 I/min (124 I/s) without changing the control settings for the pressure reduction scheme on 14 June 2017 providing that LFB utilised multiple hydrants (e.g. fire hydrants $1,3,8,4$ and $7 \ldots$ ).
"2. It was possible to achieve a flow rate of $12,000 \mathrm{I} / \mathrm{min}(200 \mathrm{I} / \mathrm{s})$ by changing the control settings for the pressure reduction scheme on 14 June 2017 and providing that LFB utilised multiple hydrants (e.g. fire hydrants $1,2,3,4,5,7,8,11,13$ and $14 \ldots$ )."

Now, taking a step back from that, that seems to

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show -- and please say if this is not a correct
summary -- that your modelling showed that a total flow
rate of 7,400 litres per minute could theoretically have
been achieved without turning off the pressure reduction
in the network or, alternatively, 12,000 litres per
minute if the pressure reduction had been turned off; is
that fair?
A. That's right.
Q. For context, the peak flow rate actually delivered on
    14 June 2017 was about 4,320 litres per minute; is that
    correct?
A. That's right.
MR KINNIER: Could we go to page 218 in this chapter
    {ISTRP00000008/218}, please.
SIR MARTIN MOORE-BICK: Mr Kinnier, can I just ask you,
    sorry, on the page we've just left {ISTRP00000008/226},
    it suggested that the LFB could have used, what, ten
    hydrants?
MR KINNIER: Yes.
A. That's right.
SIR MARTIN MOORE-BICK: How far away would they be from the
    site of the fire? Would it be worth looking at the
    little diagram?
MR KINNIER: I'm trying to find ... if I can be given the
    reference to the map of the area.
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A. So, just for context, clearly here what we've done is
we've used the mathematical model, which simulates the
distribution of flow and pressure --
SIR MARTIN MOORE-BICK: Yes.
A. -- and also the formulation of this optimisation problem
to say -- find, given the flow coefficient -- we assume
that we know the flow coefficient of hydrants, that's
why it's so important. Given the flow coefficient of
hydrants, extract that maximum flow rate with a minimum
distance to hydrants. So that was the formulation of
the optimisation problem.
SIR MARTIN MOORE-BICK: Right.
A. But, equally, one does not need to run that more sophisticated optimisation problem; one can go and just pick up hydrants and say, "I'm going to fully open that hydrant, and if I get these things, what impact does it have?" And that is kind of the importance of having this technical knowledge and analysis available in almost near real time, which I see no reason why Thames Water couldn't have performed that duty.

The other option is what happened on the night where, as I highlight in chapter 7, there is this complete mismatch of communication. You know, you have a representative from the London Fire Brigade who says, "Give me more pressure", and at the same time you have
a technician from Thames Water who looks and, in their mindset, pressure in the network is pretty good, and they say, "We can't deliver any more", and then the intuition of making the decision on behalf of the fire rescue service is, "We can't get any more flow, so let's just keep whatever we are doing".
SIR MARTIN MOORE-BICK: All right.
MR KINNIER: Could I go to the diagram, just before the break, if it would help you, sir?
SIR MARTIN MOORE-BICK: Well, I'd just be interested to see it , to be honest.
MR KINNIER: Could we go to \{ISTRP00000006/6\}, which should give us figure 5-2, and if that could be expanded.
A. If it's more helpful, I have the solution of this specifically with the diagram of hydrants which were identified into ... I don't have the report in front of me, but certainly there was a diagram of that.
MR KINNIER: It might be.
Given the time, sir, if we could see the particular diagram -- we can find the diagram to which Dr Stoianov is referring and maybe draw it up when we return at 2.00 .

SIR MARTIN MOORE-BICK: Would that be convenient? MR KINNIER: Yes.
SIR MARTIN MOORE-BICK: All right.
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Well, Dr Stoianov, we will look at the diagram, but after lunch. All right? So we will stop there. We will resume, please, at 2 o'clock, and again, while you're out of the room, please don't talk to anyone about your evidence or anything relating to it. All right?
THE WITNESS: Thank you very much.
SIR MARTIN MOORE-BICK: Thank you very much.

## (Pause)

Thank you, Mr Kinnier. 2 o'clock, please.
MR KINNIER: Thank you, sir.
SIR MARTIN MOORE-BICK: Thank you.
(1.01 pm)
(The short adjournment)
( 2.00 pm )
SIR MARTIN MOORE-BICK: Right, Dr Stoianov, ready to carry on?
THE WITNESS: Yes, I am, thank you.
SIR MARTIN MOORE-BICK: Thank you very much.
Yes, Mr Kinnier.
MR KINNIER: Thank you, sir.
Before the break, Dr Stoianov, we were searching for a diagram which showed all the hydrants. We think we have found the diagram to which you were referring, so could we look at $\{$ ISTRP00000008/219\}. If the diagram,
figure 6-114, could be expanded.
(Pause)

Sometimes these things take time, so don't worry.
A. I appreciate this.
(Pause)
Q. Thank you.

That shows, I think, the hydrants which we were discussing before lunch, and I think in the centre we see FH1, and immediately below that is a circle with two bits coming off it. That's the private hydrant; is that right?
A. Correct. Just, first of all, what this figure shows is the hydrants which are within the area of
Grenfell Tower. All the hydrants which I considered in my analysis are within 300 metres from Grenfell Tower on this diagram, and the assumption was that these hydrants could be accessed with a pump relay, with a single pump relay, very much as LFB has done.

Just a little bit more context to this diagram and the analysis. Clearly the diagram also assumes, and the analysis also assumes, that we have some estimates about the flow coefficients of hydrants which normally should be a regular practice of flow testing, so that's one aspect.

The second aspect, what it does is it runs the
analysis for loading conditions or for demand, which first of all take into account a standard PDA procedure of LFB, you know, pre-determined attendance procedure, which includes a single aerial appliance for high-rise buildings. So, in other words, what I assume for these 7,500 litres per minute is that I have one aerial appliance of about 4,200 litres per minute, let's assume that they have to deploy also a ground monitor of about 1,600 litres per minute, then there needs to be about 1,500 litres per minute for internal firefighting, so this is very much, I would imagine, a reasonable assumption, to assume that if a PDA includes that appliances, we need to have sufficient flow rate to fully deploy these appliances, and that's where the 7,500 litres per minute come from for this first analysis.

The second --
Q. Sorry, Dr Stoianov, my question, some time ago now --
A. Okay.
Q. -- was simply to confirm the diagram.
A. It is .
Q. Thank you.

I want to sort of return back to where we were,
doctor, and deal with the assessment of whether higher flow rates could have been achieved. I think some of
the points you are adverting to now we can better address in a more focused way as we go through that particular topic.
A. Okay.
Q. Now, could we go back to $\{$ ISTRP00000008/218\}. This is an extract from your report, and it sets out some points which are relevant to the assumptions that you made in the assessment which we were discussing before the break and which you have been touching upon again.

What it sets out there, under the heading "6.8.1.2 Assessment 2: assumptions", is this:
"It is important to note the limitations for this Assessment. The estimated flow figures scenarios above [the flow rates of 7,400 and 12,000 which the assessment tested] are for illustrative purposes only, to assess from the perspective of the water distribution network whether it would have been possible to supply those flow rates given the hydraulic conditions in the network.
"None of the above should be interpreted as any suggestion on my part as to which appliances or equipment LFB could or should have deployed on the night of the fire, those being questions far beyond both my expertise and the scope of this report.
"The Assessment further relies on the following factors:

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"1. LFB having up-to-date knowledge of the operational status and flow discharge characteristics of fire hydrants based on flow tests of fire hydrants (this does not appear to have been the case at Grenfell Tower ...);
"2. LFB using multiple fire hydrants to supply water to individual aerial appliances (e.g. LFB setting up pump relays as done for fire hydrant $\mathrm{H} 8 \ldots$ )
"3. TWUL [Thames Water] providing expert engineering guidance and support to LFB, including the use of a hydraulic model and near real time hydraulic telemetry data ..."

Now, in addition to the factors and assumptions listed there, is it also important to make clear that you don't know about and cannot comment on whether it would have been logistically possible or operationally feasible for the LFB to have used the specific optimum combination of the specific ten hydrants identified by this assessment in order to achieve those flow figures?

## A. Correct.

Q. So, for example, some of the hydrants identified may not have been in operationally suitable locations due to access problems or other difficulties which are understandably beyond your knowledge and expertise?
A. Correct. As I said, this is an illustrative example of
a process that -- analytics that could have been deployed.
Q. This assessment was calculated using a complex mathematical model which you validated and refined following physical testing carried out after the fire; is that right?
A. That is correct, but I also have expectations that water utilities should and they do that sort of level of analysis on a regular basis.
Q. Now, the mathematical modelling you used also factored in the flow coefficients of the hydrants at or near the tower which you were able to calculate following a series of tests you carried out in 2008; is that right?
A. 2018, yes.
Q. 18, apologies, yes. That data, of course, wasn't available to anyone on 14 June 2017.
A. No, that's absolutely correct, but as an engineering judgement, I can make certain assumptions about these flow coefficients if I'm faced with the need to run that sort of level of analysis.
Q. Whatever data was available at the time of the fire, for quite proper reasons, you're not in a position to comment on whether it would have been practically possible for Thames Water to carry out these kind of

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complex mathematical modelling and hydrant optimisation calculations in real time in the midst of the incident in the early hours of 14 June 2017; would you agree with that proposition?
A. Not entirely, no.
Q. Let's take it in stages. What do you agree with, then?
A. I agree that running probably a complex -- formulating this as an optimisation problem might have been beyond the scope and knowledge of Thames Water on the night of the fire. But, equally, the problem what I'm describing could have been enumerated manually. In other words, Thames Water had access to a hydraulic model, they had access to near real-time telemetry coming from their system, and that would have been sufficient to run the hydraulic model and manually almost pick up hydrants and demonstrate that larger flow rates could have been extracted. They might not have been optimal, as optimal defined in mathematical terms, but they would have been far greater than what was achieved on the night of the fire.
Q. If Thames Water had been able, for example, to carry out an exercise in mathematical modelling and hydrant optimisation calculations in real time in the middle of the incident, and were indeed able to communicate the ideal combination of hydrants to the LFB, that would
likely have required the LFB to completely reorganise its water supply set-up midway through the incident, which of itself would have caused disruption and delay. Again, would you agree with that proposition?
A. I agree that that would have required the LFB to change their operational strategies, but I wouldn't go as far as stating that this would delay activities. So I don't know how that conclusion can be drawn, that this would delay activities, because if you look -- and I'm just observing facts here, by no means this is part of my competence, but if I look at the statements made by Incident Commander Roe and O'Loughlin, they completely dismissed the role of the use of water in the firefighting operations.
Q. But is it fair to say that, looking at the assumptions you yourself have set out in the report and the limitations you have fairly conceded there, the answers you have, again, fairly given to the points I've put to you just now, that the results of the assessment about flow rates are what theoretically could have been delivered from the water distribution network in optimum hydraulic conditions, and they don't allow us to draw any safe conclusions about what flow rates the LFB and Thames Water could or should have achieved on the night?
A. I guess, yes.

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## Q. Can I now turn to a separate topic, which --

A. Just before we move away, can I just also note that the analysis I carried out was carried out for peak demand, and that prompted me because the network management centre of Thames Water raised serious concern that as demand picks up, they will have significant problems. So I ran that analysis on the worst-case scenario, which was the morning peak demand at 8 o'clock in the morning.

## Q. Thank you.

The next section I'd like to turn to is whether regulatory standards relating to the supply of water were met.

For this purpose, if we could turn to \{ISTRP00000005/48\}. In this part of your report, you provide, usefully, an overview of the relevant statutory and regulatory standards that apply to the provision of water. I'd like to go through those standards that apply to various aspects, such as water pressure, flow rate and the rest of it.

Turning, first, though, to water pressure, you set out at paragraph 2 , which starts at line 7 on that page, this:
"The Water Supply and Sewerage Services (Customer Service Standards) Regulations 2008 (the
GSS Regulations) require a minimum pressure of 7 m
(0.7 bar) static head (pressure) in the communication pipe supplying premises with water. Ofwat [the water regulator] also refers to a 'reference level of service' of 10 m pressure on the customer's side of the main stop tap. Due to the practical difficulties of measuring pressure there, Ofwat suggests that water companies instead use a 'surrogate' measure of 115 m pressure head in the adjacent distribution main and this is common industry practice."

If we could go to page 234 of chapter 6 , which we find at $\{$ ISTRP00000008/234\}, at paragraph 6.9 .6 you set out your conclusions in relation to the pressure levels on 14 June 2017, and we can see, at paragraph 29 at the foot of that page, this:
"I mathematically simulated the pressure heads at each hydrant used by LFB to supply water for firefighting on the 14 June 2017. The lowest estimated pressure head is 25 m (2.5 bar) for the fire hydrant H8 The pressure head at hydrants H 1 (a fire hydrant), H3 (a fire hydrant) and H5 (a wash-out hydrant) varied between 29.4 m and 35.8 m pressure head (2.9 bar to 3.5 bar)."

You go on to say these minimum pressure figures on 14 June exceeded, indeed comfortably exceeded, both the 0.7 bar and the 1.5 bar regulatory standards. Is that

[^1]
## A. Yes.

MR KINNIER: If we can go to --
SIR MARTIN MOORE-BICK: That sounded like a rather guarded reply. You say with a lot of caveats; I think possibly we ought to know what you say about that.
A. I mean, I find a lot of these documents - - first of all, they are not regulatory documents, they just provide recommendations in that respect, and they have --

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there's a lot of ambiguity between these numbers. So if I take the number of the national guideline document for the provision of water, first of all, I've identified a number of limitations. It gives a certain flow rate between 1,200 to 2,400 litres per minute, so this is a very wide range.

At the same time, that wide range, it doesn't really seem to match the pre-determined attendance, again going back to my point that if the London Fire Brigade has pre-determined attendance to deploy an aerial -- and as we learned from the press recently, they've purchased a whole set of new aerial ladder platforms -- does that mean that you're purchasing a Rolls Royce and you're driving this Rolls Royce in first gear because purely you don't have the capacity to utilise that equipment? And that's the kind of -- that's the caveats I want to put around. There are these numbers, but actually the meaning of these numbers, it's hugely questionable.
SIR MARTIN MOORE-BICK: All right, thank you.
MR KINNIER: I was going to draw you now to the points which you would want to caveat that with --
A. Okay.
Q. -- so I was going to come to those questions now.

If we can go to $\{$ ISTRP00000005/14\}, I think really
I want to take you through the issues which you say the
guidance document doesn't take account of but it should in order to provide, I think, a more satisfactory or tolerably reliable figure.

In essence, we can see from the underlined subheadings on that page the facts and matters which you think ought to be accounted for which aren't: first of all, the size of the building; secondly, the building materials used and the extent of compliance with Building Regulations; thirdly, the presence of fire protection systems, such as sprinklers; finally, whether or not an aerial appliance is required.

Are those the particular points which you feel the national guidance document ought to consider but it doesn't?
A. Correct.
Q. The final matter I would like to take you to is the quantity of water and compliance with regulatory standards in that regard.

To this end, can we stay in this particular chapter but go to page 48 \{ISTRP00000005/48\}, and if we look at paragraph 4 at line 28 on that page, dealing here, as the subheading indicates, with quantity of water, is it right to say that quantity of water is simply about there being enough in the system, so it's not going to run out, whereas flow rate is about how much water can
be delivered at any particular given time?
A. Correct.
Q. Now, your report addresses the available quantity of water on 14 June on page 229 of chapter 6 , which we find at $\{$ ISTRP00000008/229\}. If we look at paragraph 2 , the report lists the sources of water which reply the Barrow Hill zone in which the tower is found. At paragraph 3 you say this:
"The average daily demand for the Barrow Hill Zone in 2017 was estimated at 116.58 megalitres per day, or the equivalent of $80,958 \mathrm{l} / \mathrm{min}(1,349 \mathrm{l} / \mathrm{s})$. In comparison, the maximum flow rate used by LFB for firefighting on the 14 June 2017 did not exceed $4,320 \mathrm{I} / \mathrm{min}(\sim 72 \mathrm{I} / \mathrm{s})$, and this water flow rate for firefighting peaked at hours of minimum water consumption."

Then if we go slightly further down the page to paragraph 5 , you concluded thus:
"The Barrow Hill zone had no water storage and/or water availability constraints to be able to meet, and significantly exceed, the water demand for fighting the fire at Grenfell Tower."

Now, in your view, therefore, is it safe to say that the quantity of water available for firefighting was more than adequate?

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A. Yes, definitely.
MR KINNIER: Dr Stoianov, those are all the questions I have
        for you now.
            Sir, might I ask for the usual break of, say --
SIR MARTIN MOORE-BICK: Yes.
MR KINNIER: -- quarter of an hour to see whether I have
    missed anything or to see whether there are any
    particular points that anyone else would like me to
    raise.
SIR MARTIN MOORE-BICK: Yes. Very well.
            Well, Dr Stoianov, when we get to this stage and
        counsel thinks he's asked all the questions he ought to
        ask, we always have a short break to give him a chance
        to check that he has not overlooked anything --
THE WITNESS: Okay.
SIR MARTIN MOORE-BICK: -- and also to give other people who
    are following the proceedings from elsewhere the chance
    to suggest questions which perhaps ought to be put to
    you.
            So we're going to break now. We'll resume at 2.40,
        please, and at 2.40 we'll see if there are any more
        questions for you. All right?
    THE WITNESS: Okay, thank you.
SIR MARTIN MOORE-BICK: Thank you very much.
        (Pause)
            1 3 5
            Thank you very much, Mr Kinnier. 2.40.
MR KINNIER: Thank you, sir.
SIR MARTIN MOORE-BICK: Thank you.
(2.23 pm)
            (A short break)
(2.40 pm)
SIR MARTIN MOORE-BICK: All right, Dr Stoianov. Let's see
    if there are any more questions for you, shall we?
            Yes,Mr Kinnier.
MR KINNIER: Sir, thank you for the further time.
            I have no further questions for you, Dr Stoianov, so
    it just leaves me to say thank you very much for
    providing such a comprehensive report and, indeed,
    a further supplemental report, and for attending to give
    evidence today. It's very, very much appreciated.
THE WITNESS: Thank you.
SIR MARTIN MOORE-BICK: Yes, and it's right that I should
    say thank you as well, Dr Stoianov, on behalf of all
    three members of the panel. You have done an awful lot
    of work on this matter, with great care, as we can tell
    from your report, and it's been very interesting to have
    the chance to hear you in person as well. So thank you
    very much, we have benefitted greatly from your
    evidence, and we're very grateful to you for coming to
    give it. So thank you very much.
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THE WITNESS: Thank you very much for the opportunity as
    well. Thank you.
SIR MARTIN MOORE-BICK: You're free to go, thank you.
THE WITNESS: Bye-bye.
    (The witness withdrew)
SIR MARTIN MOORE-BICK: Yes, Mr Kinnier. Well, that's all
    we have for today; is that right?
MR KINNIER: That's right, sir.
SIR MARTIN MOORE-BICK: So we shall finish at that point,
    but tomorrow we have another expert witness coming to
    give us his evidence, and we shall look forward to
    seeing him, I think it is -- Professor Bisby, isn't
    it? --
MR KINNIER: Yes.
SIR MARTIN MOORE-BICK: -- tomorrow. Good, and we'll do
    that at 10 o'clock tomorrow morning.
MR KINNIER: Thank you, sir.
SIR MARTIN MOORE-BICK: Thank you very much.
        10 o'clock tomorrow morning. Thank you.
(2.43 pm)
            (The hearing adjourned until 10 am
            on Thursday, 9 June 2022)
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DR IVAN STOIANOV (sworn)
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[^0]:    A. Not entirely, because we have a certain hierarchical structure within the systems. The systems include the bulk transmission of water, for example from reservoirs to treatment works to certain kind of service reservoirs. We call this the water transmission network. Then, from the water transmission networks, the pipes go into the streets to deliver water to individual customers, so this is what we refer to generally as water distribution. Then we have the supply pipes which go to the individual customers.

    So "water supply system" is the overarching term which combines both the transmission and the distribution.
    Q. Thank you.

    Now, if we can stay in this chapter of your report but go to page 8 \{ISTRP00000003/8\}, and we see at the top of that page figure 3-2. In broad terms, this illustrates how water is delivered from the water distribution system to a Fire Brigade during a fire. In broad terms, is that a correct summary?
    A. Yes, it is.
    Q. If we can first identify the various components of this diagram, the blue symbol to the left is a water tank or reservoir, ie the water source; is that right?
    A. Correct.

[^1]:    a fair summary of your position?
    A. It is.
    Q. Thank you.

    Can I now turn to water flow rate.
    For this purpose, can we go to \{ISTRP00000005/48\}, and if we could look at paragraph 3 in particular.

    If we could look at paragraph 3, you note there that:
    "Section 38(1) of the Fire and Rescue Services Act 2004 states that a ' fire and rescue authority must take all reasonable measures for securing that an adequate supply of water will be available for the authority's use in the event of fire. '"

    Elsewhere in this chapter \{ISTRP00000005/11\} you note that:
    "The statute provides no further detail on what constitutes an 'adequate' supply and there is no minimum flow rate figure explicitly stipulated in the Fire and Rescue Services Act 2004."

    Now, there is guidance, I think you identify in your report, and if we continue in paragraph 3 on the page that's on the screen, we see at the end of line 21 you say this:
    "The National Guidance Document on the Provision of Water for Fire Fighting ... recommends a flow rate of

